

AN INVESTIGATION INTO FLAT GLASS FIBRES FOR INJECTION MOULDED POLYAMIDE 6,6 COMPOSITES

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1. Background

- Glass fibres (GFs) account for over 90% of reinforcement fibres used in fibre-reinforced composites
- Innovation is required in glass reinforced thermoplastics to support the transition to low-carbon vehicle platforms
- Flat glass fibres (FGFs) developed to improve mechanical & physical properties in injection moulded parts
- Flat glass fibres are fibres with a 'flattened elliptical' cross-section
- Composite property improvement thought to be related to reported increased in residual FGF length
- Very little academic literature to support industrial uptake
- In depth study required to correlate differences in fibre properties to composite microstructure and properties

2. Fibre geometry characterisation

- The cross-sectional area (CSA) of FGFs was characterised & compared against circular fibres of same composition
- Established that accurate characterisation of FGF CSA only possible using Scanning Electron Microscopy (SEM)
- Attempts to measure FGF CSA from less resource intensive optical microscopy were unsuccessful
- With optical microscopy significant edge effects observed; SEM has higher magnification and minimal edge effects
- Significant difference in tensile properties found depending on CSA observation method used:

	Optical transverse diameter	Optical cross-sectioned	SEM cross-sectioned
Mean Cross Sectional Area (μm^2)	145 ± 6	134 ± 9	143 ± 7
Mean Fibre Tensile Strength (MPa)	2080 ± 100	2315 ± 158	2345 ± 174

Table 1: Mean CSA and tensile strength of unsized, circular fibres, 20mm gauge length, with CSA measured by different methods, 95% confidence interval error.

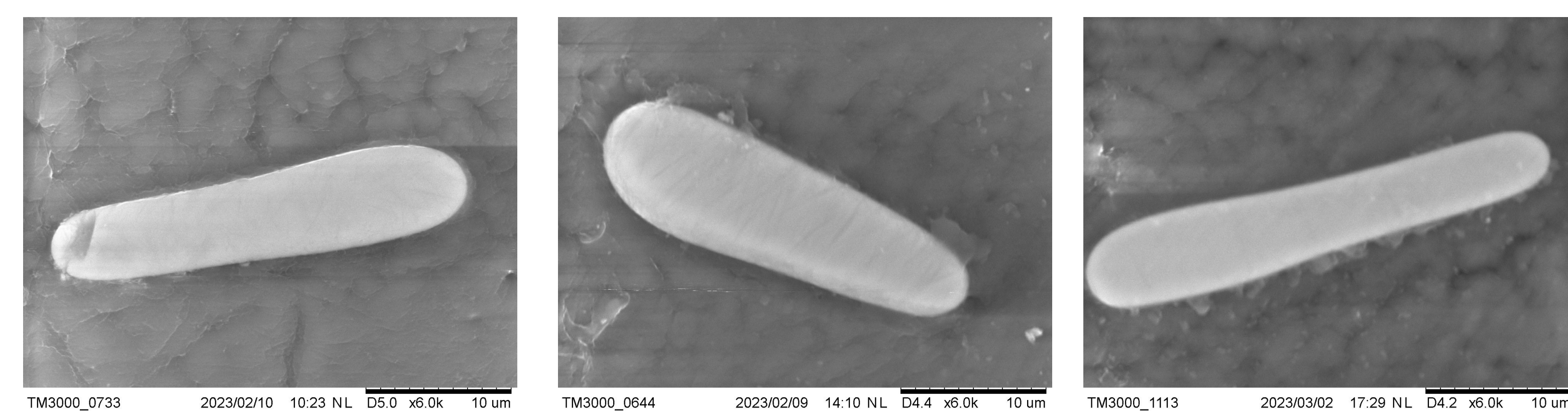


Figure 1: SEM images of flat glass fibres, highlighting the sometimes-skewed nature of the observed cross-section.

- Observed that FGF shape is not always 'perfectly flat'; many fibres show skewed cross-sections

3. Fibre tensile properties

- Tensile strength characterised at 20mm, 40mm and 80mm gauge lengths
- Sized flat glass fibres found to be significantly stronger than circular sized fibres (CGFs); PA compatible sizing
- No significant difference observed between unsized flat and circular fibres

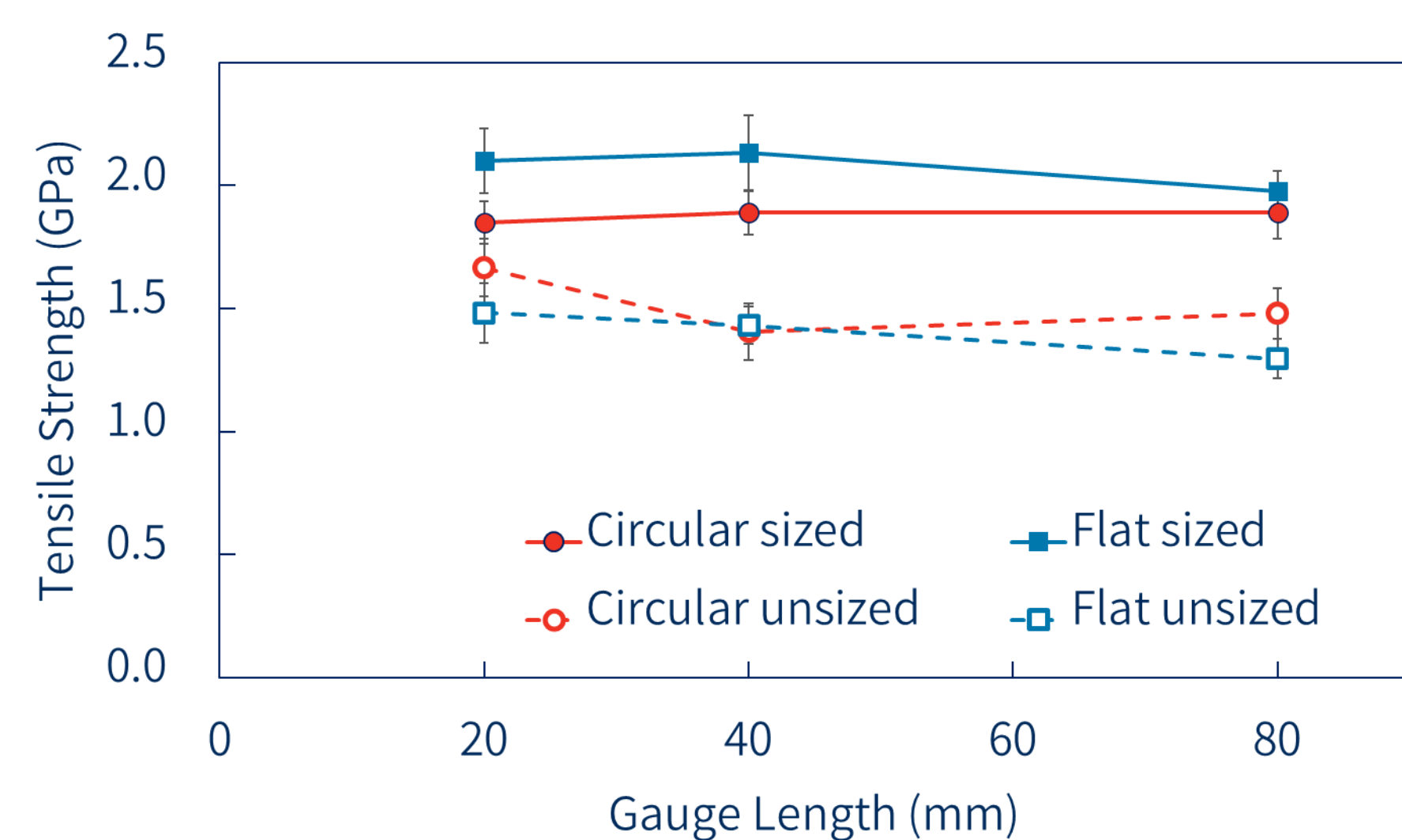


Figure 2: Tensile strength of flat and circular, unsized and sized fibres, at 20 mm, 40 mm and 80 mm gauge length, with 95% confidence interval error bars

- Differences in failure behaviour noted for flat and circular fibres across different gauge lengths; FGFs shatter less

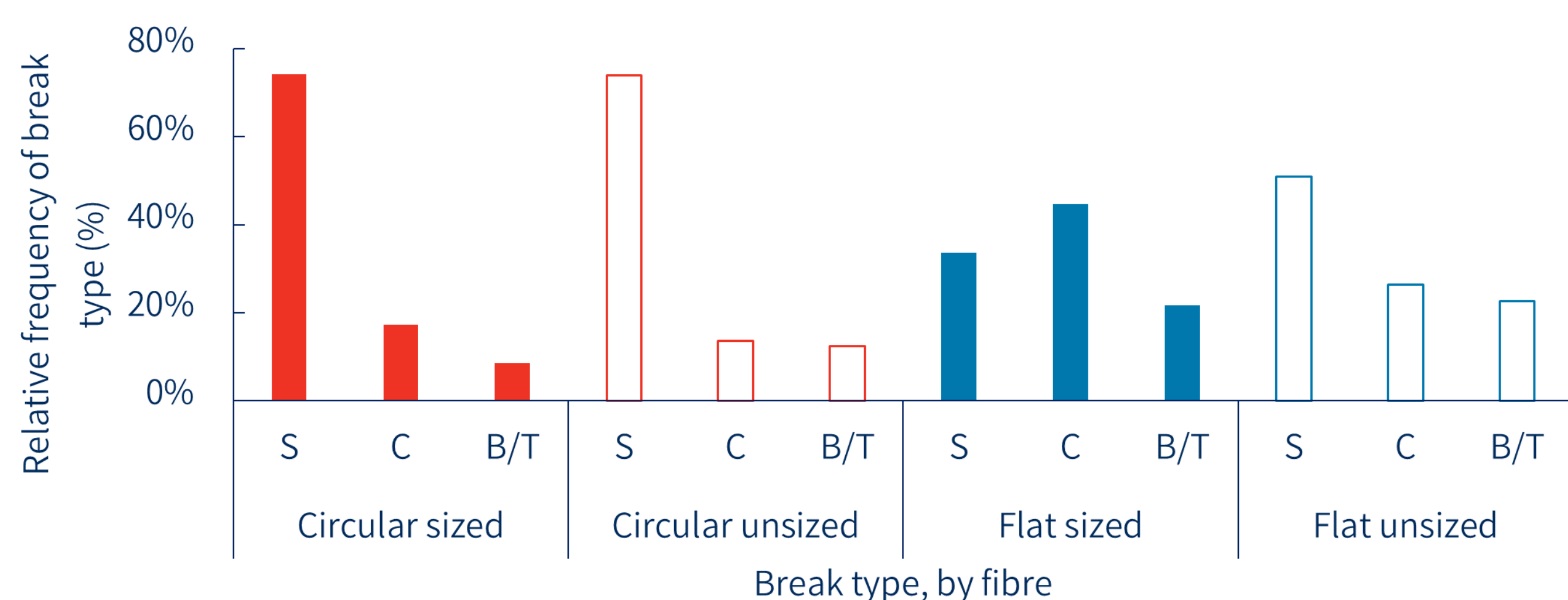


Figure 3: Failure behaviour of circular and flat, sized and unsized fibres, at 20 mm gauge length, where: S, denotes shattered fibres; C, fibres which broke cleanly with remains; B/T, fibres which broke cleanly with remains near the end tabs.

- Fractography observations show the different types of failure behaviour of flat glass fibres

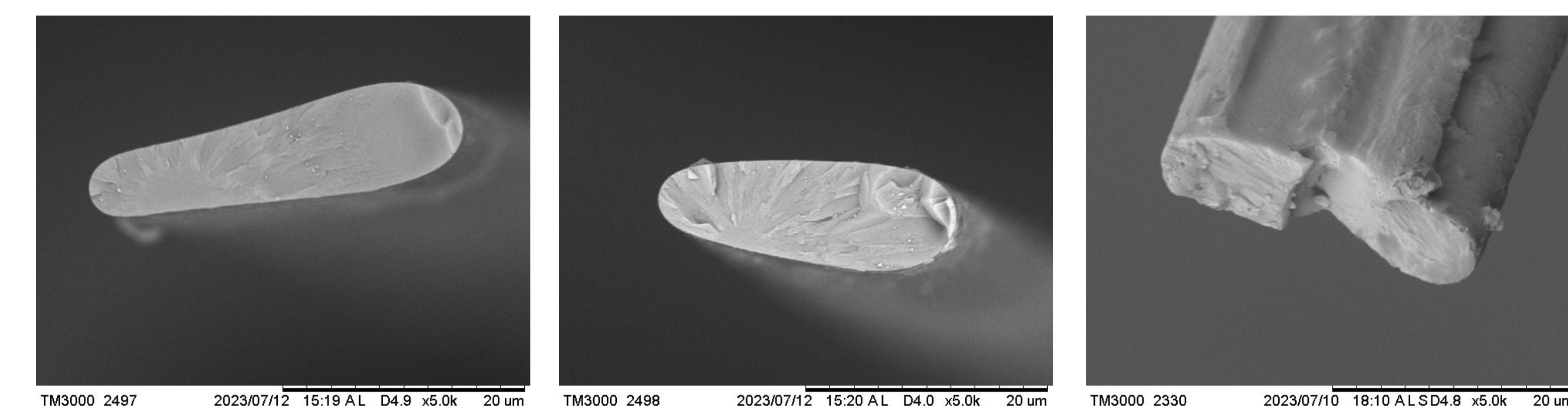


Figure 4: Fractography analysis using SEM showing different fracture surfaces of glass fibres after tensile testing

4. Composite fibre length analysis

- Fibre length degradation occurs throughout the compounding and injection moulding process
- Tensile strength is directly correlated to the residual fibre length of injection moulded composites

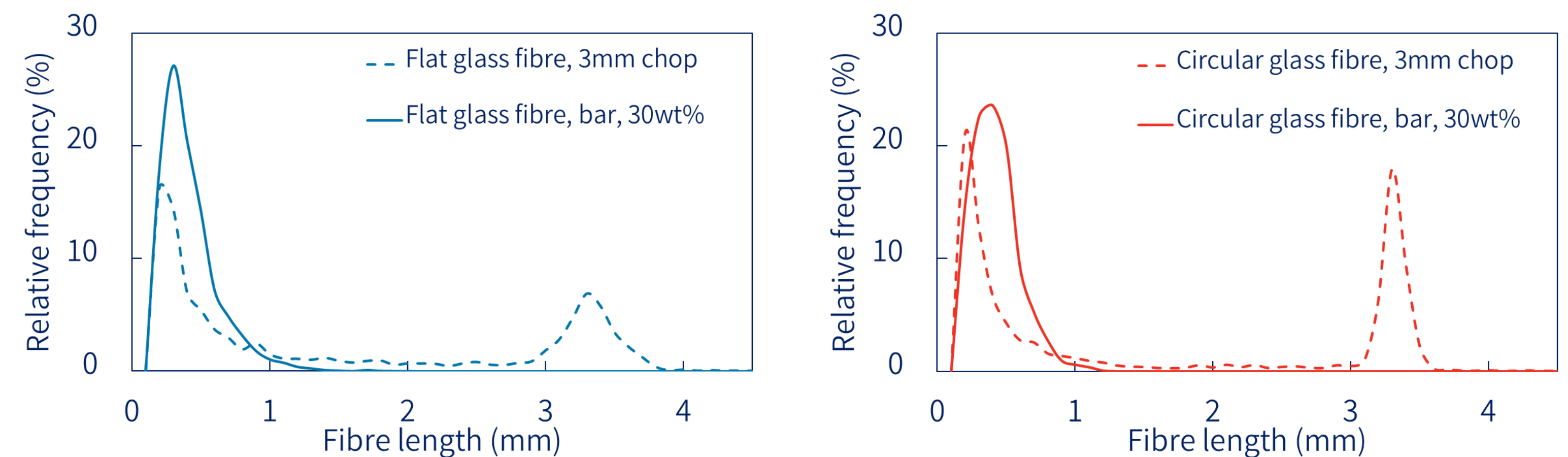


Figure 5: Fibre length distributions for virgin input chop and residual fibre length in composite (PA6,6) bars with 30wt% fibre, circular fibres left, flat fibres right.

- Residual fibre length found to be greater in flat glass fibre reinforced polyamide 6,6 (PA6,6) than circular fibre

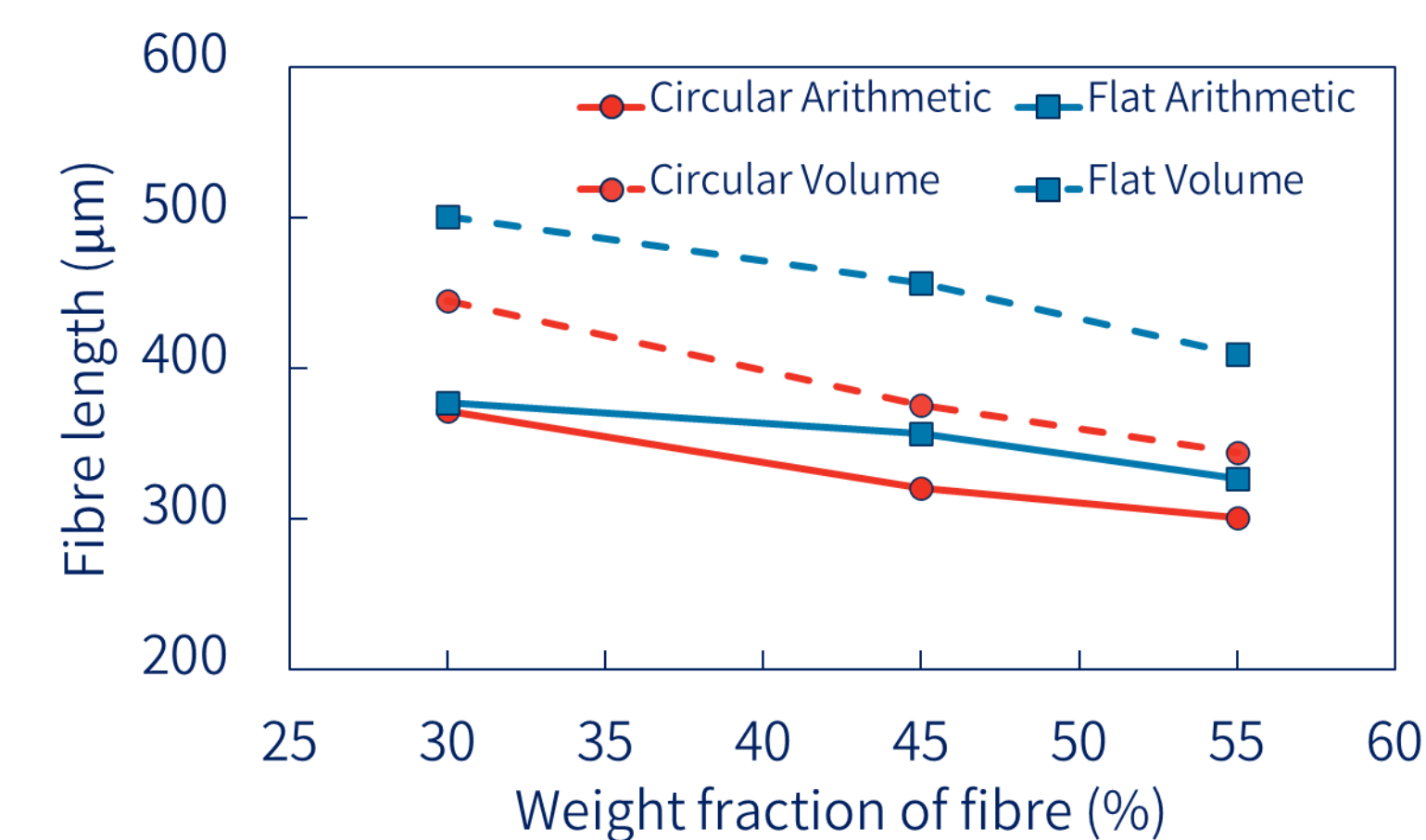


Figure 6: Arithmetic and volume mean residual fibre length of circular and flat fibre reinforced polyamide 6,6, composites.

- Data supports hypothesis that lower fibre second moment of area leads to less fibre breakage during processing

5. Composite tensile properties

- Tensile properties assessed in PA6,6 reinforced glass of varying glass weight contents: 30-55 wt%
- Use of FGF only have significant improvement on properties at high weight fractions when dry as moulded (DaM)

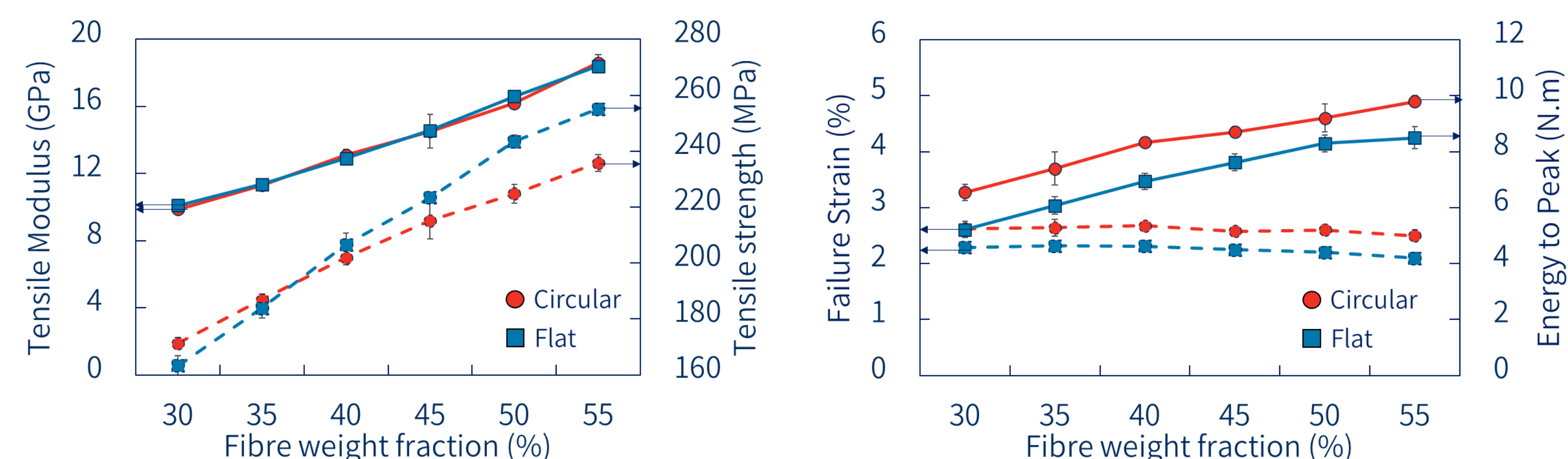


Figure 7: Tensile strength and modulus (left), and Energy to yield and Failure strain (right), of unconditioned (DaM) flat and circular reinforced polyamide 6,6, at 30-55wt% fibre content, with 95% confidence interval error bars.

- After 24 h conditioning in a water bath at 100°C (and subsequently tested at room temperature), FGF have a significant influence on room temperature tensile properties

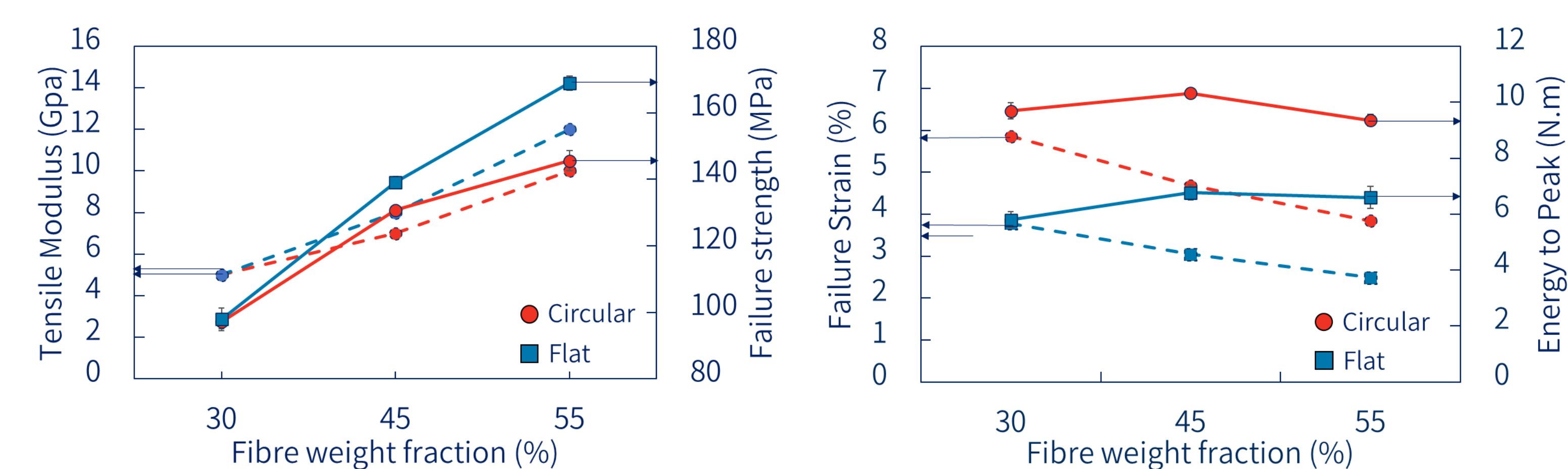


Figure 8: Failure strain and Failure strength (left), and Energy to yield and tensile modulus (right), of conditioned (24 h boiling water) flat and circular reinforced polyamide 6,6, at 30 wt%, 45 wt% and 55 wt% fibre content, with 95% confidence interval error bars.

- This significant influence after conditioning is consistent with predictions based upon micromechanical modelling
- In order to fully understand the origins of these differences, characterisation of Interfacial Shear Strength and fibre orientation also required in future works

6. Conclusions

- SEM is required for accurate characterisation of FGF CSA; FGFs frequently show skewed cross-sections
- Sized FGFs have improved tensile properties over CGFs; failure behaviour of FGFs is different to CGFs
- Use of FGFs leads to increased residual fibre length at same wt% of fibre when compared to CGFs
- Improved DaM composite tensile properties with FGFs only noted at high fibre weight fractions
- Significant improvement in boiling water conditioned composite tensile properties with FGFs

7. Acknowledgements

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