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# **Hierarchically porous carbon foams coated with carbon nitride: Insights into adsorbents for pre-combustion and postcombustion CO<sup>2</sup> separation**

Maryna Vorokhta<sup>a,b\*</sup>, Muhammad Irfan Maulana Kusdhany<sup>c</sup>, Martina Švábová<sup>a</sup>, Masamichi Nishihara<sup>b,c,d</sup>, Kazunari Sasaki<sup>b,d,e</sup>, Stephen Matthew Lyth<sup>b,f,g\*</sup>

*<sup>a</sup>Department of Geochemistry, Institute of Rock Structure and Mechanics, Czech Academy of Sciences, V Holešovičkách 94/41, 18209 Prague 8, Czech Republic*

*<sup>b</sup>Next-Generation Fuel Cell Research Center (NEXT-FC), Kyushu University, 744 Motooka, Nishi-ku, Fukuoka, 819-0395, Japan*

*<sup>c</sup>Department of Automotive Science, Graduate School of Integrated Frontier Sciences, Kyushu University, 744 Motooka, Nishi-ku, Fukuoka, 819-0395, Japan*

*d International Research Center for Hydrogen Energy, Kyushu University, 744 Motooka, Nishi-ku, Fukuoka, 819-0395, Japan*

*<sup>e</sup>Department of Hydrogen Energy Systems, Faculty of Engineering, Kyushu University, 744 Motooka, Nishi-ku, Fukuoka, 819-0395, Japan*

*<sup>f</sup>Department of Chemical and Process Engineering, University of Strathclyde, 75 Montrose St, Glasgow G1 1XL, United Kingdom*

*<sup>g</sup>Department of Mechanical Engineering, University of Sheffield, Western Bank, Sheffield, S10 2TN, United Kingdom*

\*Corresponding Author. E-mail address: [vorokhta@irsm.cas.cz](mailto:vorokhta@irsm.cas.cz) (M. Vorokhta), stephen.lyth@strath.ac.uk (S.M. Lyth)

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#### **Abstract**

Adsorption is fundamental to many industrial processes, including separation of carbon dioxide from other gases in pre- or post-combustion gas mixtures. Adsorbents should have high capacity and selectivity, which are both intimately linked with surface area, pore size distribution, and surface energy. Porous carbons are cheap and scalable adsorbents, but greater understanding of how their textural properties and surface chemistry affects their performance is needed. Here, we investigate the effect of nitrogen doping on  $CO<sub>2</sub>$  adsorption. Microporous carbon foams with large surface area (> 2500 m<sup>2</sup> g<sup>-1</sup>) and pore volume (1.6 cm<sup>3</sup> g<sup>-1</sup>) are synthesized, then coated with varying amounts of carbon nitride (up to  $17$  at% nitrogen) to achieve high  $CO<sub>2</sub>$  uptake (25.5 mmol  $g^{-1}$ ) and selectivity (CO<sub>2</sub>:N<sub>2</sub> = 21), whilst also giving insights into the relationship between structure and function. At low pressure (relevant to post-combustion capture), moderate carbon nitride loading leads to enhanced uptake and selectivity by combining large ultramicropore volume with the introduction of Lewis base sites, leading to high isosteric heat of adsorption. Higher carbon nitride loading further increases selectivity but lowers uptake by blocking micropores. Conversely, at high pressure (relevant to pre-combustion capture) the uncoated carbon foam displays superior uptake, because mesoporosity is the dominant factor in this regime, rather than the presence of ultramicropores. Finally, the samples displayed excellent regeneration under repeated adsorption-desorption cycles, and breakthrough curves were measured. These results underscore the delicate balance required for optimal material design when applying porous carbon adsorbents to  $CO<sub>2</sub>$  separation processes. Moving forward, improved adsorbents will contribute to the proliferation of carbon capture and storage (CCS) and carbon capture and utilisation (CCU) technologies, ultimately contributing reduced anthropogenic  $CO<sub>2</sub>$  emissions.

Keywords: porous carbons, CCS, CO<sub>2</sub> adsorption, selectivity, breakthrough curve, isosteric heat

## **1. INTRODUCTION**

Anthropogenic  $CO<sub>2</sub>$  emissions are contributing to global heating, extreme weather, and ocean acidification [1,2]. Resolving this is crucial to prevent environmental catastrophe. Thermal power plants burning fossil fuels are the main culprit for these emissions, so should be the main target of remediation technologies [3]. Carbon capture utilisation and storage (CCUS) technologies, crucial for the separation of  $CO<sub>2</sub>$  from other gases, include pre-combustion, postcombustion, and oxy-fuel combustion capture methods [4].

In the field of gas separation, much research focusses on the design of adsorbent materials tailored for CO<sup>2</sup> capture. Adsorbents must fulfil stringent criteria, including high adsorption capacity, good selectivity, fast kinetics, and efficient regeneration over many adsorptiondesorption cycles [5]. Furthermore, the material must be cost-effective and obtained sustainably. As such, porous carbons are widely employed in separation [6–10]. Other materials commonly investigated include metal-organic frameworks (MOFs) [11], carbonyl-based polymers [12], hypercrosslinked polymers (HPCs) [13], zeolites [14,15], cement [16], and silica [17,18]. Machine learning analyses of the extensive data, identify essential adsorbent characteristics for separation, including large pore volume ( $> 0.5$  cm<sup>3</sup> g<sup>-1</sup>), high specific surface area (> 450 m<sup>2</sup> g<sup>-1</sup>), and small pore diameter (< 0.442 nm), confirming the suitability of porous carbons [19]. Indeed, activated carbons are thought to be the most-studied class adsorbents for of CO<sup>2</sup> separation in recent years [20].

Despite their widespread application, there is still significant scope for improving the activated carbons for  $CO<sub>2</sub>$  separation. Two main strategies involve: (i) maximising the surface area and tailoring the pore volume to increase the adsorption sites within micropores, and (ii) altering the surface chemistry to enhance the adsorbate-adsorbent interactions by inducing hydrogen bonding, dipole-dipole or Lewis acid-base interactions. Varying the porosity can be achieved by controlling the activation conditions. For pre-combustion applications, mesopores are generally beneficial [7,21], whilst for post-capture technologies micropores are targeted [22,23]. Meanwhile, surface chemistry adjustments often involve nitrogen-doping [24,25], introducing Lewis base sites that interact strongly with  $CO<sub>2</sub>$ , a Lewis acid [26]. Nitrogen incorporation can be achieved by using nitrogen-rich precursors [27], or heating carbons in the presence of nitrogen-rich compounds [28]. However, these techniques often make it challenging to precisely control the nitrogen content or achieve high nitrogen levels.

Coating materials with carbon nitride, with its high nitrogen-to-carbon ratio (4:3), can significantly increase nitrogen content. Graphitic carbon nitride  $(g-C_3N_4)$  can be formed by the condensation of melem into tri-s-triazine subunits, linked by tertiary nitrogen (Scheme S1) [29], while incomplete polymerisation yields amorphous forms  $(a-C_3N_4)$  with variable nitrogen content [30]. Due to the combination of excellent stability, high nitrogen content, and ultramicropores formed between triazine subunits, carbon nitrides have been investigated as  $CO<sub>2</sub>$  adsorbents in several cases. For example, carbon nitride aerogels adsorb 4.2 mmol  $g<sup>-1</sup>$  of  $CO<sub>2</sub>$  with selectivity of 113 ( $CO<sub>2</sub>/N<sub>2</sub> = 10/90$  vol%) at 300 K and 100 kPa [31]; microporous carbon nitrides with uptake of  $\sim 6.2$  mmol  $g^{-1}$  at 273 K and 3 MPa [32], and ordered mesoporous carbon nitrides with uptake of 5.63 mmol  $g^{-1}$  at 273 K and 3 MPa [33] have been reported. Meanwhile, templated mesoporous carbon nitrides achieved very high  $CO<sub>2</sub>$  uptake of 13.5 mmol g<sup>-1</sup> at 3 MPa due to their relatively large surface area (901 m<sup>2</sup> g<sup>-1</sup>) [34]. Most notably, polyethylenimine-functionalized carbon nitrides exhibited exceptional selectivity (>6500 for  $CO<sub>2</sub>/N<sub>2</sub> = 15/85$  vol%), albeit with low adsorption capacity (1.8 mmol g<sup>-1</sup> at 298 K) [35], attributed to strong chemisorption by amine groups reacting with  $CO<sub>2</sub>$  [35].

Carbon nitride coating exhibits a different mechanism in  $CO<sub>2</sub>$  adsorption compared to nitrogen doping. Accordingly, nitrogen doping integrates nitrogen atoms into the carbon material lattice, creating defects and altering electronic properties of the carbon framework. This enhances the carbon surface basicity and improves  $CO<sub>2</sub>$  uptake, as nitrogen atoms acting as Lewis bases readily interact with acidic  $CO<sub>2</sub>$  [28]. Conversely, carbon nitride does not integrate into the carbon framework but rather coats the material, primarily adsorbing  $CO<sub>2</sub>$ through interactions with its nitrogen-containing units. The high  $CO<sub>2</sub>$  adsorption of carbon nitrides is mainly due to abundant amine groups  $[34]$ . Additionally,  $CO<sub>2</sub>$  adsorption occurs on the polarised micropore edges formed by the surface roughness of graphitic carbon nitride, exposing electron-rich edges towards  $CO<sub>2</sub>$  through induced dipole-dipole interactions, while tertiary nitrogen and heptazine sites exhibit very weak or no polarisation effect on  $CO<sub>2</sub>$  [31]. When analysing the mechanism of  $CO<sub>2</sub>$  adsorption on different nitrogen functional groups, adsorption energy studies showed that quaternary nitrogen and pyrrolic nitrogen enhance surface  $CO<sub>2</sub>$  adsorption, while pyridine nitrogen enhances edge  $CO<sub>2</sub>$  adsorption [36].

We previously reported CO<sub>2</sub> adsorption on carbon foams (synthesized from sodium ethoxide) and nitrogen-doped carbon foams (ethanolamines as nitrogen sources), having hierarchical porosity with large micropore volume, resulting in remarkable surface area up to 3450 m<sup>2</sup> g<sup>-1</sup> [37,38]. We reported CO<sub>2</sub> uptake of up to 5.65 mmol g<sup>-1</sup> at 100 kPa, and 9.88 mmol  $g^{-1}$  at 0.5 MPa, and at 298 K [37], making them extremely promising adsorbents. We showed that selectivity was dependent on nitrogen content, but capacity decreased with nitrogen content due to reduced pore volume [28]. Therefore, further optimization is still required to find a balance between pore volume and nitrogen content.

The aim of this study is to gain insights into the performance of carbon foam adsorbents for CO<sub>2</sub> capture by increasing nitrogen content without destroying the carbon foam framework. This is achieved by synthesizing carbon nitride on the surface of carbon foams, via polymerisation of dicyandiamide. Furthermore, we investigate the suitability of the materials for both pre-combustion (2 MPa) and post-combustion (100 kPa) scenarios at different temperatures, under dynamic  $CO<sub>2</sub>/N<sub>2</sub>$  gas mixture conditions in a packed bed, and across multiple adsorption-desorption cycles. This approach to industrial adsorbent design promises not only to improve efficiency but also enhance sustainability, marking significant steps toward mitigation of the impending environmental crisis.

## **2. EXPERIMENTAL**

## **2.1 Synthesis of carbon nitride-coated carbon foams**

All chemicals were used as received without further purification. Microporous carbon foam (CF) was prepared via a single-step pyrolysis of sodium ethoxide (Wako Ltd., Japan) in a muffle furnace at 973 K with a ramp rate of 3 K min<sup>-1</sup> and under a flowing nitrogen atmosphere (6 L min<sup>-1</sup>). This high flow rate was necessary due to the large internal volume of the muffle furnace in order to prepare a substantial amount of CF for subsequent coating with carbon nitride. For the CF preparation, we used about 35 g of sodium ethoxide. The resulting product was crushed in a pestle and then magnetically stirred in deionised water for at least 24 hours, followed by vacuum filtration and washing until the filtrate had neutral pH, to remove soluble by-products such as sodium carbonate and sodium hydroxide [37]. The product was then dried for 24 hours at 333 K. The carbonaceous product yield was 1.95 g, making up 5.6 % of the initial mass of sodium ethoxide.

A portion of the CF of about 500 mg was then coated with carbon nitride. This was achieved via wet impregnation with dicyandiamide (DCD, Wako Ltd., Japan). DCD was dissolved in deionized water, and CF powder was added to the solution with a DCD:CF ratio of 1:2 wt/wt. The resulting dispersion was magnetically stirred at 500 rpm for either 1 hour or for 24 hours as a means to control the nitrogen content. Then the water was evaporated overnight in an oven at 333 K. The dried DCD-coated CF samples were then subjected to twostep heat treatment in a tube-furnace to polymerise the DCD into carbon nitride, first at 823 K for 4 hours (with a ramp rate of 3 K min<sup>-1</sup>), then at 973 K for 2 hours, both steps carried out

under flowing nitrogen gas at 100 ml min<sup>-1</sup>. The resulting samples were labelled as  $C_3N_4/CF-1$ and  $C_3N_4/CF-24$ , reflecting the different durations of the wet impregnation step.

# **2.2 Characterization methods**

The morphology of the samples was studied by scanning electron microscopy (SEM, SU-9000 microscope, Hitachi Ltd., Japan). The particle size distribution, based on the length of the particles observed in the SEM images, was determined using ImageJ software. It should be noted that as the particles were non-uniform, the length of each respective particle was measured and given as the size parameter. Surface chemical composition was determined under ultra-high vacuum via X-ray photoelectron spectroscopy (XPS, PHI 5000 VersaProbe-II Focus Microprobe, ULVAC-PHI Ltd., Japan). The bulk chemical composition was estimated by CHN elemental analysis (CHN Corder MT-6, Yanaco Apparatus Development Laboratory Co. Ltd., Japan). Crystallinity was investigated via powder X-ray diffraction (XRD, SmartLab diffractometer, Rigaku Ltd., Japan) and Raman microscopy with an excitation wavelength of 534 nm (inVia Raman microscope, Renishaw Ltd., Japan). Deconvolution of the Raman spectra to obtain the areas of the D and G peaks was performed using Fityk 1.3.1 software. The textural properties of the samples were evaluated from  $N_2$  adsorption isotherms measured at 77 K using a volumetric sorption analyser (Belsorp Mini-II, Microtrac Bel Ltd., Japan), and CO2 adsorption isotherms measured at 273 K using a gravimetric sorption analyser (IGA-100, Hiden Isochema Ltd., UK).

## **2.3 CO<sup>2</sup> adsorption experiments and analyses**

CO<sup>2</sup> sorption experiments were conducted at up to 2 MPa, and at various temperatures (273, 298 and 323 K) using a gravimetric sorption analyser (IGA-100, Hiden Isochema Ltd., UK) supplied with pure  $CO<sub>2</sub>$  gas (99.995 vol%, Linde Gas Ltd.) [7]. Measurements of  $CO<sub>2</sub>$ adsorption-desorption isotherms up to 100 kPa and 2 MPa were performed separately at different analyser settings. The  $CO<sub>2</sub>$  adsorption isotherms up to 100 kPa were performed twice to calculate the standard deviation. The  $CO<sub>2</sub>$  adsorption isotherms at pressures up to 2 MPa were conducted only once with highly accurate weight stability of  $\pm 0.0001$  g. Prior to each sorption measurement, the target sample was evacuated overnight to  $10^{-6}$  kPa at 423 K, using a fast response oven. Isotherms were collected whilst maintaining a pressure accuracy of  $\pm 0.02\%$ . Each point on the isotherm required around 10 minutes to stabilisation and reach equilibrium.

The temperature was controlled using a water bath to an accuracy of  $\pm 0.05$  K. Dynamic CO<sub>2</sub> adsorption was estimated via breakthrough experiments carried out at 298 K using the IGA-100 connected to a quadrupole mass spectrometer (HRP-20 QIC, Hiden Analytical Ltd.). Breakthrough curves were measured using a  $CO<sub>2</sub>$  to  $N<sub>2</sub>$  gas mixture of 15:85 vol% and a flow rate of 50 ml min<sup>-1</sup>, according to a setup illustrated in our previous study [28]. Breakthrough curves were plotted displaying  $C/C<sub>0</sub>$  versus time (*t*), where *C* it the CO<sub>2</sub> concentration at time *t* and  $C_0$  is the CO<sub>2</sub> concentration at  $t = 0$ , as determined by mass spectrometry.

The CO2/N<sup>2</sup> selectivity (*SCO2/N2*) was calculated using Ideal Adsorbed Solution Theory (IAST), based on pure-phase  $CO<sub>2</sub>$  and  $N<sub>2</sub>$  adsorption isotherms measured under the same experimental conditions [23]. Sips and Langmuir models were applied to fit the  $CO<sub>2</sub>$  and  $N<sub>2</sub>$ adsorption isotherms, respectively. The IAST  $CO<sub>2</sub>$  and  $N<sub>2</sub>$  adsorption isotherms for a respective CO2/N<sup>2</sup> gas mixture were calculated using GraphIAST software [39].

Isosteric heats of  $CO_2$  adsorption  $(\Delta H_{st})$  were calculated using the Clausius-Clapeyron equation, which describes the dependence of *ΔHs*<sup>t</sup> values on surface coverage (i.e. on the amount of  $CO<sub>2</sub>$  adsorbed) [40]. Isosteres were obtained at 273, 298 and 323 K, and the corresponding pressure values at fixed amount adsorbed were obtained from the Sips fitting results.

#### **3. RESULTS AND DISCUSSION**

#### **3.1. Characterisation of carbon foam materials**

## *3.1.1. Morphology*

The morphology of the CF,  $C_3N_4/CF-1$  and  $C_3N_4/CF-24$  samples was investigated by SEM (Figure 1). At low magnification, the characteristic three-dimensional structure of carbon foams is evident as micron-scale spheroidal cells separated by thin cell walls [28]. The similarity of the three samples confirms that coating the CF scaffold with carbon nitride does not significantly affect the macrostructure. Higher magnification reveals more notable differences between the samples. Figure 1(c) shows that some regions of CF have a degree of nanoscale roughness, potentially indicating the presence of micropores. Figure 1(f) reveals a slightly different morphology for C3N4/CF-1, potentially depicting the deposited layer of carbon nitride particles [41,42]. Meanwhile, Figure 1(i), for  $C_3N_4/CF-24$  larger particles with diameter of

several hundred nanometres are clearly observed to be adhered to the surface of the CF scaffold, also be assumed to be carbon nitride. As such the SEM results depict a clear progression between the uncoated CF sample, to the sample which underwent wet impregnation with DCD for only one hour  $(C_3N_4/CF-1)$ , to the sample which was impregnated for 24 hours  $(C_3N_4/CF-1)$ 24). The particle size distribution calculated from the low-magnification SEM images (Figure S1) using ImageJ software and presented in Figure S2 shows that most particles in all three samples were in the range of 10-60 µm, and the largest determined particles had size of about 280 µm.



**Figure 1.** SEM images of the three adsorbents: (a-c) pure carbon foam (CF); (d-f) carbon foam coated with carbon nitride via wet impregnation for 1 hour  $(C_3N_4/CF-1)$ ; and  $(g-i)$  carbon foam coated with carbon nitride via wet impregnation for 24 hours  $(C_3N_4/CF-24)$ .

## *3.1.2. Elemental composition*

The bulk chemical composition of the three adsorbents was determined by CHNO elemental combustion analysis, revealing that the CF sample has only minimal nitrogen content  $(0.3 \text{ at\%})$ , increasing to 5.3 at% for C<sub>3</sub>N<sub>4</sub>/CF-1 and to 17.0 at% for C<sub>3</sub>N<sub>4</sub>/CF-24 (Table S3). This confirms that (i) the DCD polymerisation step was successful, (ii) that coating CF with carbon nitride does indeed introduce significant amounts of nitrogen, and (iii) that the duration of the wet impregnation step has a major impact on the nitrogen content of the final product.

XPS was also performed to determine the abundance and the chemical state of nitrogen atoms in the samples. The survey spectrum contains characteristic peaks at binding energies of  $\sim$  285 eV, 400 eV and 530 eV corresponding to C1s, N1s and O1s, respectively (Figure 2a). Here, the nitrogen content of CF is negligible, in agreement with the CHNO data. The nitrogen content increases to 6.2 at% for  $C_3N_4/CF-1$ , which again is close to the CHNO result, although slightly higher. Notably, for C3N4/CF-24, the nitrogen content according to XPS is just 5.3 at%, which is significantly lower than the value of 17.0 at% obtained via combustion analysis (Table S1). This discrepancy is attributed to bulk nature of combustion analysis compared with the quasi-surface sensitive nature of XPS, in which photoelectrons can only escape from a depth of several nm within the sample [43]. As such, these results indicate that a large proportion of nitrogen atoms in C3N4/CF-24 reside within the "bulk" material. An explanation for this is that DCD penetrates further into the micropores of CF during the longer wet impregnation stage, and carbon nitride is then embedded within those pores during the heat treatment step.

To gain further insight into the chemical environment of nitrogen atoms in the adsorbents, N1s spectra were recorded and deconvoluted into four peaks. These correspond to: *sp<sup>2</sup>* hybridized pyridinic nitrogen species (C=N-C, at 398.6 eV); tertiary nitrogen species or amines  $(C-(N)_3$  or -NH<sub>2</sub>, at 400.3 eV); hydrogenated pyridinic nitrogen species (C-NH-C, at ~401.5) eV); and oxidized nitrogen species (N-O, at 403.1 eV) (Figure 2b, Table S2). The ratio of different nitrogen contributions for both C<sub>3</sub>N<sub>4</sub>/CF-1 and C<sub>3</sub>N<sub>4</sub>/CF-24 are remarkably similar, with the highest abundance for pyridinic nitrogen, followed by tertiary / amine species and then hydrogenated pyridinic species and finally a small proportion of oxides. These proportions are quite typical of carbon nitride if the tri-s-triazine-type structure is considered. Deconvolution of C1s and O1s spectra was also performed (Figure S3, Table S3 and Table S4) [44–47].

Overall, the elemental analysis indicates that carbon nitride is successfully coated onto the surface of carbon foams using this method. As outlined in the introduction, this is expected to be beneficial for  $CO<sub>2</sub>$  adsorption via the introduction of Lewis base sites. However, it is also hinted that the micropores could be filled with carbon nitride, which may be detrimental to adsorption.



**Figure 2.** XPS spectra of the adsorbents: (a) survey spectrum; (b) N1s region.

# *3.1.3. Crystalline structure*

The crystallinity of the adsorbents was assessed via XRD (Figure 3a). The XRD spectra all display a broad 2 $\theta$  peak in the range of 15-30°, with a maximum at ~22°. This corresponds to the (002) plane of graphitic carbon with an interlayer distance of 0.4 nm indicating a relatively amorphous structure (i.e. significantly larger than the 0.36 nm of highly oriented pyrolytic graphite) [28]. Notably, a prominent shoulder is observed at  $27.4^{\circ}$  in the C<sub>3</sub>N<sub>4</sub>/CF-24 sample with a high nitrogen content of 17 at%. In contrast, this shoulder is absent in the C3N4/CF-1 sample, which has a lower carbon nitride content with 5-6 at% of nitrogen only. This corresponds to the (002) plane of graphitic carbon nitride, with a lattice parameter of 0.167 nm and an interlayer distance between triazine sheets of 0.32 nm [30,48]. The prominence of this shoulder in C3N4/CF-24 confirms that longer wet impregnation time results in the formation of more carbon nitride, in agreement with SEM and elemental analysis. Additionally, a small peak at  $\sim$  44 $\degree$  is attributed to the (100) plane of graphitic carbon [37]. Overall, the peaks are not particularly sharp, indicating that both the CF scaffold and the carbon nitride coating are relatively amorphous materials.

The degree of crystallinity was also assessed via Raman spectroscopy, by calculating the ratio of the intensities  $(I_D/I_G)$  and the peak areas  $(A_D/A_G)$  of the D and G bands at 1338 cm<sup>-1</sup> and  $\sim$  1580 cm<sup>-1</sup>, respectively (Figure 3b, Table S5). The D peak is indicative of breathing vibrations of  $sp<sup>2</sup>$  aromatic rings in carbon materials, and the G peak represents stretching vibrations of these rings [49]. Both the  $I_D/I_G$  and  $A_D/A_G$  ratios increase significantly from CF to  $C_3N_4/CF-1$ to C3N4/CF-24. This signifies greater degree of disorder in the carbon structure after coating with carbon nitride, attributed to the increased presence of triazine aromatic rings. The 2D peak is generally associated with in-plane vibrational modes of the  $sp<sup>2</sup>$ -bonded carbon and nitrogen atoms in the two-dimensional lattice, and the intensity, shape, and position are sensitive to the degree of graphitization, the presence of defects, and the stacking arrangement of carbon and nitrogen layers in the material [50]. In both CF and  $C_3N_4/CF-1$  the 2D peak is relatively featureless, but a more pronounced fine structure at  $2680 \text{ cm}^{-1}$  is observed for the C<sub>3</sub>N<sub>4</sub>/CF-24 sample. This may be indicative of higher crystallinity in that sample, suggesting that graphitic carbon nitride  $(g-C_3N_4)$  may have been synthesized in this case. An excitation wavelength of 534 nm was used, so the number of layers is estimated to be less than five [50]. The formation of this graphitic phase could be due to confinement in micropores during polymerisation.



**Figure 3.** a) XRD patterns and b) Raman spectra of the three adsorbents.

# *3.1.4. Textural properties*

Isotherms were measured in  $N_2$  and  $CO_2$  to assess the porosities and surface areas of the adsorbents. Micropores are defined as having a pore diameter below 2 nm, and sometimes a further distinction into supermicropores (ranging from 0.7 to 2 nm) and ultramicropores (below 0.7 nm) is made [51]. Meanwhile, mesopores are defined as having pore diameters between 2

and 50 nm. The  $N_2$  adsorption isotherms measured at 77 K (Figure 4a) can all be classified as Type IV. A distinct knee at low relative pressures  $(P/P<sub>s</sub> < 0.01$ , where  $P<sub>s</sub>$  is the saturation pressure) indicates micropore filling, whilst the H4-type hysteresis loop at  $P/P_s > 0.4$  is characteristic of capillary condensation in mesopores [23]. Similarly, in the case of  $CO<sub>2</sub>$ adsorption isotherms measured at 273 K (Figure 4b) micropore filling with  $CO_2$  gas at  $P/P_s$ values of up to  $\sim 0.03$  is also evident [52].

The ultramicropore volume was determined using the Dubinin-Radushkevich (DR) adsorption model applied to the  $CO<sub>2</sub>$  adsorption isotherms [53], while the micropore volume (*Vmicro*) was obtained using the Lippens and de Boer *Vads*-*t* plot models, applied to the N<sup>2</sup> adsorption isotherms [54]. All pore parameters determined from the adsorption isotherms are listed in Table 1. Meanwhile, the pore size distribution in the range 0.36 to 30 nm was obtained by applying the non-local density functional theory (NLDFT) adsorption model to the combined adsorption isotherms(Figure 4c, Figure S4a and Figure S4b). The results are in broad agreement with each other.

CF exhibits remarkable surface area  $(2537 \text{ m}^2 \text{ g}^{-1})$ , as well as the highest ultramicropore volume, micropore volume, and mesopore volume, translating into the largest total pore volume. Meanwhile, for C3N4/CF-1 there is a moderate decrease in the surface area and total pore volume, but only a slight decrease in ultramicropore volume. Finally, for C3N4/CF-24 there is a significant decrease in surface area, total pore volume, and ultramicropore volume. This further supports the hypothesis that wet impregnation for 24 h reduces porosity and surface area by blocking or filling micropores with carbon nitride.

Samples	$S_{BET}^a$	$V_{\text{ultra}}^{\text{b}}$	$V_{\text{micro}}^{\text{c}}$ $V_{\text{meso}}^{\text{e}}$	$V_{\rm tot}^{\rm d}$	$dl^f$	$d2^f$	$d3^f$	$d4^f$
				$\text{cm}^3 \text{ g}^{-1}$	nm	nm	nm	nm
<b>CF</b>	2537	0.4617		1.3407 0.2664 1.6071	0.40		$0.63$ 1.19 2.46	
$C_3N_4/CF-1$	2127	0.4495		1.1011  0.1940  1.2951	0.41	0.60		$1.21 \quad 2.46$
$C_3N_4/CF-24$	1263	0.2774		0.6869 0.1116 0.7985	0.41	0.64		$1.33 \quad 2.46$

**Table 1.** Specific surface area pore parameters obtained from combined NLDFT analysis of the CO<sup>2</sup> and N2 adsorption isotherms measured at 273 K and 77 K, respectively.

<sup>*a*</sup>**BET** applied to the  $N_2$  *adsorption isotherm: specific surface area (S<sub>BET</sub>)* 

 $b$ <sup>*b*</sup>DR applied to the CO<sub>2</sub> adsorption isotherms: ultramicropore volume (V<sub>ultra</sub>)

*cL ippens and de Boer Vads-t plot applied to the N<sup>2</sup> adsorption isotherm: micropore volume (Vmicro)* 

<sup>*d*</sup>*Gurvitch applied to the N<sub>2</sub> <i>adsorption isotherm: total pore volume* ( $V_{tot}$ ) *at p/p<sub>s</sub>* = 0.99

$$
e_{Wmeso} = V_{tot} - V_{micro}
$$

*<sup>f</sup>NLDFT applied to CO<sup>2</sup> and N<sup>2</sup> isotherms: ultramicropore (d1, d2), micropore (d3) and mesopore (d4) diameters*



**Figure 4.** a)  $N_2$  adsorption isotherms for the three adsorbents measured at 77 K. b)  $CO_2$ adsorption isotherms measured at 273 K. c) Pore size distribution as determined by NLDFT.

## **3.2. CO<sup>2</sup> capture performance**

#### *3.2.1. Post-combustion capture*

 $CO<sub>2</sub>$  adsorption-desorption isotherms for pressures up to 100 kPa at three temperatures are shown in Figure 5a-c, corresponding to post-combustion capture conditions. The amount of  $CO<sub>2</sub>$  adsorbed increases with pressure, and the highest  $CO<sub>2</sub>$  uptake occurs at the lowest temperature, as expected. The desorption isotherms closely follow the adsorption isotherms and are therefore not clearly visible in these graphs, but this indicates that adsorption is highly reversible. Numerical values for the  $CO<sub>2</sub>$  uptake ( $\eta_{CO2}$ ) at different temperatures and their standard deviations, ranging up to  $\pm 0.05$  are given in Table 2.

Under these conditions,  $C_3N_4/CF-1$  exhibits the highest  $CO_2$  uptake (i.e. 5.24 mmol  $g^{-1}$  at 273 K), followed by CF  $(5.09 \text{ mmol g}^{-1})$  and then C<sub>3</sub>N<sub>4</sub>/CF-24  $(2.83 \text{ mmol g}^{-1})$ . To help understand this trend, it should be noted that ultramicropores are known to enhance  $CO<sub>2</sub>$ adsorption, due to overlapping dipole moments of the  $CO<sub>2</sub>$  molecules and pore walls, leading to more efficient packing [55]. Furthermore, nitrogen functionalities can serve as Lewis base sites favourable for  $CO_2$  adsorption via weak chemisorption [26]. Analysis of  $CO_2$  adsorption mechanism, investigating adsorption energy of different nitrogen functionalities with molecules  $CO_2$  ( $E_{ad}$ ) showed that quaternary nitrogen ( $E_{ad}$  = -14.88 kJ mol<sup>-1</sup>) and pyrrole nitrogen ( $E_{ad}$  =  $-17.47$  kJ mol<sup>-1</sup>) enhance the surface CO<sub>2</sub> adsorption, whereas pyridine nitrogen ( $E_{ad} = -22.57$ ) kJ mol<sup>-1</sup>) enhances the edge  $CO_2$  adsorption [36]. In this study, the XPS results confirmed that carbon nitride was the major nitrogen coating the carbon foam surface, which is composed of pyridinic nitrogen, followed by tertiary/amine species, then hydrogenated pyridinic species and small amount of oxidized nitrogen (Figure 2, Table S2). Therefore, the trend of  $CO<sub>2</sub>$  uptake shown in Figure 5 is attributed to the fact that (i)  $C_3N_4/CF-1$  combines large ultramicropore volume with an abundance of nitrogen sites, whilst (ii) CF only has large ultramicropore volume (and no nitrogen sites), and (iii) that  $C_3N_4/CF-24$  has dramatically reduced pore volume despite its high nitrogen content. This underscores the significance of nitrogen functionality in combination with the presence of micropores for post-combustion capture.



**Figure 5**. CO<sub>2</sub> adsorption isotherms measured at 100 kPa and at: a) 273 K, b) 298 K, and c) 323 K. Bold symbols correspond to adsorption isotherms and empty symbols correspond to desorption isotherms. Desorption isotherms are not clearly visible as they closely follow the adsorption isotherms.

Table 2. CO<sub>2</sub> uptake of the carbon foam samples at temperatures of 273, 298 and 323 K, and at pressures of 100 kPa and 2 MPa.

Sample	$\eta_{CO2}$ at 273 K			$\eta_{CO2}$ at 298 K			$\eta_{CO2}$ at 323 K		
	(mmol $g^{-1}$ )		(mmol $g^{-1}$ )			(mmol $g^{-1}$ )			
	100 kPa	$2.0$ MPa		100 kPa	$2.0 \text{ MPa}$		100 kPa	$2.0$ MPa	
CF	$5.09 \pm 0.03$	25.52		$2.90 \pm 0.04$	18.44		$1.70 \pm 0.04$	14.09	
$C_3N_4$ /CF-1	$5.24 \pm 0.05$	21.84		$3.16\pm0.01$	15.70		$1.97 \pm 0.02$	12.04	
$C_3N_4$ /CF-24	$2.83 \pm 0.03$	11.92		$1.57 \pm 0.04$	8.19		$0.99 \pm 0.02$	6.40	

## *3.2.2. Pre-combustion capture*

Meanwhile,  $CO<sub>2</sub>$  adsorption-desorption isotherms for pressures up to 2 MPa are shown in Figure 6a-c, corresponding to pre-combustion capture conditions [56]. Notably, in contrast with the lower pressure measurements, CF now exhibits the highest  $CO<sub>2</sub>$  uptake, adsorbing up to a maximum of 25.52 mmol  $g^{-1}$  at 273 K (see Table 2). This is comparable with the highest reported uptake values in the literature under similar conditions. Meanwhile,  $C_3N_4/CF-1$  has slightly lower uptake (21.84 mmol  $g^{-1}$ ), and C<sub>3</sub>N<sub>4</sub>/CF-24 has significantly lower CO<sub>2</sub> uptake  $(11.92 \text{ mmol g}^{-1} \text{ g}).$ 

In this case (i.e. higher pressure), the trend can be attributed to an increased presence of supermicropores (0.7 to 2.0 nm) and small mesopores (2.0 to 3.0 nm) in CF (Figure 4c), which tend to become filled at higher pressures, and do not take part in adsorption at lower pressures [68]. Indeed, it is known that pores up to 10 nm are completely filled with  $CO<sub>2</sub>$  at pressures up to the vapour saturation pressure of  $CO<sub>2</sub>$ , and pores smaller than 3 nm should be filled at pressures up to  $P/P_s \sim 0.58$  (i.e. 2.0 MPa at 273 K) [57]. Figure S5 shows the CO<sub>2</sub> adsorption capacity at 2 MPa and 273 K, depending on different parameters, including nitrogen content (Figure S5a), *SBET* (Figure S5b), *Vultra* (Figure S5c), *Vmicro* (Figure S5d), *Vmeso* (Figure S5e) and *V*<sub>tot</sub> (Figure S5f). All trends, except for *V*<sup>*ultra* ( $R^2 = 0.8994$ ) and *V*<sup>*meso* ( $R^2 = 0.9270$ ), show good</sup></sup> linear fits with correlation coefficients higher than  $0.9800$ . The best fit for  $CO<sub>2</sub>$  uptake was found with nitrogen content  $(R^2 = 0.9991)$ . However, since nitrogen content is directly related to  $S_{BET}$  (Figure S5g), it can be concluded that  $CO<sub>2</sub>$  uptakes are primarily determined by the specific surface area, which is influenced by the volume of micropores and mesopores (i.e. total pore volume *Vtot*). Thus, CF, with the highest *SBET* value and *Vtot* (Table 1), showed the highest  $CO<sub>2</sub>$  uptake at 2 MPa. Conversely, the C<sub>3</sub>N<sub>4</sub>/CF-24, with the lowest *S<sub>BET</sub>* value and  $V<sub>tot</sub>$  among the studied materials, adsorbed the least  $CO<sub>2</sub>$  under the same pressure and temperature conditions. This conclusion aligns well with previous studies [58,59]. Another explanation of CO<sup>2</sup> adsorption can be that in the case of adsorbents with larger adsorption energy (due to the introduction of Lewis base sites), the increase in  $CO<sub>2</sub>$  uptake (d $\eta$ /dP) at low partial pressure is relatively fast compared to materials with lower adsorption energy, the result being that saturation can occur at lower partial pressure. Thus  $C_3N_4/CF-1$  may display higher uptake than CF at 100 kPa due to the presence of nitrogen, but lower uptake at 2 MPa due to lower total adsorption capacity. This implies that for  $CO<sub>2</sub>$  uptake at higher pressures (relevant to precombustion capture), nitrogen-doping has minimal influence on adsorption capacity, with porosity being the dominant factor.

Meanwhile, the Sips adsorption model was used to determine the homogeneity of the sample surfaces [60], with Sips fits in excellent agreement with the corresponding adsorption isotherms (Figure 6a-c, Figure S6). Analysis of the fitting data (Table S6) reveals Freundlich exponent values of  $n \le 1$ , indicating heterogeneous adsorption. Notably,  $C_3N_4/CF-1$  and C3N4/CF-24 have a greater degree of heterogeneity than CF. This is as expected since two different materials (carbon foam and carbon nitride) are present in the same adsorbent which have presumably distinct adsorption properties.



**Figure 6.** CO<sub>2</sub> adsorption isotherms measured at 2 MPa and at: a) 273 K, b) 298 K and c) 323 K. Dotted lines correspond to the Sips fittings.

## *3.2.3. Comparison with literature*

To add context to the CO<sub>2</sub> adsorption capacities of carbon foam samples, the properties are herein compared with data reported for similar materials and conditions in the literature (Table 3). Differences in experimental conditions, such as temperature and pressure, as well as variations in the porous and chemical structure of the carbon materials, significantly impact reported CO<sup>2</sup> sorption capacities. As discussed above, adsorption capacity increases with higher pressure and lower temperature. Additionally, the specific surface area, porosity and surface chemistry of the carbon materials also play critical roles. Based on this, the uptake values and  $CO<sub>2</sub>/N<sub>2</sub>$  selectivity of the carbon foam materials presented here are comparable to reported values of the best carbon materials in the comparable study in the literature (Max.  $\eta_{CO2}$ ). Specifically, different pore parameters (*SBET*, *Vmicro*, *Vmeso*, *Vtot*) and the presence or absence of nitrogen content under similar pressure (100 kPa and 2 MPa) and temperature (273 K and 298 K) are focused on. In this comparison, differences are accounted for by normalising the  $CO<sub>2</sub>$ uptake to the pressure and temperature conditions applied in this work. This approach allows for a clearer assessment of the performance of the CF and C3N4-coated carbon foam samples.

Overall, nitrogen-doped carbons in Table 3 have predominantly been measured at low atmospheric pressures due to their higher selectivity in that region (as discussed in the next section) [25,31,35,40,61–63]. Especially, polyethyleneimine-functionalized carbon nitride exhibited extremely high  $CO<sub>2</sub>/N<sub>2</sub>$  selectivity ( $> 6500$ ) due to strong reactivity of amine groups with  $CO<sub>2</sub>$  [35]. In contrast, pure carbon materials tend to be measured at higher pressure, where porosity dominate over adsorption energy [6–8,64–67]. Some carbon materials exhibited high adsorption capacity due to their high specific surface areas in addition to the presence of Lewis base centres that attract  $CO<sub>2</sub>$  [28,58,68–74]. In particular, amine-functionalized porous carbon [74] exhibited exceptionally high  $CO<sub>2</sub>$  uptake of ~25.94 mmol g<sup>-1</sup> at 2 MPa and 298 K, preferably attributed to high microporosity. Other porous carbons [17,32–34,59,75] displayed varying CO2 uptake based on their micropore and total pore volumes.

**Table 3.** Comparison of the CO<sub>2</sub> adsorption capacities for various porous carbon in the literature, with the carbon foam materials presented in this study.

Sample	$S_{BET}$ $(m^2 g^{-1})$	V <sub>micro</sub>	$V_{meso}$	$V_{tot}$ $\text{ (cm}^3 \text{ g}^{-1}) \text{ (cm}^3 \text{ g}^{-1}) \text{ (cm}^3 \text{ g}^{-1})$	N content	T (K)	P (MPa)	Max. $ηCO2$ (mmol $g^{-1}$ )	IAST $S_{CO2/N2}$ $(CO_2:N_2)$	Study
Carbon foam (CF)	2537	0.46	0.27	1.61		273	0.1	5.1	$\overline{\phantom{0}}$	This
						273	2.0	25.5	$\overline{\phantom{0}}$	study
						298	0.1	2.9	14(15/85)	
						298	2.0	18.4	$\overline{\phantom{0}}$	
Carbon nitride-coated	2127	0.45	0.19	1.30	5.3 at%	273	0.1	5.2	$\overline{\phantom{0}}$	This
carbon foam						273	2.0	21.8	$\overline{\phantom{0}}$	study
						298	0.1	3.2	21(15/85)	
						298	2.0	15.7	$\overline{\phantom{a}}$	
Activated carbon	3575	1.22	0.61	1.83		298	0.1	~2.5	$\overline{\phantom{a}}$	[6]

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# *3.2.4. Ideal Adsorbed Solution Theory and CO2/N<sup>2</sup> Selectivity*

The selectivity towards either CO<sub>2</sub> or N<sub>2</sub> adsorption (*S<sub>CO2/N2</sub>*) is a crucial factor in designing industrial adsorption processes. Here, a practical scenario is simulated using the Ideal Adsorbed Solution Theory (IAST), with a post-combustion flue gas composition of 15 vol%  $CO<sub>2</sub>$  and 85 vol%  $N_2$  at 298 K [23]. The high degree of accuracy of the measurements is confirmed by the excellent fits obtained for both pure  $CO<sub>2</sub>$  and  $N<sub>2</sub>$  adsorption isotherms, using the Sips adsorption model for  $CO_2$  [76] and the Langmuir model for N<sub>2</sub> [37] (Figure 7a).

The values for selectivity obtained at 5 kPa are: 17.3 for CF, 15.6 for C<sub>3</sub>N<sub>4</sub>/CF-24, and 20.0 for C3N4/CF-1 (Figure 7b). This trend clearly aligns with the nitrogen content and amount of ultramicropores of the samples:  $C_3N_4/CF-1$  exhibits high  $V_{ultra}$  (0.45 cm<sup>3</sup> g<sup>-1</sup>) and high nitrogen content (5.3 at%), thus demonstrating the highest selectivity, while CF has with high *Vultra* (0.46  $\text{cm}^3 \text{ g}^{-1}$ ) but negligible nitrogen content has middle selectivity, and C<sub>3</sub>N<sub>4</sub>/CF-24 with the highest nitrogen content (17.0 at%) and the lowest  $V_{ultra}$  (0.28 cm<sup>3</sup> g<sup>-1</sup>) results in the lowest selectivity. This trend indicates strong binding between  $CO<sub>2</sub>$  molecules and nitrogen functionalities, in addition to CO<sup>2</sup> physically adsorbing in ultramicropores through van der Waals forces. Meanwhile, the selectivity decreases with increasing pressure for CF, which is attributed to competitive adsorption: at higher pressure, more molecules of all components become more available for adsorption on a limited number of ultramicropore sites, regardless of selectivity. Conversely, the selectivity slightly increases for  $C_3N_4$ -coated carbon foams with pressure increase, showing a more intense increase at the beginning of the sorption process. This phenomenon can be explained by  $CO<sub>2</sub>$  having a preference over N<sub>2</sub> for adsorption by nitrogen functionalities due to the more vital binding interaction ( $E_{ad} > -15$  kJ mol<sup>-1</sup>) compared to the weaker interaction with N<sub>2</sub> (E<sub>ad</sub> < -13 kJ mol<sup>-1</sup>) [36,77]. At 100 kPa selectivities of 13.9, 18.4 and 21.2 are obtained for CF,  $C_3N_4/CF-24$  and  $C_3N_4/CF-1$ , respectively. Overall, these values are competitive with published results for porous carbons measured under similar conditions

[68,70,71] (Table 3), highlighting the potential of carbon nitride-coated carbon foams to be applied in industrial gas separation processes.

Following the principles of IAST, the  $CO<sub>2</sub>$  and  $N<sub>2</sub>$  adsorption isotherms were calculated for a gas mixture comprising 15 vol%  $CO<sub>2</sub>$  and 85 vol% N<sub>2</sub>, using GraphIAST software [39] (Figure 7c). Notably,  $C_3N_4/CF-1$  exhibits high  $CO_2$  uptake of 0.81 mmol  $g^{-1}$ , surpassing that of CF (0.72 mmol  $g^{-1}$ ). In contrast, C<sub>3</sub>N<sub>4</sub>/CF-24 displays the lowest uptake (0.41 mmol  $g^{-1}$ ). This pronounced disparity underlines the critical importance of selecting an optimal amount of carbon nitride relative to the porous carbon foam to achieve the highest selectivity. The properties must be finely balanced, considering not only the carbon nitride content, but also the micropore volume since both factors significantly influence the overall adsorption performance and selectivity.



**Figure 7.**  $CO_2/N_2$  selectivity: a) Experimental  $CO_2$  and  $N_2$  adsorption isotherms fitted with the Sips and Langmuir models; b)  $CO<sub>2</sub>/N<sub>2</sub>$  selectivity; and c)  $CO<sub>2</sub>$  and  $N<sub>2</sub>$  adsorption isotherms calculated for the 15 vol%  $CO<sub>2</sub> - 85$  vol%  $N<sub>2</sub>$  gas mixture using IAST. Bold symbols represent

 $CO<sub>2</sub>$  adsorption isotherms, empty symbols represent N<sub>2</sub> adsorption isotherms, dotted lines display Sips fitting and solid lines represent Langmuir fitting.

## *3.2.5. Breakthrough experiments*

Experimental dynamic breakthrough curves were obtained at 298 K and 100 kPa (Figure 8a-c), using a 15 vol%  $CO<sub>2</sub>$  - 85 vol%  $N<sub>2</sub>$  gas mixture to simulate post-combustion flue gas. The resulting dynamic CO<sub>2</sub> uptake values were 0.35, 0.54 and 0.44 mmol  $g^{-1}$  for CF, C<sub>3</sub>N<sub>4</sub>/CF-1 and C3N4/CF-24, respectively. Both nitrogen-containing samples exhibited better performance than pure CF, as expected in this pressure regime, as outlined above. The bestperforming sample was  $C_3N_4/CF-1$ , attributed to the combination of suitable porosity and high nitrogen content. This trend is consistent with the calculations obtained via IAST, however the experimental adsorption values are slightly lower (see Figure 7c). This may be attributed to the small sample size used here, resulting in a relatively short length of the packed bed, and thus there may be insufficient time to reach equilibrium before breakthrough is observed in this case. The values are compared with the literature in Table 4.

Meanwhile, the breakthrough time ( $t_b$ ) recorded at  $C/C<sub>o</sub> = 0.05$  was  $\sim$ 1.25 mins for all three samples. These breakthrough times are rather short, but this is again attributed to the relatively small sample size used in this case (several tens of milligrams), which was unavoidable due sample synthesis scale limitations. In other studies reporting longer breakthrough times, gramscale samples were used [78–80]. Recalculating an equivalent breakthrough time for a hypothetical packed bed with 1 g of the three carbon foam adsorbents results in values ranging from 45.4 to 75.3 min, which are comparable to values reported in the literature [81,82]. Repeating these results with gram-scale samples will be imperative for verification of these breakthrough results, so scale-up of carbon foam synthesis will be the subject of future studies.



**Figure 8**. Breakthrough curves for a 15  $CO<sub>2</sub>$  vol% - 85 vol%  $N<sub>2</sub>$  gas mixture for: a) CF, b)  $C_3N_4/CF-1$  and c)  $C_3N_4/CF-24$ .

Sample	$S_{BET}$ $(m^2 g^{-1})$	Temperature (K)	Gas mixture (CO <sub>2</sub> /N <sub>2</sub> vol%)	Flow rate $\text{ (ml min}^{-1})$	$CO2$ uptake (mmol $g^{-1}$ )	<b>Breakthrough</b> time (min $g^{-1}$ )	Study
Carbon foam	2537	298	15/85	50	0.44	75.3	This study
Carbon nitride-coated carbon foam	2127	298	15/85	50	0.54	49	This study
Activated 3D-ordered micromesoporous carbon	1462	298	15/85	50	0.29	49.1	[8]
Activated carbon	1922	303	20/80 20/80	50 70	1.31 1.20	3.2 2.2	$[78]$
Nitrogen-doped carbon foam	1064	298	15/85	50	0.84	20.2	$[28]$
Nitrogen-doped activated carbon	1495	298	15/85	50	0.99	10.6	[69]

Table 4. Comparison of dynamic CO<sub>2</sub> uptake of the carbon foam materials with literature data.

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# *3.2.6. Isosteric heats of adsorption*

The isosteric heats of  $CO_2$  adsorption ( $\Delta H_{st}$ ) were determined from adsorption isotherms recorded at 273 K, 298 K, and 323 K and at pressures up to 2 MPa, employing Clausius-Clapeyron theory [84]. The isosteric heats serve as vital indicators of strength of interaction between  $CO_2$  molecules and the adsorbent surface. In general,  $\Delta H_{st}$  values below ~40 kJ mol<sup>-1</sup> signify physisorption, whereas values above  $\sim 80$  kJ mol<sup>-1</sup> indicate chemisorption [85]. Lower isosteric heats are generally more favorable for adsorbent regeneration.

Isosteric heats can be calculated by plotting plotting *ln(p)* versus *1/T* at fixed adsorbed amount (i.e. under isosteric conditions). Here, this was performed from 0.5 to 14 mmol  $g^{-1}$ (Figure S7), resulting in isosteric heats ranging from 19 to 30  $kJ$  mol<sup>-1</sup>, indicating physical adsorption (Figure 9). In all three samples,  $\Delta H_{st}$  increases substantially at lower values of CO<sub>2</sub> adsorption  $(\eta)$ , which has also been reported elsewhere [84,86,87]. One explanation for this is that at lower values of  $\eta$ , adsorbate molecules are more likely to interact with the most energetically favorable sites on the adsorbent surface, leading to stronger binding. As more adsorbate molecules occupy the surface, the adsorbate binds to the remaining less favorable sites, leading to weaker binding (i.e. lower isosteric heat of adsorption). An alternative explanation is that this is simply an artifact of the limitations of the Sips model as  $\eta$  approaches zero (i.e. the Sips model does not simplify to Henry's law in the limit of low partial pressure [28]). To account for this, the following interpretations focus on the isosteric heat at moderate values of  $\eta$  (i.e. 6 mmol g<sup>-1</sup>).

Comparing the three samples, pure CF has relatively low isosteric heat  $(\sim 19.5 \text{ kJ mol}^{-1})$ . Meanwhile,  $C_3N_4/CF-1$  has significantly increased isosteric heat  $(\sim 21.5 \text{ kJ mol}^{-1})$ . However, there is then a significant drop in the isosteric heat for  $C_3N_4/CF-24$ , to a value similar to that of pure CF  $(-19.5 \text{ kJ mol}^{-1})$ . An explanation for this involves the combined effects of enhanced gas-surface interactions within micropores and increased surface interactions due to the introduction of Lewis base sites. Pure CF has a certain isosteric heat due to the presence of micropores, into which  $CO<sub>2</sub>$  molecules can enter and experience stronger binding by interacting with multiple surfaces simultaneously. Adding a small amount of carbon nitride (as in C<sub>3</sub>N<sub>4</sub>/CF-1) retains access to these micropores, but also introduces Lewis base sites further increasing the interaction strength with  $CO<sub>2</sub>$ . Further increasing the amount of carbon nitride decreases the isosteric heat despite the larger nitrogen content. This is attributed to the blocking of micropores, thus preventing enhanced gas-surface interactions with  $CO<sub>2</sub>$  in the micropores. The isosteric heats of the studied carbon foam samples are comparable with reported values for other porous carbons [25,61,88], but lower than some reports for nitrogen-doped carbons [74,82].



**Figure 9.** Isosteric heats of CO<sub>2</sub> adsorption as function of adsorption capacity.

## *3.2.7. Regenerative capability of the adsorbents*

Finally, the regenerative performances of CF and C3N4/CF-1 were evaluated over 15 adsorption-desorption cycles conducted at 298 K and 100 kPa (Figure 10). Overall, the samples displayed remarkable stability, but there are subtle differences between the compared samples. For pure CF a slight decrease in the maximum amount adsorbed is observed after the first cycle (Figure 10a), which could be attributed to pore blocking, e.g. by residual  $CO<sub>2</sub>$  in ultramicropores. In contrast, the maximum amount adsorbed for  $C_3N_4/CF-1$  remains constant, but the residual amount adsorbed increases slightly over the first six cycles (Figure 10b), which could be attributed to strong binding between CO<sup>2</sup> molecules and nitrogen groups on the carbon surface. These findings highlight the interplay between pore structure and surface chemistry on the regenerative behaviour of adsorbent. However, these minor changes in adsorption are small

compared to the total amount adsorbed and are not expected to significantly affect industrial application of these materials. When comparing the regenerative ability of CF and  $C_3N_4/CF-1$ with commercial activated carbon [89], both materials show robust regeneration capabilities. However, carbon foam and carbon nitride-coated carbon foams offer distinct advantages due to their higher specific surface area and the presence of Lewis base sites. These attributes enhance  $CO<sub>2</sub>$  uptake and  $CO<sub>2</sub>/N<sub>2</sub>$  selectivity compared to commercial activated carbons.

On the other hand, it should be noted that scaling up the synthesis of both pure carbon foams and carbon nitride-coated carbon foams presents significant challenges for industrial applications. These include (i) optimization of the synthesis parameters, i.e. temperature, heating rate, time, precursor concentration, inert atmosphere etc. to maintain the carbon foam properties observed at the laboratory scale, (ii) achieving uniform coating of carbon foam with carbon nitride to increase a large active surface for  $CO<sub>2</sub>$ , (iii) handling of hazardous chemicals and safety issues, (iv) quality control measurements to ensure the reproducibility of the carbon foam properties, and (v) managing the material coasts. Solutions for these challenges include performing systematic studies to determine the optimal conditions for large-scale synthesis and using pilot-scale reactors to refine these parameters before full-scale production, ensuring consistency and reproducibility; using chemical vapor deposition (CVD) or atomic layer deposition (ALD) methods to achieve uniform coating with carbon nitride; implementing safety training programs and enforcing to strict operational guidelines to minimize risks associated with hazardous chemicals used in the synthesis process; verifying and maintaining the desired porous and mechanical properties using reliable quality control measures; and optimizing resource utilization, and developing recycling strategies for by-products to reduce overall production expenses.



**Figure 10.** CO<sub>2</sub> adsorption-desorption cycling at 298 K and a pressure range of 0-100 kPa for a) CF, and b)  $C_3N_4/CF-1$  adsorbents.

## **4. Conclusions**

In this comprehensive study, hierarchically porous nitrogen-doped carbon foam adsorbents were synthesized and characterised. Carbon foam (CF) was obtained via thermal decomposition of sodium ethoxide, exhibiting exceptional surface area  $(2537 \text{ m}^2 \text{ g}^{-1})$  and large pore volume  $(1.6 \text{ cm}^3 \text{ g}^{-1})$ , attributed to self-blowing and self-activating effects. This carbon foam was then coated with carbon nitride via wet impregnation with dicyandiamide (for either 1 or 24 hours) followed by thermal polymerisation, resulting in nitrogen contents of 5.3 at% (for  $C_3N_4/CF-1$ ) and 17.0 at% (for C<sub>3</sub>N<sub>4</sub>/CF-24). However, the pore volume decreased to 1.3 and 0.8 cm<sup>3</sup> g<sup>-1</sup>, respectively, attributed to the micropores being blocked and/or filled with carbon nitride. The three samples were investigated as adsorbents for  $CO<sub>2</sub>$  separation, and the key finding were as follows:

- At 100 kPa (relevant to post-combustion capture), coating with carbon nitride resulted in enhanced CO<sup>2</sup> uptake and selectivity compared to the uncoated carbon foam. This was attributed to a combination of the large micropore pore volume and increased isosteric heat of adsorption due to the introduction of Lewis base sites via nitrogen doping. However, higher nitrogen content resulted in lower  $CO<sub>2</sub>$  uptake due to the dramatically lower micropore volume.
- At 2 MPa (relevant to pre-combustion capture), coating with carbon nitride resulted in lower CO<sub>2</sub> uptake compared to the pure carbon foam. This was attributed to the increased importance of supermicropore and mesopore volume over nitrogen doping in this pressure regime.
- The regenerative capability of the adsorbents under pressure swing adsorption cycling displayed negligible deterioration over 15 tested cycles. This was attributed to the relatively weak adsorbate-adsorbent interactions and indicates the suitability of these unique adsorbents to be used in industrial applications.
- Furthermore, the adsorption characteristics of the materials presented in this work were competitive with the best results for carbon adsorbents reported in the literature, with a maximum adsorption capacity of  $\sim$ 25 mmol g<sup>-1</sup>.

In summary, this study offers a nuanced understanding of  $CO<sub>2</sub>$  capture strategies via the use of novel materials with tailored properties. It emphasizes the potential application of alkoxide-derived carbon foams for pre-combustion capture technologies at high pressure. Furthermore, it underscores the benefit of tailoring nitrogen content to achieve selective  $CO<sub>2</sub>$ capture in post-combustion capture scenarios. This research advances our current understanding of adsorbents for CCS, offering new options for efficient operation across a wide spectrum of pressures and temperatures.

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