A simple imaging solution for chip-scale laser cooling


AFFILIATIONS
1 SUPA and Department of Physics, University of Strathclyde, G4 ONG Glasgow, United Kingdom
2 Kelvin Nanotechnology, University of Glasgow, G12 8LS Glasgow, United Kingdom
3 Department of Physics, University of Colorado, Boulder, Colorado 80309, USA
4 National Institute of Standards and Technology, Boulder, Colorado 80305, USA
5 FEMTO-ST, CNRS, 26 Chemin de l’Epitaphe, 25030 Besançon, France

ABSTRACT
We demonstrate a simple stacked scheme that enables absorption imaging through a hole in the surface of a grating magneto-optical trap (GMOT) chip, placed immediately below a micro-fabricated vacuum cell. The imaging scheme is capable of overcoming the reduced optical access and surface scatter that is associated with this chip-scale platform while further permitting both trapping and imaging of the atoms from a single incident laser beam. The through-hole imaging is used to characterize the impact of the reduced optical overlap volume of the GMOT in the chip-scale cell, with an outlook to an optimized atom number in low volume systems.

Micro-fabricated physics packages based on the measurement of thermal atomic ensembles have been integrated in metrological instruments, ranging from magnetometers to interferometers and clocks. Most such instruments rely on spin transitions in atoms and require the presence of buffer gas mixtures or cell wall coatings to reduce the relaxation rate due to wall collisions. For clocks, the presence of these buffer gases causes temperature dependent frequency offsets and requires careful temperature stabilization to achieve good medium- and long-term stability. The use of cold atom ensembles avoids these difficulties and can result in an increased interaction time and improved absolute accuracy compared to their thermal atom counterparts.

While the transition to cold atoms offers clear advantages over thermal atom packages, the additional experimental size and complexity associated with laser cooling have limited the deployability and application range of cold atom devices. Significant efforts have been made on the miniaturization of cold atom components to facilitate portability for next-generation atomic sensors. However, the fabrication complexity of many of these components remains unfavorable for mass production, preventing their adoption in commercial applications.

Recent work has demonstrated a dramatic reduction in the cooling platform to the chip-scale by combining an anodically bonded glass-silicon-glass vapor cell with a diffractive optical element that redirects a single incident beam into the components required for laser cooling. However, such systems have demonstrated that the detection of cold atoms is made difficult by the reduced optical access of the cell and light scattering from the grating and cell surfaces. As such, the authors required adopting a non-trivial two-photon spectroscopy scheme for improved detection, greatly increasing both the size and complexity of the optical system.

In this Letter, we demonstrate a simple imaging solution for chip-scale laser cooling platforms. The stackable structure of the apparatus provides simplicity in alignment as well as enabling future scalability for device mass production. A hole is laser cut in the center of the grating chip to enable on-axis absorption imaging from the cooling beam without significantly degrading atom trapping. Although grating chips with a central hole have been used to reduce surface reflections, as a source for cold electrons, and for Zeeman slowing with an alkali and alkaline–earth metal source, the impact of the reduced grating surface area on the MOT number has not yet been quantified or used as an imaging axis. The ability to measure the trapped atom number in the chip-scale cell is demonstrated using fast imaging.
number in such a chip-scale system is used to characterize the impact of the 3 mm internal height constraint on the optical overlap volume, with an outlook to an optimized atom number.

A simplified schematic for the cooling and imaging of $^{87}$Rb is shown in Fig. 1. The incident light is derived from a single-volume Bragg-grating laser (VBG) frequency stabilized using saturated absorption spectroscopy. A double-pass acousto-optic-modulator (AOM) shifts the light frequency to be approximately 8 MHz red detuned from the 780 nm $D_2 F = 2 \rightarrow F = 3$ cycling transition, while also enabling frequency and intensity control for the imaging process. Re-pumping is achieved by modulating a free-space electro-optic-modulator (EOM) at 6.5 GHz to generate 5% sidebands on the carrier frequency. The light is then fiber coupled into a single-mode, polarization maintaining fiber and passed to the cooling platform.

From the fiber, we expand an $\approx 30$ mW beam to a $1/e^2$ radius of $\approx 1.6 \text{ cm}$ to flatten the intensity distribution at the grating surface. The trap beam is then circularly polarized with a quarter wave-plate and aligned onto the grating chip, mounted externally to the actively pumped chip-scale cell. A pair of anti-Helmholtz coils is used to produce a trapping field within the cell volume, with an axial gradient of $\approx 1.5 \text{ mT/cm (15 G/cm)}$.

The cell, shown in Fig. 1, is composed of a $3 \text{ mm}$ thick silicon wafer, sandwiched between two anodically bonded aluminosilicate glass wafers of $0.7 \text{ mm}$ thickness. The cell was fabricated with a square central region of dimensions $2.5 \times 2.5 \text{ cm}^2$ to enable cooling with a $2 \text{ cm}$ wide grating chip. The upper window of the cell is mechanically drilled with a $5 \text{ mm}$ hole to enable active pumping from an ion pump through a copper pinch-off tube, adhered to the upper cell surface. Square cavities are cut in the silicon walls to house non-evaporable getters (NEGs) for future passive pumping measurements.

The grating chip, shown in Fig. 1(a), has a $1100 \text{ nm}$ period in a tri-segment geometry. The central region of the chip is laser cut to provide a through-hole axis for absorption imaging. This central region of the grating plays a limited role in forming the trap overlap volume while also providing an unfavorable zeroth order reflection, such that its removal has a minimal impact on atom number. A two-lens imaging telescope and camera are placed behind the grating hole to detect atomic absorption from the GMOT.

While extracting atom number with the through-hole system, fluorescence measurements from the MOT loading curves were simultaneously measured using a separate detection telescope with a spatially selective focal plane (described in Ref. 25) at an angle of around $30^\circ$ to the grating surface (not shown in Fig. 1). The loading curves were used for the extraction of background pressure at the MOT location using the relation between MOT lifetime and background rubidium pressure, while also checking the validity of the through-hole measured atom number. We note that the atom number measured from fluorescence imaging at this angle well matched the atom number extracted from conventional orthogonal fluorescence imaging. Additionally, an average ratio of $1.6 \pm 0.4$ was observed between the calculated atom number from the through-hole absorption and orthogonal fluorescence during our data sets. However, the alignment of the angled fluorescence imaging axis was complicated due to the surface scatter and diffracted orders further restricting the available imaging angles and contributing to an increased noise level on the atom number extraction. The complexity in aligning the camera at a position and angle that minimizes the impact of surface scatter does not meet the needs of a simple, mass-producible device.

The experimental procedure is initiated by turning the trap coils on, followed by a $500 \text{ ms}$ loading time at $8 \text{ mW/cm}^2$ peak intensity. The $500 \text{ ms}$ load time enables resolving the vacuum pressure down to $1.4 \times 10^{-6} \text{ Pa (1.4} \times 10^{-8} \text{ mbar)}$. The trap coils are then turned off while concurrently decreasing the incident beam below saturation to around $115 \mu\text{W/cm}^2$ and bringing the frequency on resonance. This serves the dual purpose of reducing image distortion due to diffraction effects within the atom cloud while also maximizing the signal contrast. We note that the measured atom number from this method did not differ with the addition of a static magnetic field, provided from a Helmholtz pair along the imaging axis, to aid the optical pumping of the atoms. An initial image $I_1$ is taken with the MOT present for an exposure time of $25 \mu\text{s}$. We then wait $100 \mu\text{s}$ such that the trapped atoms are no longer present before taking a second image $I_2$. Finally, the trap beam is turned off with an extinction ratio of $62 \text{ dB}$ and a

![Fig. 1. Experimental set-up. CCD: charge coupled device, AHC: anti-Helmholtz coils, $\lambda/4$: quarter-wave plate. (a) Image of the grating chip with a central hole removed. (b) An on-axis, through-hole absorption image of $\approx 2 \times 10^6$ atoms within the chip-scale platform. This image was taken with a peak beam intensity of $115 \mu\text{W/cm}^2$ at zero detuning.](image-url)
In the present work, the stretched state saturation intensity \( I_{sat} = 1.67 \text{ mW/cm}^2 \) was used for calculating the trapped atom number from the fluorescence and absorption methods, as is consistent with previous publications of our group.\(^{1,11} \) Additionally, we found good agreement between the calculated atom numbers from the two imaging methods with the stretched state saturation intensity, compared to the average of all polarizations and magnetic sub-levels, \( I_{sat} = 3.57 \text{ mW/cm}^2 \). A saturation parameter, \( S = \frac{I}{I_{sat}} \), sums over the intensities of the single input trap beam and the three diffracted beams from the grating to account for the total intensity the atoms experience. This inclusion modifies \( S \) such that \( S = (1 + n \eta_1 \sec \theta) \frac{I_{sat}}{I} \approx \frac{2.4 \eta_1}{I_{sat}} \), where \( I_{sat} \) is the imaging light intensity, \( n \) is the number of diffracted first orders interacting with the atoms, \( \eta_1 \) is the efficiency of the first diffracted order, and \( \theta \) is the angle of diffraction. An example of the obtained MOT image is shown in Fig. 1(b), where \( 2 \times 10^5 \) atoms are trapped in the chip-scale cell.

Our investigation of the impact of removing the central region of the grating chip was initially carried out in a conventional glass vacuum chamber (2.5 \( \times \) 2.5 \( \times \) 10 cm\(^3\) with 1 mm thick glass walls) using fluorescence imaging, with the results shown in Fig. 2. We fabricated five identical grating chips and laser cut the central regions for a hole size ranging from 1 to 5 mm. For each subsequent measurement of the atom number, the grating chip was carefully implemented immediately below the same vacuum cell, under the same conditions as the previous grating chip. We found that a hole diameter up to 3 mm did not significantly degrade the measured atom number, shown in Fig. 2(a), due to the minimal impact that such a hole size has on the total optical overlap volume, shown in Fig. 2(b). The theoretical optical overlap volume is numerically integrated for a 2 cm beam diameter, incident upon a 1100 nm period tri-segmented grating chip with a central hole of varying diameter. As the grating hole was increased to 4 mm, the atom number decreases, reducing to the point that no MOT was detected for a 5 mm hole diameter, even with additional optimization of the MOT parameters, such as detuning and intensity. The atom number drops faster than would be expected from the decrease in the overlap volume, likely due to the additional sensitivity of the radiation pressure balance from the grating chip. This is emphasized by the red curve shown in Fig. 2(a), where the theoretically calculated overlap volume is scaled to the atom number through \( N \propto V^{1/2} \) and normalized to the measured atom number for the 1 mm hole. For a grating hole diameter of 4 mm, a factor of \(-2\) difference between the expected and measured atom number is observed. However, the increased hole diameter aids an improved numerical aperture, also plotted in Fig. 2(b) for a MOT position of 2 mm. We observe the cooling surface, such that a larger hole diameter is favorable for imaging with the small atom numbers that have been observed in passively pumped vacuum cells.\(^{25} \) Taking this into account, a 3 mm hole diameter was selected for through-hole imaging.

Once the through-hole imaging was well aligned, and in focus, the glass cell was replaced by the actively pumped chip-scale vacuum cell. The chip-scale cell was pumped down to an initial pressure of \( 10^{-3} \text{ Pa} (10^{-8} \text{ mbar}) \), measured using an ion pump. The validity of the ion pump reading was later verified with the pressure calculated from MOT loading curves. Following pump down, a resistively heated dispenser within the larger vacuum chamber was used to provide a moderate rubidium density. With the grating overlap volume aligned within the chip-scale cell, an image of the cold atoms was extracted from the through-hole scheme, highlighted in Fig. 1. The initial atom number measurement yielded a total of \( 2 \times 10^5 \) atoms, which was an order of magnitude lower than what had been observed for the glass cell.

To investigate the cause of the reduced atom number, the diameter of the incident cooling light onto the grating surface, \( d \), was reduced while measuring the trapped atom number for both the glass and chip-scale cells. This measurement provides an insight to the impact of the reduced vacuum volume of the chip-scale cell on the grating chip’s optical overlap volume and, therefore, trapped atom number. During this process, a comparable background vapor density of \( \approx 3 \times 10^4 \text{ cm}^{-3} \) and a total pressure of \( \approx 3 \times 10^{-5} \text{ Pa} \) \((\approx 3 \times 10^{-7} \text{ mbar})\) were maintained in both vacuum systems. The resulting data set is shown in Fig. 3(a) in blue and red for the glass and chip-scale cells, respectively.

At the largest values of \( d \), an order of magnitude difference in the atom number is observed between the glass and chip-scale cell, with the glass cell data reaching a maximum around \( 10^6 \) atoms, in line with previous atom numbers measured with a similar incident intensity.\(^{9} \) Concurrently, the red data set extracted from the chip-scale cell reaches a maximum around \( 10^5 \) atoms. When \( d \) is reduced from this maximum atom number, there is initially no impact on the optical overlap volume, since the majority of the overlap volume is outside the cell’s internal thickness and, therefore, cannot play a role in the cooling process. As \( d \) is decreased below \( \approx 17 \) mm, the overlap volume is
The impact of the reduced optical overlap volume is emphasized by the theoretical atom number expected from the grating MOT as a function of the incident beam diameter, shown with solid curves in Fig. 3(a). This atom number, \( N \), is derived from a numerical integration of the optical overlap volume from the grating chip as a function of \( d \). The normalized theoretical atom number is pinned to the maximum measured atom number for the glass cell. The red line shows an overlap volume that is restricted to a 3 mm height due to the vacuum volume of the chip-scale cell. The dashed line represents a \( d^{6.6} \) fit to the atom number in the glass cell. (b)–(d) illustrate the optical overlap volume of the grating chip as a function of \( d \) with a highlighted 3 mm height of the chip-scale cell. The gray line highlights the grating chip position.

The dashed black line in Fig. 3 shows a \( d^{1.6} \) scaling of the atom number, expected for a constant intensity of the incident beam \(^{31,32} \) that expands in three dimensions. Previous studies have demonstrated that significantly smaller overlap volumes for 6-beam MOTs \(^{33} \) and pyramid MOTs \(^{34} \) are reduced to a \( d^{2} \) scaling, as the atom number is then limited by the stopping distance of the overlap volume rather than the cooling light intensity that dominates the process for larger beam diameters. We note that the measured atom number in the chip-scale cell is lower than the theoretical \( V^{1.2} \), shown as a solid red curve. The cause of this is currently unknown and will be investigated in future studies.

When limited by atom shot noise, the stability of cold atom sensors scales inversely with the square-root of the atom number. In this case, an order of magnitude improvement in the chip-scale cell would be favorable. Expanding the overlap volume simulation to a 5 mm thick silicon frame enables a 71% overlap between the optical overlap volume and the vacuum volume of the chip-scale cell when the grating is held 1 mm from the cell lower window. Using identical scaling parameters to the 3 mm chip-scale cell curve shown in Fig. 3(a) results in an achievable atom number of \( 10^{6} \) atoms for a 2 cm incident beam diameter in this thicker cell geometry. Thus, we plan to fabricate thicker silicon cells in the near-future to enable a wider range of applications for this chip-scale laser cooling platform. Additionally, a steeper angle of diffraction with a two-dimensional grating geometry would provide an overlap volume that is largest at the chip surface for an improved atom number within the reduced vacuum volume compared to the tri-segmented chip used here. The improved atom number will enable studies into passive pumping with NEGs in an aluminosilicate based chip-scale cell.\(^{25} \)

In conclusion, we have demonstrated a simple imaging solution for atom number extraction in a chip-scale cooling platform. The laser cut hole in the grating chip has shown a negligible atom number degradation, while enabling a sufficient numerical aperture for imaging small atom numbers in future experiments. We have shown that the 3 mm height of the micro-fabricated cell reduces the achievable overlap volume and, hence, atom number, when coupled with a micro-fabricated grating chip. However, moving to the machining of thicker silicon wafers will enable a work around to bring this platform to a competitive stance for quantum technologies. In addition, it may also be advantageous to apply an anti-reflection coating to the cell windows during fabrication due to the increased etaloning observed in the through-hole images. While the effect of these fringes on the images was minimal, especially for larger MOTs, and can be mitigated through alignment, there are also several fringe removal algorithms that can be applied in post-processing to further reduce their impact.\(^{35,36} \)

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AUTHOR DECLARATIONS
Conflict of Interest
The authors have no conflicts to disclose.

DATA AVAILABILITY
The data that support the findings of this study are available from the corresponding author upon reasonable request.

REFERENCES