

Discrete Power-Stepping Pulse Amplitude Modulation for Optical Camera Communications Employing a CMOS-Integrated GaN μ LED Array

N. Bani Hassan^{1,*}, M. J. Strain¹, M. D. Dawson¹, J. Herrnsdorf¹

¹Institute of Photonics, Department of Physics, University of Strathclyde, Glasgow G1 1RD, UK

*email: navid.bani-hassan@strath.ac.uk

Abstract— We present discrete power-stepping m -ary pulse amplitude modulation for non-line-of-sight rolling-shutter-based optical camera communications. A bit error rate of 2.2×10^{-4} at a data rate of 16000 bps was achieved using a micro-pixel light emitting diode array and 4-ary pulse amplitude modulation.

Keywords—optical camera communications, discrete pulse amplitude modulation, LED array.

I. INTRODUCTION

Optical camera communications (OCC) is an emerging technology, enabling communication using off-the-shelf cameras and light emitting diode (LED)-based transmitters (Tx's). Cameras can offer multiple functions such as vision, positioning, and communication, simultaneously. However, the data rate in OCC is limited normally to the frame rate of the camera. Different techniques including multi-input multi-output (MIMO) [1], colour shift keying [1], and equalization [2] have been employed to enhance the data rate in OCC. Moreover, complex modulations such as m -ary quadrature amplitude and phase (m QAM) [3] and m -ary pulse amplitude modulation (m PAM) [4] can boost the data rate to $\log_2 m$ times the frame rate of the camera. However, complex modulation schemes require a digital to analog converter (DAC) to generate the electrical signal. Complementary metal oxide semiconductor (CMOS) image sensors with the implemented rolling shutter (RS) exposure mechanism can map temporal variation in the intensity of light into spatial changes in the image. This feature can be used to significantly improve the data rate in OCC by hundreds of times the data rate of the camera [4]. In the case of m PAM, the variations in the light intensity in the RS mode forms multiple bands with different brightness, see Fig. 1(a). In the absence of a DAC, an LED array can be employed to generate an analog signal by aggregating the intensity of individual LEDs, also referred to as digital-to-light conversion (DLC) [5]. In this paper, we demonstrate a DLC technique for PAM similar to [5] for non-line-of-sight RS-based (NLOS) OCC.

II. SYSTEM MODEL

Figure 1(a) illustrates the schematic system model used for this work. A μ LED array with a size of $M \times N$ transmits the optical information and a lens system projects the light onto a wall/screen in defocused mode. At the receiver side, an RS camera with a resolution of $U \times V$ captures the variations in the intensity of the reflected light, i.e., a $(M \times N) \times V$ non-imaging MIMO link at each time instant. Every symbol of the data generated in m PAM modulation is mapped to binary forming $\log_2(m)$ bits/symbol. Each bit is sent to a separate column of the LED array corresponding to its bit value. On the LED array, all LEDs within one column transmit the same data but independent of other columns (labelled c1, c2, and c3 in Fig. 1(b)). Note, the sum intensities (SIs) of transmitting columns are different corresponding to the bit value and a power of 2 times the column with lowest SI. That is, the column with lowest SI transmits the least significant bit, while the most significant bit is transmitted by the columns with the SI of $m/2$ times the lowest SI. As a result, a m -level illumination pattern is formed on the wall by aggregating the illumination of different columns, representing the same symbol of the generated PAM signal. Note, it is essential that Tx optics create a highly defocused footprint on the wall/screen so that the footprint of all LEDs fully overlap. Accordingly, at each time-step, labelled t1, t2, and t3 in Fig. 1(b), a striped pattern with discrete multi-level illumination is captured, see Fig. 1(c). The images taken are next processed to extract the data. In order to improve the signal to noise ratio (SNR), we element-wise average the values of all columns. However, this imposes distortion to the signal due to the shape of the footprint and illumination pattern. To compensate for the distortion, a picture of the footprint with no AC signal is taken to obtain a calibration curve. Next, we element-wise divide the received signal by the calibration curve; see Fig. 1(d). The SNR at the edges of the footprint is very low and dividing by a small number imposes a high noise level. Therefore, we truncate the signal on both sides to ensure a reasonable SNR for the received signal. Note, this method can also be implemented in line-of-sight OCC, provided that a large defocused footprint of the light source can be created on the image sensor.

III. RESULTS

We evaluated the proposed concept experimentally. The system setup comprised a 16×16 flip-chip bonded array of GaN μ LEDs with 100- μ m pitch, 72- μ m pixel diameter, a bandwidth of 110 MHz, and a peak intensity at 410 nm; a camera lens with a FoV of ~ 4.5 degree; a white wall; and an iPhone-7-plus wide-angle rear camera. The camera, the LED array and the optics were positioned at a height of 25 cm from the base, all facing towards the wall, creating an NLOS link. The ISO and exposure time of the camera was

set to 1760 and 125 μ s, respectively, and the resolution of the camera was 3024 \times 4032. To obtain the calibration curve, we took 20 pictures of the footprint with no AC signal on and took an average over the pictures and the columns. This ensures a reduced temporal noise standard deviation, hence a low noise calibration curve with a size of 3024 \times 1. We generated 4000 bits in 4-PAM format and passed it to the system in 10-symbol long packets and captured 1000 JPG images of the footprint. For each image, an average over all columns was taken, leaving an array with a size of 3024 \times 1. This array is then elementwise divided by the calibration curve. Figure 2 (a)-(c) show the eye diagram of the 4-level received signal for R_b of 2000, 4000, and 8000 symbol/s, respectively. We sample at the maximum eye opening to minimise the impact of inter-symbol interference (ISI). We measured the mean and standard deviation of each level and estimated the bit error rate as 9.5×10^{-8} , 9.2×10^{-8} , and 2.2×10^{-4} , respectively, which are all below the 7% forward error correction limit of 3.8×10^{-3} . Therefore, we achieved a data rate of 16 kbps. Note, the eye closes as the R_b increases. This is due to the ISI imposed by the exposure time, i.e., to open the eye a shorter exposure time must be used at a cost of reduced SNR.

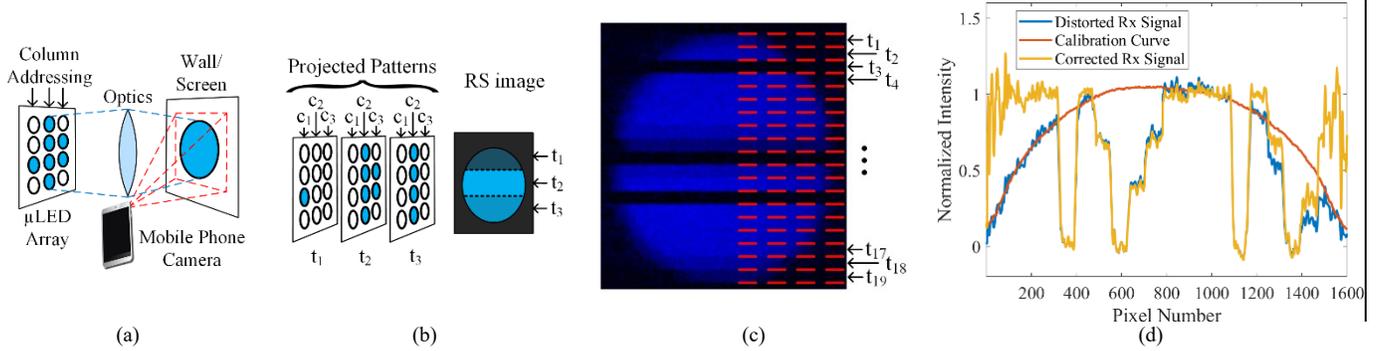


Fig. 1. (a) Schematic of the setup, (b) illustration of discrete PAM encoding and received image with RS effect, (c) experimental result, where the horizontal red lines indicate symbol boundaries, (d) Normalized intensity as a function of pixel number for the received signal.

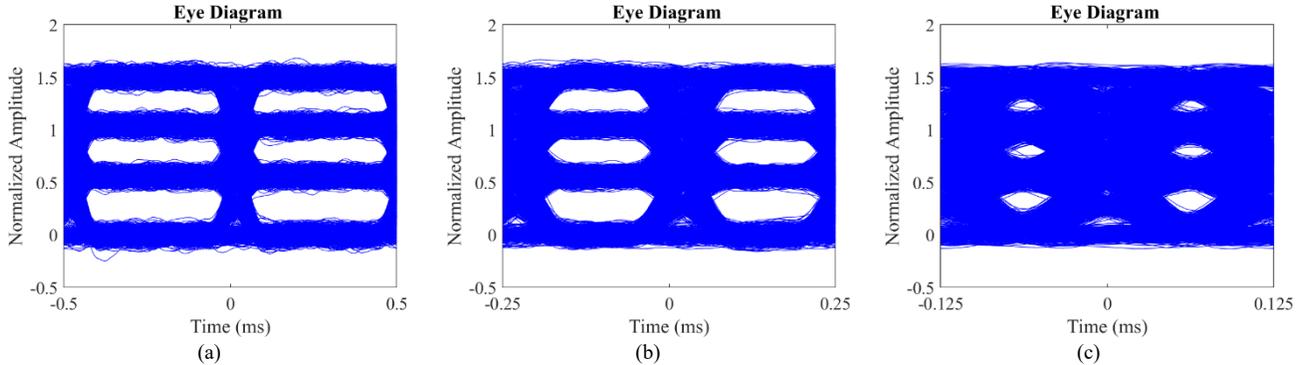


Fig. 2. Eye diagram of the received signal for R_b of (a) 2 ksymbol/s, (b) 4 ksymbol/s, and (c) 8 ksymbol/s.

IV. CONCLUSION

In this paper, we demonstrated experimentally that the digital-to-light approach is readily implemented in optical camera communications and helps to increase the achieved data rate; in our case by a factor of 2 compared with conventional RS-OCC using OOK modulation schemes.

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