

Development of Modular Bio-inspired Autonomous Underwater Vehicle for Close Subsea Asset Inspection

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Abstract: To reduce human risk and maintenance costs, Autonomous Underwater Vehicles (AUVs) are involved in subsea inspections and measurements for a wide range of marine industries such as offshore wind farms and other underwater infrastructure. Most of these inspections may require levels of manoeuvrability similar to what can be achieved by tethered vehicles, called Remotely Operated Vehicles (ROVs). To extend AUV intervention time and perform closer inspection in constrained spaces, AUVs need to be more efficient and flexible by being able to undulate around physical constraints. A biomimetic fish-like AUV known as RoboFish has been designed to mimic propulsion techniques observed in nature to provide high thrust efficiency and agility to navigate its way autonomously around complex underwater structures. Building upon advances in acoustic communications, computer vision, electronics and autonomy technologies, RoboFish aims to provide a solution to such critical inspections. This paper introduces the first RoboFish prototype that comprises cost-effective 3D printed modules joined together with innovative magnetic coupling joints and a modular software framework. Initial testing shows that the preliminary working prototype is functional in terms of water-tightness, propulsion, body control and communication using acoustics, with visual localisation and mapping capability.

Keywords: underwater robotics, biomimetic AUV, biomimetic propulsion, 3D seafloor reconstruction, acoustic communication

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1. Introduction

The use of offshore wind power will play an essential role in our future electricity generation. It is forecast that by 2050, 12 percent of the world's primary energy supply will come from wind energy, and 20 percent of this will come from offshore wind [1] [2]. However, ongoing wear and corrosion from the harsh sea environment drives up cost and introduces downtime to this renewable and clean energy source [3]. To ensure reliable production, regular inspection tasks during high seas up to 100m depth need to be performed in a cost effective and safe manner [4]. These tasks are currently being conducted largely using Remotely Operated Vehicles (ROVs) which generally need tethers and a human operator, or using Autonomous Underwater Vehicles (AUVs), which are limited in their accessibility and manoeuvrability [5] [6]. To extend AUV intervention ability and perform critical inspection tasks, they need to be efficient and flexible in operation. A fish-like AUV with a bending body of a spinal column design that is able to mimic propulsion techniques of living fish can provide efficient thrust at minimum swimming velocities, and higher manoeuvrability in limited spaces during



Figure 1. RoboFish CAD Model with Four modules: Head, Two Segments, and Tail

33 sensor data acquisition. RoboFish was created by the project "Autonomous Biomimetic
34 Robot-fish for Offshore Wind Farm Inspection" supported by the EPSRC Supergen
35 Renewable Energy Hub and "Innovating the Future of Bio-Inspired Autonomous, Robots
36 for Offshore Renewable Energy Inspection" supported by the White Rose University
37 Consortium. It was specifically aimed at investigating and exploiting bio-inspired
38 mobility features to facilitate autonomous inspection of offshore infrastructure, and is an
39 agile and efficient biomimetic AUV that will in the near future be able to continuously
40 inspect the foundations of offshore wind turbines and drastically reduce potential risks
41 to divers, maintenance costs, and operational constraints. RoboFish replicates the full-
42 body movement of an eel allowing greater agility and better energy efficiency in close
43 proximity to structures.

44 The understanding of fish swimming and exploring its benefits and application
45 in engineering designs is an interdisciplinary research field of significant and ongoing
46 interest [7] [8] [9] [10]. Swimming robots mimicking techniques of natural swimmers
47 promise to provide an increase in overall swimming performance over conventional
48 thruster propelled systems. In Reference [11], thrusters waste energy by generating a
49 vortex perpendicular to the desired thrust direction. On the other hand, aquatic animals
50 are able to efficiently produce a jet in desired direction through active and passively
51 controlled body motion. Based on the modular build-up of identical body modules and
52 the resulting equal mass distribution a swimming gait resembling an eel is anticipated.
53 Research into eel locomotion in Reference [12] predicts swimming efficiencies of 0.5 to
54 0.87 depending on choice of calculation, compared to thruster efficiencies of up to 0.4 in
55 Reference [11]. Among the two main categories of fish swimming, propulsion employing
56 displacement of the centre line of the RoboFish, so called Body Caudal Fin, is suggested
57 to have advantages in speed and long distance travel over flapping fin propulsion of
58 Median Paired Fin [13]. Given the target application of Robofish is windfarm inspection,
59 the slender body design of a BCF swimmer is beneficial for the anticipated long-distance
60 travel between wind turbines, maintaining a high level of manoeuvrability through
61 its body flexibility. Resulting from this, more complex routes are available potentially
62 reducing travel distance extending range. Low noise and mitigated risk of entanglement
63 of continuous rotating parts suggest lower environmental disturbance. Further, the multi-
64 actuated system promises advantages through flexibility and adaptability in entering
65 tight spaces and manoeuvring in complex environments. The long body shape proves
66 also suitable for the anticipated modular design, enabling extendibility and flexibility for
67 mission setup of different intervention tasks and increased robustness and survivability
68 in case of isolated module failure.

69 2. Motivation and Background

70 Traditionally, offshore infrastructure such as wind turbines have been inspected
71 in person by humans, with the associated risks to safety in inclement weather and
72 changing underwater conditions. More recently, automated inspection systems such as
73 drones above the water and underwater vehicles have been developed, but with limited
74 autonomy and loitering time. Human intervention to control an underwater vehicle can

75 be quite beneficial, especially during complex inspection tasks which require human
76 judgement and intuition. ROVs have been in existence since 60s [14], and received
77 international attention following the aftermath of the Deepwater Horizon disaster in
78 the Gulf of Mexico in 2010 [15]. In this disaster, human operators sent ROVs fitted out
79 with a saw and manipulators to cut and cap an oil well head at a depth of one mile. The
80 precise control, flexibility and ability to have dangerous jobs done at great depths make
81 ROVs an ideal solution for such inspection tasks in open water. ROVs enable unique
82 access to the underwater world, and can also have robotic arms for object manipulation
83 to provide a safe alternative to perform otherwise costly and dangerous tasks. Being
84 tethered, their advantage over AUVs will, however, be restricted by the complexity of
85 the underwater infrastructure.

86 Unlike ROVs, AUVs have no human intervention in their control loop and they run
87 more independently. AUVs are traditionally used to gather oceanographic data using
88 cameras, SONAR, and other sensing instruments. Using advanced control algorithms,
89 AUVs can run in an autopilot mode for hours and even days without receiving constant
90 operator guidance. REX II [16] from MIT is a unique AUV that can run autonomously and
91 through a remote operator. While loitering around autonomously, Rex II can transmit
92 video images over a wireless channel using a tethered buoy equipped with a radio
93 modem, which is also used in the manual operating mode to enable remote control by an
94 operator. Odyssey IV is an AUV with a pioneered concept known as hovering [17]. It is
95 capable of remaining stationary anywhere up to 6000 meter depth. After AUVs became
96 able to reach great depths and hover around in the oceans, the ability to operate over a
97 longer period of time and cover an extended range were the next features to improve.
98 AUVs can, otherwise, catch only brief glimpses in time and space of the underwater
99 world. Thus, a newer class of more recent AUVs such as Autosub-Long-Range [18] and
100 HUGIN-AUV [19] were developed to push beyond their powers of endurance for longer
101 ranges, and larger sensor payloads. This class of AUVs is particularly useful in offshore
102 surveying applications.

103 Although the aforementioned sophisticated AUVs are extremely capable, they are
104 not the optimal platform to operate in shallow water and inspect assets closely in critical
105 locations due to their relatively large size, unbending bodies. Because of the limitations
106 of AUVs and constraints of ROVs in certain applications, a new, low cost, bendable
107 vehicle was needed to efficiently perform research missions in shallow water and inspect
108 subsea assets. This requirement is what initiated the design for RoboFish, a low cost,
109 modular, hovering AUV or wireless ROV. The concept of a flexible subsea vehicle
110 comprising a chain of joints that are collectively able to change shape was previously
111 successfully implemented by Eelume-AS [20]. Elemue demonstrated dexterity and
112 hyper-redundancy that has not been commercially available before in the inspection,
113 maintenance and repair (IMR) applications. During IMR, the vehicle is able to transit
114 over distances and hover around using ducted lateral and vertical thrusters attached
115 along its flexible body. Unlike Eelume, RoboFish does not use any thrusters and has
116 the ability to run both autonomously or remotely controlled by means of an acoustic
117 communication system.

118 Fish-like robots have been an active research area due to the remarkable physical
119 mobility of fish in nature. A review of biomimetic robotic fish, their gaits, and actuators
120 is in [21]. The Eel gait (Anguilliform) is most suitable for the current eel-like body
121 of RoboFish and the trout gait (Subcarangiform) is more likely to show instability
122 in this kind of robot than robotic fish that have a trout-like body [22]. The eel gait is
123 used in many similar robot fish also and is well known in the literature. Reference
124 [23] shows an underwater snake robots named Mamba for underwater operations in
125 2016. The long and slender structure of such robots provide capabilities through narrow
126 openings and within confined areas. Other related robot fish projects are Envirobot by
127 EPFL [24] and ACM R5 by Hirose Fukushima Robotics lab in Japan [25]. The Envirobot
128 platform was based on their existing segmented anguilliform swimming robots, but with

129 important adaptations in terms of energy use and efficiency, control, navigation, and
130 communication possibilities in 2016. Envirobot was powered by an ARM processor in the
131 head unit and micro processors in each active module. An integration of a computer-on-
132 module enables versatile high level control methods was used in this underwater robot.
133 ACM R5 was developed an amphibious snake like robot named that can manoeuvre both
134 on ground and in water surging its long body in 2005. ACM R5 was set with paddles
135 and passive wheels around the body to attain that nature both in water and on ground.
136 ACM R5 had an advanced control system. Each joint unit had a CPU, a battery, and
137 motors so it can operate independently. Through communication lines each unit can
138 exchange signals and automatically recognise its number from the head, as well as how
139 many units join the arrangement. The dynamic structure of ACM R5 gave operators the
140 freedom to remove, add, and exchange units freely.

141 In this paper, we stated some new features that RoboFish will have as advantage
142 over these examples. This paper is intended as a high level overview of the RoboFish
143 architecture which contains modularity of this type eel like robot using magnetically
144 coupled joints. We consider the way they are applied in RoboFish essential for achieving
145 some fundamental needs in cyber physical autonomous underwater systems, a single
146 universal end to end communications system, a modular control and software architec-
147 ture based on the resiliency of autonomic elements but using off the shelf parts for cost
148 effectiveness, and a physical embodiment that is 3D printable yet fully enclosed and
149 watertight without the chance of wear and collisions causing seal failures. This paper
150 describes the first working prototype of RoboFish that is equipped with an acoustic
151 modem, a SONAR rangefinder, a camera, and uses computer vision for close-range
152 navigation and inspection of structures, with the ability to build complete visual models
153 of the structure using 3D reconstruction methods. This prototype is a cost effective
154 underwater platform and could be spun out to a successful commercial product.

155 The paper is organised as follows: Section 1 is an introduction; Section 2 provides the
156 motivation and background; Section 3 discusses the system design; Section 4 describes
157 the vision system; Section 5 describes the acoustic communication system; Section 6 is
158 the locomotion control design of the RoboFish; Section 7 presents the outcomes of initial
159 testing; Section 8 presents ideas for future work; Section 9 concludes the paper.

160 3. RoboFish Design

161 Development of a modular bio-inspired autonomous underwater vehicle for close
162 subsea asset inspection is a task of extraordinary hardware and software challenges
163 (shown in Figure 1). Splitting a protective, watertight 3D printed enclosure into jointed
164 segments, collectively mimicking the motion of a fish is an example of these challenges.
165 To overcome this, innovative mechanical and electronic modular designs were created
166 as this section introduces.

167 3.1. Vehicle Requirements

168 The current RoboFish design was created within the scope of offshore wind farm
169 inspection. While the mission of RoboFish is clear, there were a number of other re-
170 quirements that had to be involved into the design such as affordability, underwater
171 docking, manoeuvrability, and acoustic remote control. To meet all the requirements, the
172 academic and industrial project partners were involved in early design meetings. The
173 following list outlines the partners that were involved in defining the current RoboFish
174 prototype's requirements.

- 175 • University of York (Intelligent Systems and Nanoscience Group and Underwater
176 Communication Group)
- 177 • University of Strathclyde (Computational Fluid Dynamics and Fluid Structure
178 Interaction Research Group)
- 179 • Supergen ORE Hub
- 180 • PicSea Ltd

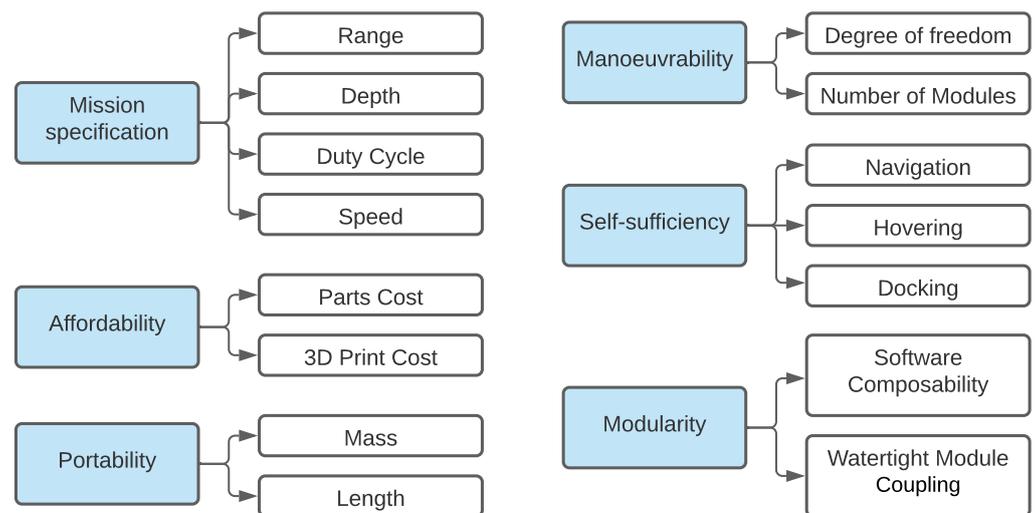


Figure 2. RoboFish's Mapping of Top-level Design Parameters to KPAs.

- 181 • EC-OG Ltd
 182 • Offshore Renewable Energy Catapult

183 Consulting with the aforementioned partners, the budget boundaries were defined
 184 in order to avoid involving materials, features and characteristics that were beyond the
 185 budget. Next, through collective research and engineering discussions, the minimum
 186 requirements to operate RoboFish in the ocean environment around wind farms was
 187 defined. Finally, the type of data required in inspection missions was decided. The
 188 primary RoboFish requirements defined in the early design stage are:

- 189 • Manoeuvrability
 190 • Affordability
 191 • Portability
 192 • Modularity
 193 • Self-sufficiency

194 3.2. Key Performance Attributes

195 Ideally, all design requirements are defined at the top-level to ensure that the
 196 mission of RoboFish is comprehensively covered. In the design process of RoboFish, the
 197 attributes that ensure meeting the minimum design requirements were further defined.
 198 This was achieved by creating Key Performance Attributes (KPAs) as depicted in Figure
 199 2. KPAs were linked to the top-level design requirements in order to determine how
 200 RoboFish would meet the overall requirements of a subsea asset inspection mission.
 201 The current RoboFish KPAs are determined based on the mission of offshore wind farm
 202 inspection and are measurable design characteristics that control the overall effectiveness
 203 of the RoboFish design. The KPAs for the current prototype are listed in Table 1. Based
 204 on the top-level design requirements, a decision matrix was created to determine the
 205 best off-the-shelf options with regards to batteries, cameras, servos and micro-controllers.
 206 Using KPAs, associated weights are used to evaluate each decision matrix. In general,
 207 the author were guided by a design philosophy that can be quoted as:

208 Design a low cost, modular AUV to perform underwater inspection around
 209 complex structures. To keep costs at minimum, off-the-shelf parts and acces-
 210 sible additive manufacturing technologies will be used. The vehicle will be
 211 easy to launch, capture videos, recharge, and return to a home location with
 212 minimum or no human intervention.

Table 1: RoboFish Key Performance Attributes (KPA's)

Attribute	Objective
Depth [m]	100
Mission Duration [hrs]	3
Weight [kg]	30
Length [m]	1.9
Duty Cycle [%]	75
Modular	Yes
Speed [knot]	0.5

213 3.3. Mechanical Design

214 Robofish is composed of several separate body segments with a head at one end
 215 and a caudal fin at the other end. The segments are joined together using an innovative
 216 magnetically coupled joint. This allows it to have the required multiple degrees of
 217 freedom in its agility in order to move very precisely by aiming its head and undulating
 218 its body. With this type of locomotion, RoboFish features greater agility in close proximity
 219 to structures compared to conventional underwater vehicles. The current RoboFish
 220 prototype is developed using off-the-shelf parts and a common 3D printing technology,
 221 i.e. Fused Deposition Modelling (FDM). The prototype currently consists of three
 222 sections due to space constraints of laboratory testing. Being modular, it is scaleable
 223 and expandable. Five sections have been created and can be assembled easily during
 224 field testing to produce longer operation time, more efficient movement and higher
 225 agility. Buoyancy control is necessary for long-term loitering capability of biomimetic
 226 vehicles, and the buoyancy control of RoboFish is currently still being refined in design
 227 as the miniaturisation and pressure capability of such a buoyancy unit is a considerable
 228 challenge. To allow pitch control, one buoyancy unit will be ultimately installed in each
 229 segment of RoboFish, and they will operate independently to trim the attitude of the
 230 vehicle. The buoyancy units will draw a small amount of water from a port outside
 231 the body segment and compress the air inside to increase the mass of the segment a
 232 small amount, enough to offset the buoyancy of the vehicle for rising and diving. Roll is
 233 statically limited by placing the batteries low in the body.

234 3.3.1. Body Segment

235 This is a 3D printed enclosure using Acrylonitrile Styrene Acrylate (ASA) material.
 236 The primary part of the enclosure takes the form of cylinder of 9.3 cm internal diameter
 237 and 23.3 cm length, as shown in Figure 3. The total length of a segment can be variable
 238 with any modifications that are needed, but the length of the current configuration is
 239 43cm due to the size of the servomotors used. To reach the inside of the enclosure,
 240 O-ringed stainless steel rings with a male-to-female fit are used to hold the two parts of
 241 the enclosure together. This allows convenient disassembly while keeping the system
 242 watertight under high pressure. The enclosure is designed with a fork at one end to
 243 interlock with the rotor of the following segment, whereas the other end of the enclosure
 244 is fused to a magnetic coupling joint containing a rotor. The top of the enclosure allows
 245 wire entry via M10 penetrators, making a waterproof, high-pressure seal to pass Ethernet
 246 cable into the segment. The bottom of the segment is fitted with a M10 plugged vent,
 247 allowing trapped pressure to escape from the segment while it is being closed. This is
 248 also used for testing water-tightness on the segment using a vacuum pump inserting
 249 into the enclosure vent. Segments are joined together using a magnetic-coupling joint
 250 that allows a servo in each joint to rotate an external rotor that in turn rotates an internal
 251 rotor to move the next joint connected to the fork. Four guides with holes are built in on
 252 the outside circumference to allow the attachment of fins, ballast, or other accessories
 253 as required. Internally, components are mounted on a 3D printed mounting plate. The

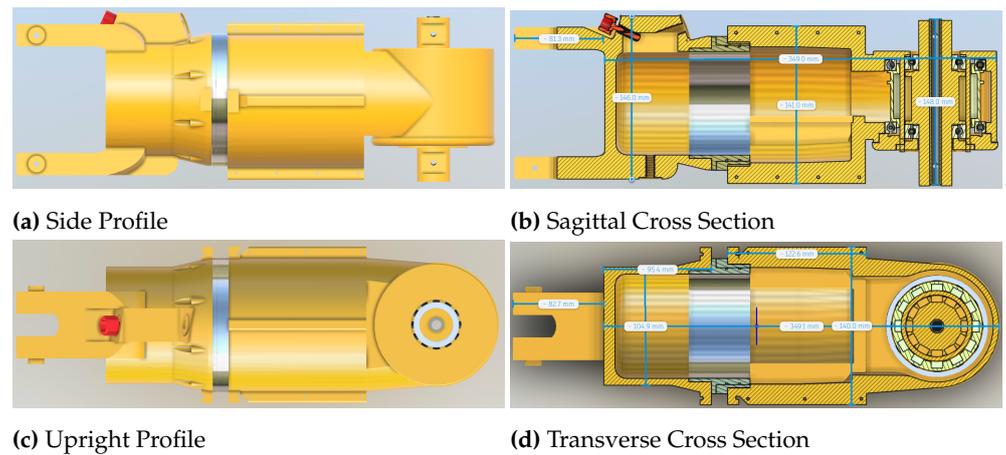


Figure 3. RoboFish Perspectives of a Segment's Cross Sections.

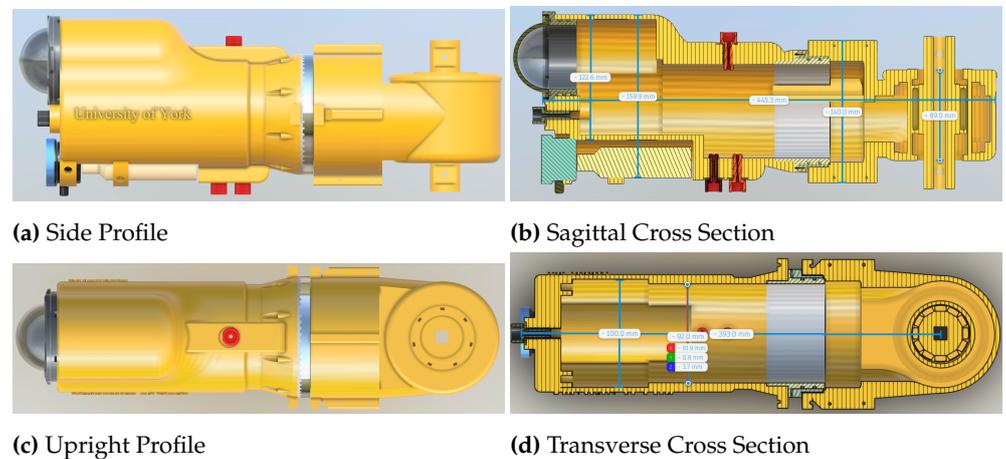


Figure 4. RoboFish Perspectives of the Head's Cross Sections

254 servo fits into a 3D printed frame moving on linear rails, working as a tilting drawer to
 255 provide the required tension for the timing belt by adjusting the sliding servo on the
 256 rails and locking it in place with two screws.

257 3.3.2. Head

258 This is a modified segment with the same 9.3cm diameter cylindrical enclosure,
 259 but with a front end that appears like a cockpit, allowing the attachment of clear acrylic
 260 dome end cap. The dome shape allows for extra room within the head for additional
 261 two or more cameras or sensors. It gives the camera a wider view than that of a flat end
 262 cap. It is very transparent and does not warp or distort camera images. The dome is
 263 fit into the head using a flange that has a double O-ring seal. Like the other segments,
 264 the head enclosure is fit with a pressure releasing vent and two cable penetrators. It is
 265 also provided with an additional M10 penetrator at the nose of the head, allowing a
 266 waterproof high-pressure seal to pass a 4-8mm tether into the head (should it be required).
 267 To mount the acoustic modem and rangefinder on the head without being obstructed, the
 268 head has an external hollow at the bottom, in which both devices are placed. Internally,
 269 like in the segment, components are mounted on a 3D printed mounting plate and a
 270 servo is fitted into a pull-on 3D printed frame (shown in Figure 4).

271 3.3.3. Tail

272 This is modelled after a caudal fin directly connected to a magnetic joint that en-
 273 ables active control of the fin motion, manoeuvrability and thrust generation for the

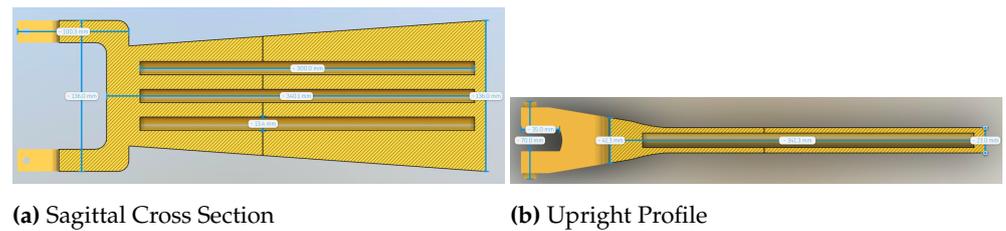


Figure 5. RoboFish Perspectives of the Tail's Cross Sections.

274 overall body. An appropriate fin design can contribute to the overall device stability and
275 manoeuvrability. Many species use their caudal fin as the main propulsive and manoeu-
276 vring appendage in addition to the body. For example, almost all of the thrust comes
277 from the caudal fin for *Thunnus albacares* and *Acanthocybium solanderi* as suggested
278 by Fierstine and Walters (1968) in [26]. Moreover, the tail may also help produce lift force
279 to balance gravity and buoyancy [27]. In the current design, the caudal fin is directly
280 attached to an actuated joint (shown in Figure 5). This makes it possible to optimise the
281 interaction between the body and tail to enhance propulsion performance and achieve
282 manoeuvrability, e.g., braking, when necessary. The caudal fin in this work has another
283 function to provide additional buoyancy by using a hollow design. In this way, the mass
284 of the caudal fin itself is decreased and it also reduces the energy consumption when the
285 joint servo actuates the rotation of the tail.

286
287 Using Computational Fluid Dynamics (CFD) techniques and Fluid Structure In-
288 teraction (FSI) numerical solvers, it was possible to numerically study the propulsion
289 performance ahead of the manufacturing stage. This provides insights into the structural
290 design and material selection. Using a fully coupled FSI numerical solver consisting of
291 a finite volume method based fluid solver and finite element method based structural
292 solver [28], a preliminary analysis was performed on the motion control of the simplified
293 system [29]. The caudal fin was simplified as a 2D cross-section in rotation locomotion.
294 The yaw angle was a result of PID control with feedback and the control objective is to
295 find the yaw angle matching with the specified steady swimming speed. Initial results
296 showed that the medium stiffness is the most favourable in terms of thrust production,
297 which provides insights into our material selection of the caudal fin and locomotion
298 parameters in the design of the AUV.

299
300 The current fin is printed with ASA materials, which are rigid, to manufacture a
301 fish-inspired tail. Subsequently, the project consortium is curious as to whether flexibility
302 can enhance thrust production and, if so, how flexible the fin needs to be to achieve the
303 most thrust improvement. For a real fish, the conformation of flexible fins would be
304 changed as the fin rays and membrane deform under hydrodynamic forces and inertial
305 force. In return, the fin deformation changes the surrounding flow field; and thus, the
306 resultant force conditions of the fin. During the dynamic interplay between the flexible
307 caudal fin and immersed fluid, the propulsive capabilities may be improved significantly
308 compared with cases when a rigid fin is adopted.

309 3.3.4. Magnetic Coupling Joint

310 This is a mechanism that mechanically joins two watertight enclosures together and
311 transmits the torque of a rotary actuator between an outer driving shaft and an inner
312 driven shaft without physical contact. This enables a servomotor in one of the enclosures
313 to actuate the other enclosure and achieve a precise control of angular position, velocity
314 and acceleration of the body. The contact-less bond is created by the magnetic attraction
315 of a number of magnetic blocks evenly distributed on the side surface of the two shafts
316 with opposite polarity. This allows the two enclosures to function like a robotic arm with
317 rotational joint motion. To keep costs to a minimum, off-the-shelf small magnetic bricks

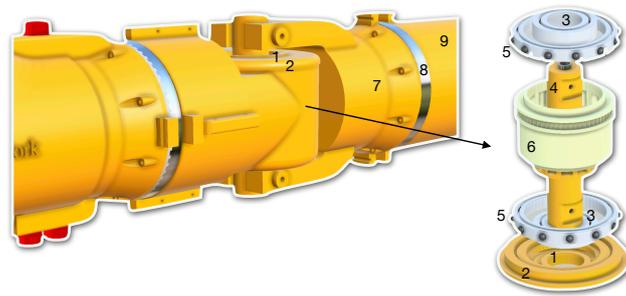


Figure 6. Body parts comprising a segment: 1- Inner joint housing lid; 2- Outer joint housing lid; 3- Zirconia ceramic bearing; 4- Driven shaft; 5- Stainless bearing; 6- Driving shaft; 7- Electronic

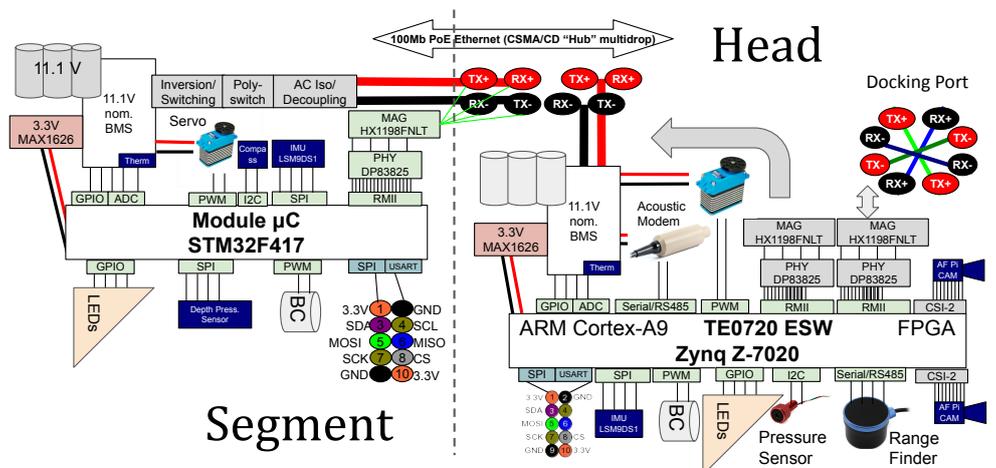


Figure 7. Simplified Electronic System Design of RoboFish; Modular Software and Hardware Architecture; Each Module is Self-contained.

318 were used. Figure 6 illustrates the magnetic joint's internal parts. The recent paper [30]
 319 provides additional details about the implementation of RoboFish magnetic coupling
 320 joints and how to maximise the transmittable torque with different numbers, types and
 321 arrangement of magnetic blocks.

322 3.4. Electronic Design

323 A simplified design schematic of the RoboFish electronic systems is shown in
 324 Figure 7. RoboFish uses a modular software and hardware architecture. Each segment is
 325 self-contained and includes self-managed battery power, internal and external sensor
 326 data, and actuator control using a low-cost microcontroller. Communications and power
 327 transfer between segments are performed through a customised 100 Mbit Ethernet bus,
 328 and it can charge autonomously underwater by docking with a source such as EC-OG's
 329 Subsea Power Hub. The head segment contains a powerful Xilinx Zynq SoC that serves
 330 as a master control node, communications router, and FPGA-accelerated vision platform
 331 with an acoustic rangefinder for position detection. While Wi-Fi communication is only
 332 available on the surface, RoboFish can also communicate at low rates underwater by an
 333 acoustic modem. It currently uses vision for close-range navigation and inspection of
 334 structures, with the ability to build complete visual models of the structure by using 3D
 335 reconstruction methods.

336 3.4.1. Requirements

337 As the RoboFish project aims to produce an autonomous agent, significant pro-
 338 cessing capabilities are required. On board real-time vision processing is required for
 339 navigation. Acoustic communication is required for feedback and issuing control com-

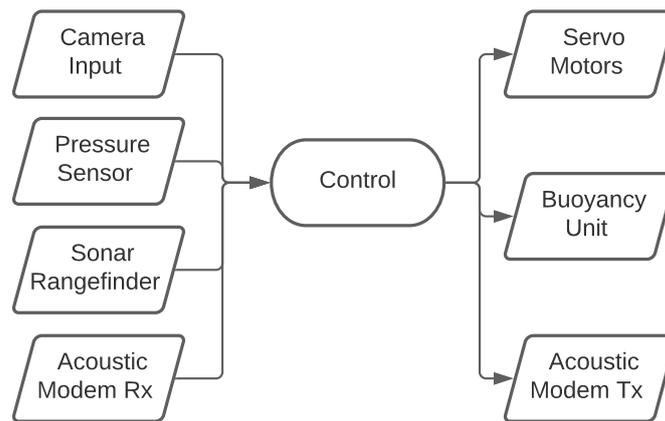


Figure 8. RoboFish Control Requirements

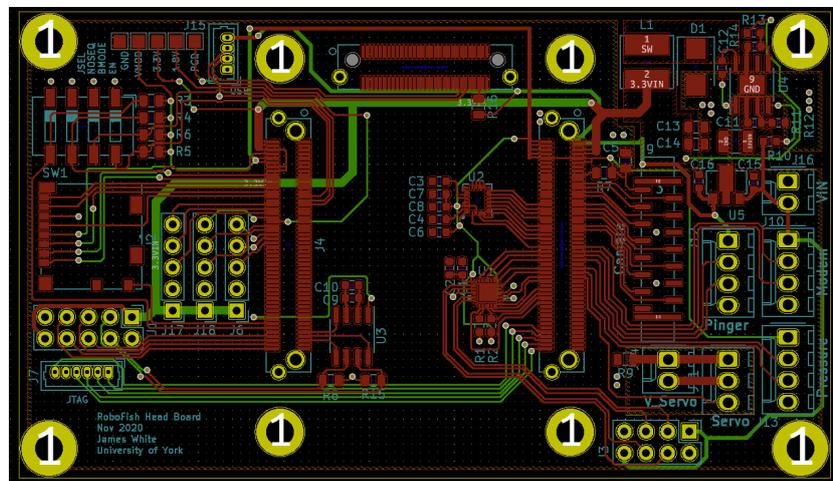


Figure 9. RoboFish Carrier Head board: a carrier PCB designed to contain all of the necessary hardware for interfacing the TE0720 SoM with the rest of RoboFish, programming the SoM and Regulating DC supplies; Either MIPI CSI-2 connector and USB is used for camera interfacing. SD card slot is provided; Either CAN or Ethernet is used for communication; LSM9DS1 IMU is used to provide orientation awareness.

340 mands during operation. Pressure sensing is required for water depth acquisition. A
 341 SONAR sensor is used for range-finding. Each of these sensory inputs are to be used as
 342 inputs to the control system of the robot. Actuation is produced using servo motors. The
 343 system of inputs and outputs is summarised in Figure 8.

344 3.4.2. Hardware choices

345 To fulfil the requirements stated in the previous section, while also making the
 346 platform upgradable in the future, the Xilinx Zynq 7000 SoC platform was chosen for the
 347 main processor of the system. The Zynq 7000 SoC is built around a hybrid processor and
 348 FPGA architecture. It consists of two ARM Cortex-A9 processor cores and Artix-7 FPGA
 349 programmable logic, with a high bandwidth AMBA AXI interface between them. This
 350 platform enables rapid development of software systems using a Linux operating system
 351 on the processor cores, with the ability to offload processor intensive tasks to the FPGA
 352 fabric. Offloading demanding tasks to the FPGA speeds up execution time for tasks like
 353 vision processing with potential power saving benefits too, which is important for a
 354 battery powered autonomous vehicle such as this. The FPGA fabric can also be used to
 355 create an inter-segment communications controller for communicating between the head
 356 and other segments without sacrificing processor time, resulting in higher-reliability



Figure 10. RoboFish Head Carrier PCB with the TE0720 SoM.

357 communication. For the other segments in the robot, the STM32 platform was chosen.
 358 Each segment is a modular element of the system, which accelerates development and
 359 upgradability.

360 3.4.3. Hardware implementation

361 *Head board:* The head board is based around a Trenz electronic TE0720 system on
 362 Module. This module incorporates the Zynq 7020 SoC, a 1 GB DDR3 RAM, 32 MB QSPI
 363 flash for configuration, an 8 Gbyte E.MMC flash for non-volatile storage, along with the
 364 power supply and configuration electronics for the SoC. This module was chosen over
 365 creating a custom board to accelerate development and ease upgradability (shown in
 366 Figure 9). If additional processing power and FPGA fabric is required in the future, this
 367 module can be swapped for a more powerful one without affecting the carrier board.

368
 369 The carrier PCB, shown in Figure-10, contains all of the necessary hardware for in-
 370 terfacing the Trenz SoM with the rest of Robofish, programming the SoM and regulating
 371 the battery power. Camera interfacing can be accomplished using either a MIPI CSI-2
 372 connector or USB. An SD card slot is provided to increase onboard non-volatile storage.
 373 For communication with other modules in the system, CAN was used for initial testing,
 374 and Ethernet was chosen as the final solution. Power is transferred between modules
 375 by using a modified power-over-ethernet (PoE) methodology with the DP83825 PHY
 376 chip and HX1198FNLT transformer IC. It also contains an LSM9DS1 IMU to provide
 377 orientation awareness of the head segment. The head also interfaces with the acoustic
 378 modem and SONAR rangefinder via RS-485 bus and breaks out GPIO pins used to
 379 drive LEDs, one PWM signal that controls the servo that drives the movement of the
 380 segment, and another PWM signal to be used for a buoyancy control unit that is still in
 381 development as of this writing. A general SPI and power pin header is provided for
 382 future expansion also.

383 *Segment board:* The segment board is built around an STM32F417 Microcontroller.
 384 This serves as a networked extension to the robots capabilities in a segment. It commu-
 385 nicates with the head board using CAN bus (initial testing) or Ethernet with PoE, and
 386 contains all of the necessary IO for any servos or sensors that may be required. It also
 387 contains an LSM9DS1 IMU for orientation awareness (shown in Figure 11), and breaks
 388 out control pins for driving LEDs and the servo and a buoyancy control unit with PWM,
 389 and the general SPI and power pin header.

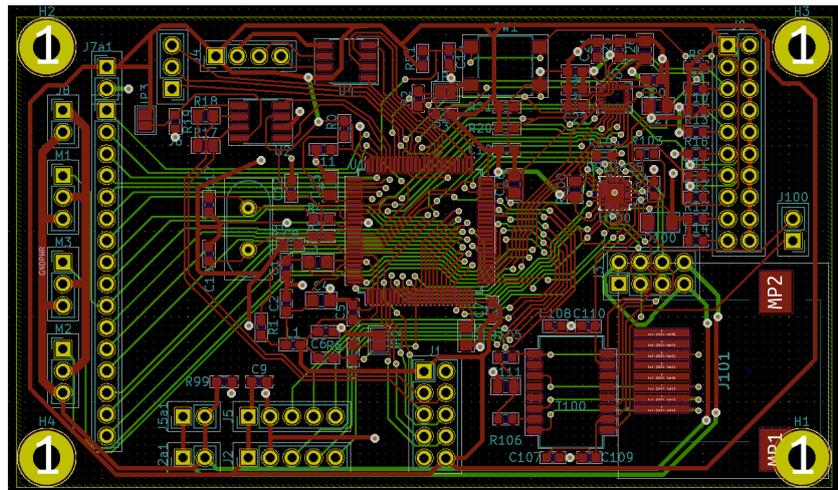


Figure 11. RoboFish Segment Board: a board designed to accommodate an STM32 F417 Microcontroller; it serves as a networked extension to communicate with the head board, and contains all of the necessary IOs for any servos or sensors, and contains an LSM9DS1 IMU.

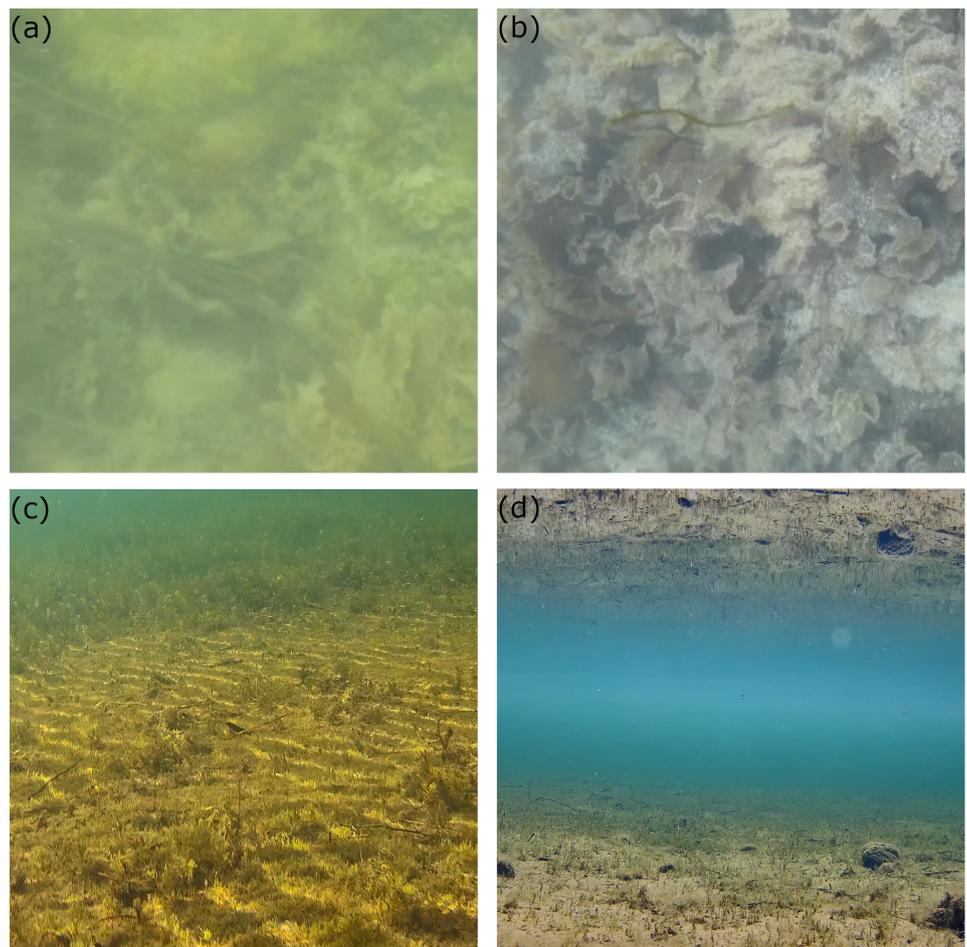


Figure 12. RoboFish Computer Vision Challenges: (a) Almost completely green image showing limited visibility, (b) floating particles in the foreground, (c) water caustics on a lake bed, created by the surface of the water, (d) total internal reflection underwater causing a mirror image of a lake bed in the water surface.

390 4. Underwater Vision

391 While visual simultaneous localisation and mapping (SLAM) has seen impressive
 392 development for autonomous ground vehicles (AGVs) [31] and unmanned aerial ve-
 393 hicles (UAVs) [32], the technical challenges presented by underwater environments
 394 have hindered progress for AUVs, particularly in real-time applications. Many unique
 395 visual phenomena affect underwater images such as wavelength-dependent attenuation,
 396 floating particles and bubbles, underwater caustics in shallow water, varying lights and
 397 shadows, moving flora and fauna and refractions through thick glass housing needed for
 398 waterproofing camera systems [33] [34], some examples of which are shown in Figure
 399 12.

400
 401 In the RoboFish project, the research aimed to test current state-of-the-art SLAM
 402 algorithms on underwater visual datasets and to quantify performance and suitability of
 403 those algorithms for use with low-cost Raspberry Pi cameras. To achieve this a graphical
 404 user interface (GUI) was developed in Python and OpenCV [36] to enable the real-time
 405 modification of popular feature matching algorithm parameters whilst providing visual
 406 feedback on performance and an estimation of the camera's 3D trajectory using visual
 407 odometry (VO). The most suitable parameters and image processing algorithms were
 408 then determined and implemented in a modified version of ORB SLAM 2 [31].

409
 410 The GUI was built in Python using the Matplotlib library. It was decided that only
 411 ORB [37] and BRISK [38] feature matching algorithms would be tested, however the
 412 design enables the addition of SIFT [39] and SURF [40] feature detectors with only minor
 413 modifications. Figure 13 shows the GUI. It enables the adjustment of either ORB or
 414 BRISK parameters in real-time via sliders and buttons, with the effects of these changes
 415 visible both qualitatively in the overlaid video feeds and quantitatively in the graphs.

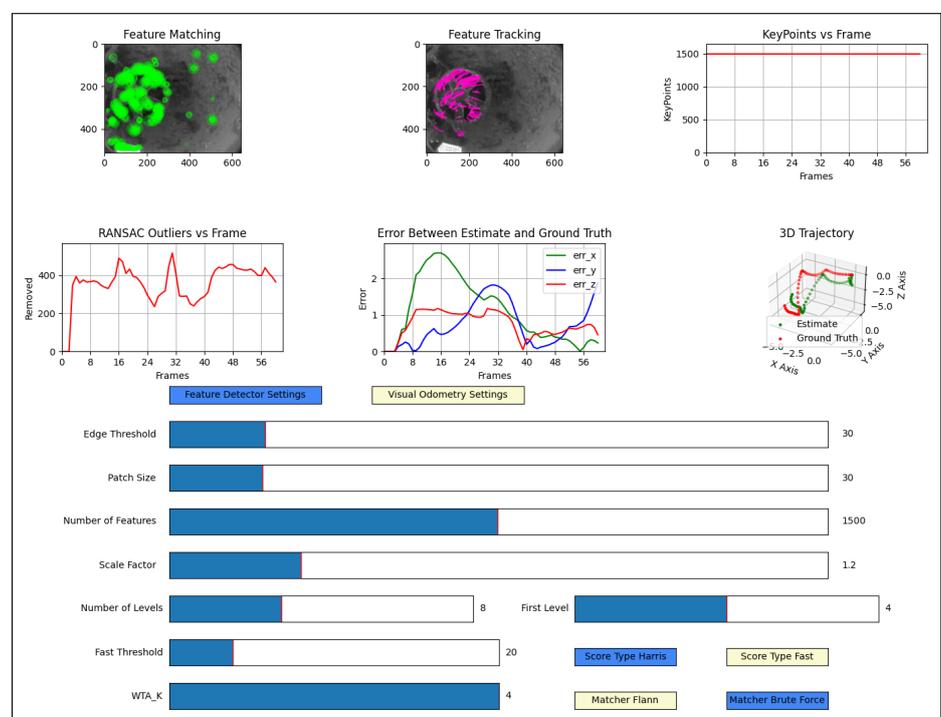


Figure 13. Python Matplotlib GUI showing the statistics of ORB features on the AQUALOC harbor-sequence-02 dataset [35] and including the video feed overlaid with ORB features: "3D Camera Trajectory" on the bottom right showing the structure-from-motion "ground truth" for comparison; "Sliders and Buttons" on the bottom enabling adjustment of ORB and VO settings in real-time.

416 Parameters can also be set prior to a test and it enables a previous tests' data to be
 417 displayed simultaneously on the graphs allowing comparisons of performance for each
 418 test. The camera's position is estimated using VO, the implementation of which was
 419 based closely on PySLAM [41].

420 5. Acoustic Communication

421 The RoboFish-specific powerful Xilinx Zynq SoC acts as a minicomputer on board
 422 processing a number of operations, one of which is communication. A half-duplex 64bps
 423 acoustic modem, called Water Linked M64 Acoustic Modem [42], is used to provide
 424 low-rate communications at medium range (i.e. 200 meter) for remote control, telemetry,
 425 and inter-vehicle coordination. This self-contained modem supports omnidirectional
 426 operation, which keeps the data link stable even when the RoboFish is in motion. It
 427 is programmed with a packet-based protocol with extensive use of error detection to
 428 enable a highly robust transmission at very low power consumption. It communicates
 429 via a serial 115200 baud UART 3.3V interface with the SoC board. Its small size enables
 430 easy integration in the RoboFish head. The Xilinx Zynq SoC includes an FPGA which
 431 will be used for acceleration of inter-vehicle communication architectures, protocols, and
 432 applications for efficient RoboFish swarm communication networks in the future.

433
 434 An interactive Python GUI, shown in Figure 14, was developed to run the RoboFish
 435 manually from a distance using the acoustic modem. The modem has a configurable
 436 data link and is interfaced using a lightweight API, on which the GUI design is based.
 437 The default serial protocol is documented in Reference [43]. This document describes
 438 the modem's Data Link Layer protocol. With this protocol, packets are sent to and
 439 received from the modem with serial communication commands taking this format
 440 115200 8-N-1 (payload size is 8 bytes). A Python script was put together to enable

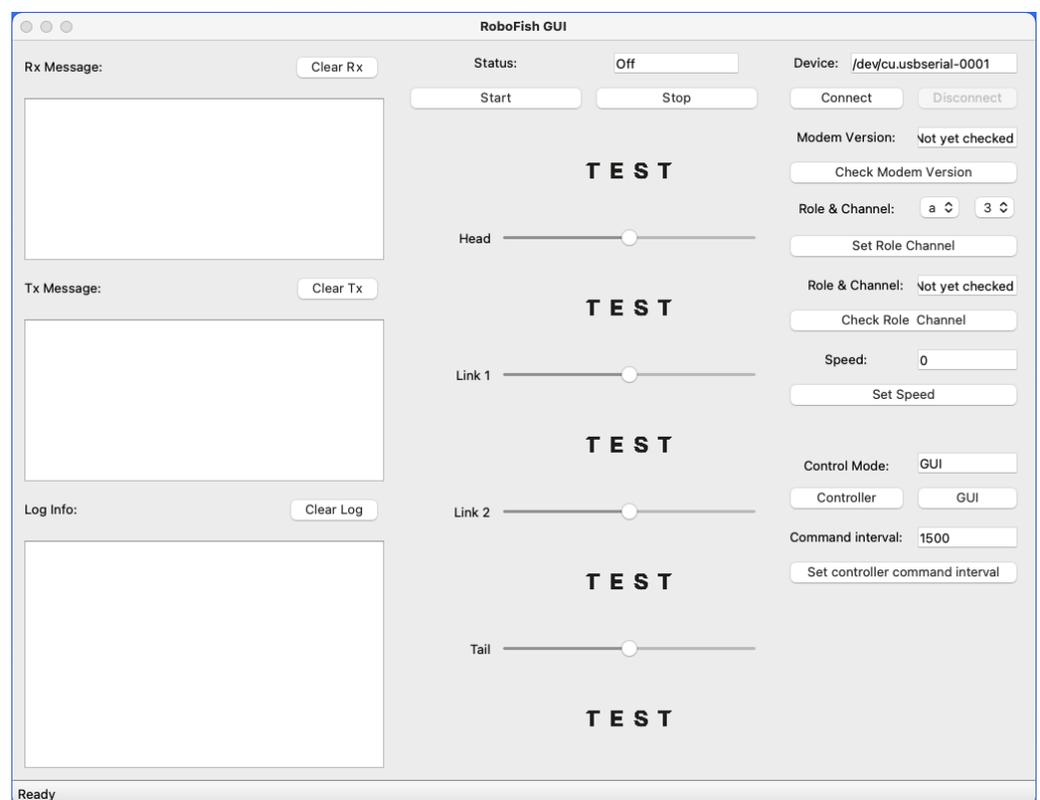


Figure 14. Python GUI for RoboFish Enabling Easier Interact with the RoboFish Acoustic Modem based on its API: works as a messaging application to remotely change parameters and control RoboFish over an acoustic channel.

441 sending and receiving these commands to the modems through the serial port. The
442 commands can be sent as a string represented by descriptive variable names or the GUY.
443 By configuring the modem that is installed in RoboFish as a receiver and the topside
444 modem as a transmitter, an operator can send these predefined commands to control
445 RoboFish manually over the acoustic channel if required. Through this GUI, the operator
446 can primarily control the degree of freedom for each joint by sending over acoustically
447 the required angle from the topside computer to RoboFish. Besides, the GUI enables
448 remote ON/OFF control, steering, selection of communication channel and displays
449 notifications received from RoboFish in humanly readable format for the operator.

450
451 In addition the acoustic modem, RoboFish uses Ping SONAR Altimeter and Echo-
452 sounder [44] that is a single-beam echo-sounder with a maximum range of 30m, a beam
453 width of 30deg and a maximum depth rating of 300m. It is connected to the RoboFish's
454 SoC through a serial connection using one of its Serial/UART ports. Distances read by
455 this Rangefinder can be read from a user interface running on the operator's computer.

456 6. Locomotion Control

457 Biological fish in nature repeat the same locomotion pattern for swimming to move
458 forward straight over a given period, it is possible to construct a precise mathematical
459 model through analytical approaches because its locomotion involves hydrodynamics
460 and kinematics [45]. However, for real-time control with microcontroller hardware, a
461 simpler parametric control method is sought. Using hydrodynamic analysis, control pa-
462 rameters that produce stable locomotion are produced for two approaches to locomotion
463 that are currently being tested, as follows.

464 6.1. Conventional Control

465 The first step of most conventional control design procedures is to establish the
466 mathematical model of the dynamic system, which is a set of ordinary differential equa-
467 tions [46]. The RoboFish has multiple joints and strong influences from the operational
468 environment. The control problem for stabilising the attitude and maximising the for-
469 ward velocity using the causal fin is high dimensional and underactuated. Designing a
470 controller taking into account the full nonlinear dynamics is challenging. The second step
471 is obtaining an approximate model for each operation scenario, i.e., the forward swim-
472 ming or the turning manoeuvre. This step is frequently performed using the feedback
473 linearization procedures [47]. Recently, reinforcement learning provides a promising
474 performance to deal with nonlinearity directly with less conservative design problems
475 [48]. The third step is to design a controller for the linearized system using linear control
476 design procedures, e.g., LQR (Linear Quadratic Regulator), PID (Proportional Integral
477 Derivative) [49]. There are several attempts to combine reinforcement learning with
478 conventional control [50] [51]. The combined methods would provide the capabilities
479 to exploit the nonlinearity in the nonlinear region and provide stability assurance in
480 the linear domain. Internal uncertainties and external disturbances would deteriorate
481 the stability and the performance. An external disturbance observer is combined in the
482 last step of the control design [52], and finally, the robustness analysis is performed [53].
483 In summary, the first control method implemented on RoboFish will be a convectional
484 controller combining linearization with reinforcement learning.

485 6.2. CPG-Control

486 Traditional model based control via numerical techniques, kinematic approaches
487 and geometric approaches is not always very well suited to dynamic and changing
488 conditions [54]. Biological systems produce rhythmic patterns using a functional unit
489 called a central pattern generator. A CPG can be considered as a dedicated neural
490 mechanism involving a group of neurons that coordinately generate rhythmic signals
491 without sensory feedback [55]. While sensory feedback is needed to shape the CPG

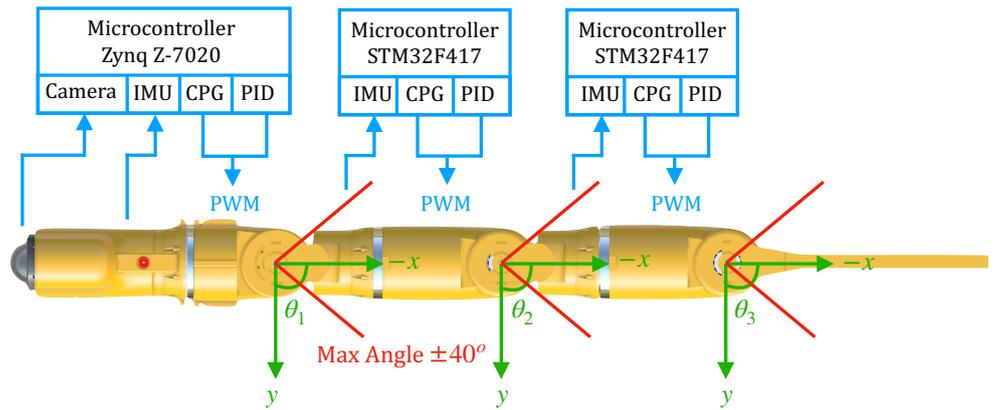


Figure 15. Locomotion Control Architecture: an example of RoboFish with three joints where θ_1 , θ_2 and θ_3 are the main parameters for locomotion control; the maximum angle of each parameter is ± 40 degree.

492 signals, the CPG can run independently without input. This method is widely used for
 493 the locomotion of robots such as crawling, flying, swimming, hopping, walking and
 494 running. The general design of CPG-based control has been focused on three aspects:
 495 CPG modelling and analysis, CPG modulation (parameter tuning and gait transition), as
 496 well as CPG implementation [56].

497 6.3. RoboFish Locomotion Control Architecture

498 In Figure 15, the RoboFish prototype is shown with its main control components. A
 499 monocular camera in the head is used for visual odometry and for detecting and tracking
 500 obstacles in the environment, with image processing running on the Zynq Z-7020 SoC in
 501 the head module. The inertial measurement units in each module of the body provide
 502 dynamic feedback from the body position. These are the main sources of sensory input
 503 for the locomotion control system. Currently, in the absence of sensory data (for example,
 504 if no visual odometry information is available), the system runs in open-loop mode, and
 505 control parameters for forward velocity and angular velocity are read directly from the
 506 desired movement commands. The output of the CPG based controller is transmitted
 507 to the servo motors in each joint via PWM signalling. The feature parameters of CPG
 508 will change the speed of the robotic fish while swimming. The power consumption of
 509 the servo motors will be recorded to compare the energy consumption corresponding to
 510 specific sets of CPG feature parameters. The modulation of the CPG will be restricted by
 511 each module's battery life. A comparison of swimming performance resulting from the
 512 conventional control methods cited, and the CPG design will be done after both control
 513 methods are implemented on RoboFish.

Table 2: List of the 3D Printer Parameters

Parameter	Value	Comment
Layer height	0.254 mm	Standard
extrusion width	0.5mm	Standard
Wall thickness	2.032 mm	To print more perimeters per layer
Solid infill	Enabled	To help preventing water ingress
Variable width fill	Enabled	To fill any small gaps
Room temperature	25 ^o	Enclosure



Figure 16. Robofish prototype with a Head, one Segment and Tail: 3D printed in ASA and using FDM.

514 7. Initial Testing and Lessons Learned

515 The work described in this paper led to the initial testing of the first RoboFish
516 prototype shown in Figure 16. This prototype is mechanically quite mature and had a
517 minimum number of completed modules in the initial testing to test water-tightness
518 in the first place. Although full autonomy has yet to be integrated into this prototype,
519 adequate electronic parts and processing capabilities were included in the initial testing
520 to fully program the vehicle with a basic operating system to primarily test propulsion.
521 The computer vision system and acoustic communication system have been completed,
522 and next trials will be fully integrated into the prototype. As a proof of concept, both
523 systems were tested separately in the initial testing and they were fully operational.

524

525 7.1. Testing Propulsion

526 This prototype is printed in ASA, with print parameters listed in Table 2 and KPAs
527 listed in Table 1. The prototype underwent its first test outdoors in December 2020.
528 The test went well and answered a number of questions. In this test, the prototype
529 undertook some important tasks, but the test was not a very long test that examines all
530 the Robofish features. This test was the foundation of more task-oriented trials to come.
531 The objectives of the test can be summarised as following:

- 532 • Testing water-tightness
- 533 • Testing the functionality of magnetic-coupling joints
- 534 • Testing propulsion

535 These initial trials were conducted in the University of York Campus West lake.
536 The depths were around 1-2 m, with temperature of around 8°C, 10 mph wind speed,
537 and poor water visibility. The prototype was put together and tested shortly on the
538 shoreline (the lake's edge platform) just before it was let go into water as shown in
539 Figure 17. In one testing scenario, RoboFish was dropped slowly into the water from
540 the platform using two ropes. To test swimming on the surface, two side plastic buoys
541 were included to maintain positive buoyancy and good balance with the right position
542 by preventing RoboFish from going below surface or turning upside down. With it
543 being directed toward the centre of the lake, the Go button was pressed and RoboFish
544 swam as expected. It was tethered to be brought back to the home point in the case of
545 failure or untimely need for battery recharge. In another testing scenario, RoboFish was
546 released to operate underwater. This was the first outdoor trial for Robofish. The shallow
547 lake seems to be an ideal place to carry out more tests to examine the functionality of

548 control, electronic and communication. As for computer vision, the location needs to be
549 investigated further.

550 Given that it is the first real outdoor trial, the performance of RoboFish was as good
551 as it was predicted. Initial testing of the propulsion mechanism revealed problems with
552 electrical connections and power cable wiring associated with batteries. To overcome this,
553 a new battery mounting plate was designed and is currently being 3D printed to enclose
554 all of the power network connections. The prototype is fitted out with cable penetrators,
555 ensuring watertight connections for the discrete cable that is used for both power
556 distribution and control signal communications between modules. In future design,
557 plug and bulkhead socket connectors would be a better option. Also, if the modules are
558 equipped with wireless chargers as an option it will save time, especially during testing.
559 Improvements on its buoyancy, thrust and swimming gait can be achieved via further
560 hydrodynamic analysis. This could involve making the head undulate less and the tail
561 oscillate more. Adding more segments will also improve the swimming gait.

562 7.2. Testing Computer Vision

563 In order to quantify the performance of the computer vision system, a dataset with
564 ground truth was required. To the best of our knowledge, one of the only underwater
565 datasets to provide a trajectory estimate is the AQUALOC dataset. This dataset provides
566 an offline calculated structure-from-motion trajectory [35]. The assumption was then
567 made that improvements in the accuracy of the PySLAM based VO calculated using
568 ORB features would result in improvements to ORB SLAM 2. A Python script was
569 written to cycle through various OpenCV image processing techniques (e.g histogram
570 equalisation and image filtering) and multiple ORB and BRISK parameters to deter-
571 mine which combination produced the most accurate estimate of the camera's trajectory.
572 This was determined using the mean squared error between the VO estimate and the
573 structure-from-motion ground truth trajectory obtained from the AQUALOC dataset. A
574 graph of the result of these tests with the most accurate configuration selected is shown
575 in Figure 18.

576
577 It was determined that the highest accuracy was achieved when using Contrast Lim-
578 ited Adaptive Histogram Equalization (CLAHE) and an ORB feature matcher with the
579 following parameters: Edge Threshold and Patch Size of 30; Minimum FAST Threshold
580 of 30; First Level of 4; Maximum ORB Features of 1500 and all others at default OpenCV



Figure 17. Robofish prototype Swimming on the Surface of a Lake: two side plastic buoys were included to maintain positive buoyancy; a rope is attached to it to be dragged to the home point in the case of failure or battery recharge.

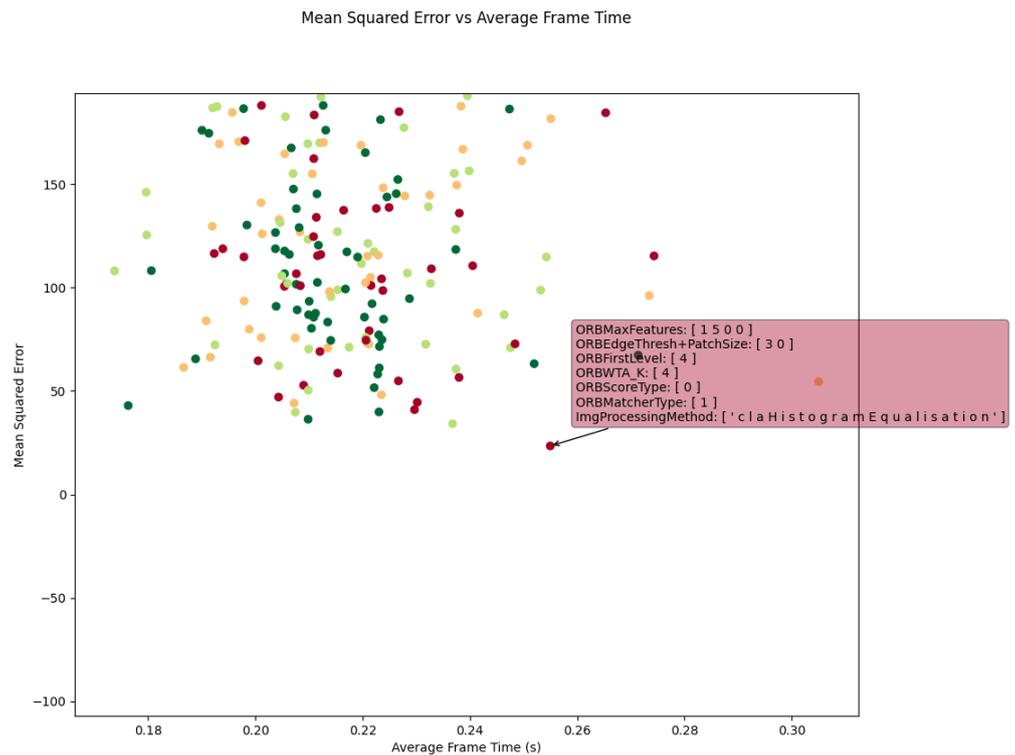


Figure 18. Results of Different Image Processing Techniques and Feature Matching Parameters on the Accuracy of VO Relative to the Structure-from-motion “ground truth”: the test with the smallest error is highlighted and the settings for that test displayed.

581 values. The ORB SLAM 2 code was then modified to include CLAHE image processing
 582 and the calculated ORB feature matching parameters. This was then compared against a
 583 version of ORB SLAM 2 without CLAHE image processing and using ORB-SLAM 2’s
 584 default ORB feature matching parameters. Tests were conducted on both the AQUALOC
 585 and Marine Autonomous Robotics for InterventionS MARIS [57] underwater datasets.
 586 The modified ORB SLAM 2 appeared to yield improved SLAM accuracy, losing tracking
 587 a reduced number of times on each dataset. ORB SLAM 2 ran at usable framerates on a
 588 Raspberry Pi 4 of around 15 - 20 fps, suitable for slow moving AUVs. It is recommended
 589 that ORB SLAM 2 with the provided settings be used as an initial platform on which to
 590 develop further underwater visual SLAM robotic applications.

591 7.3. Testing Acoustic Communication and Ranging

592 The RoboFish prototype uses an M64 Acoustic Modem [42]. Because this modem is
 593 still a Beta version during the initial testing, a number of in-water trials were conducted
 594 to establish whether the two pairs RoboFish uses are working. Both modems were
 595 functional and a point-to-point acoustic link was established and packets transmitted
 596 over it successfully. Apart from minor issues in the beginning, mainly with wiring
 597 and serial port configurations, the modem’s Channel 3, which is between 93.75khz and
 598 125.00khz, offered a very reliable acoustic link over 50-80m range in open water, as well
 599 as inside a compact water tank of 302 litres. Channel 1 had a lower signal strength
 600 causing a shorter range. Channel 4 was more unpredictable, as it worked but with a
 601 shorter range and was slightly unstable. Channel 6-7 were not tested as they would give
 602 a shorter range and not required at this stage. These parallel channels can be used by
 603 RoboFish for networking in the future, as it is possible to switch between channels to
 604 enable communication between more than two modems without packet collisions (but
 605 not at the same time).

606

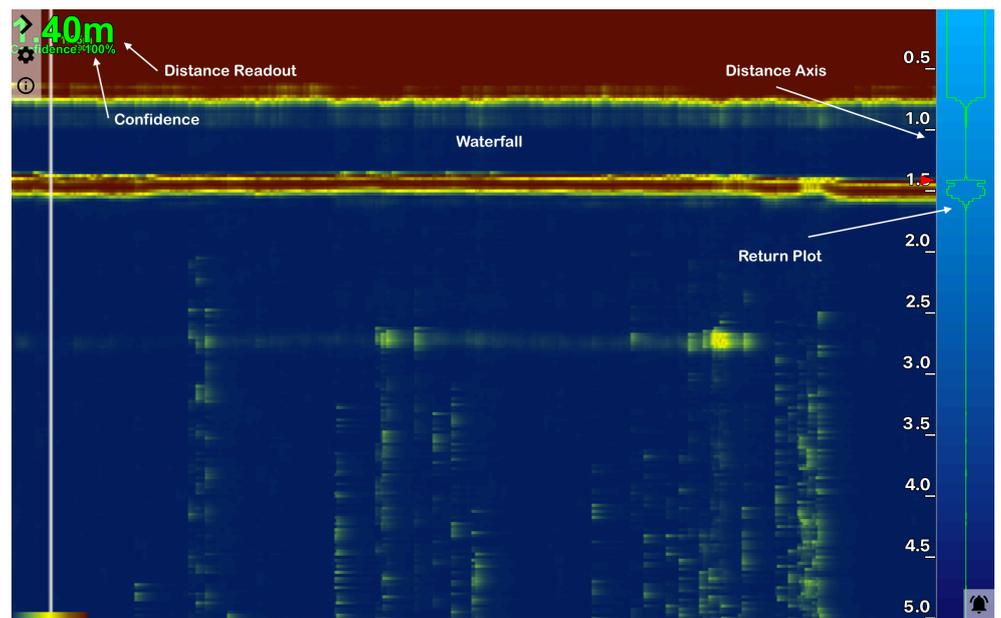


Figure 19. Ping-Viewer Interface to View and Record Ping Data showing Water Depth: consists of four important components (Distance Readout, Distance Axis; echo strength, and 3D trace presenting consecutive profile samples).

607 The minor wiring and interface issues were related to the 3.3V UART to USB serial
 608 converter. A pair of Blue Robotics' BLUART USB to serial converters [58] were used. To
 609 avoid such issues, the converter and the modem need to be common-grounded. The
 610 UART TX from the modem needs to be connected to the UART RX on the converter
 611 board and similarly for the RX pins. The modems need to work in water to avoid
 612 unwanted overheat. A blinking light about every 2 seconds on the modem will indicate
 613 it is powered, but no link is established. The head of the RoboFish is designed so that it
 614 has the modem fitted outside.

615

616 The range finder was also tested and is currently fully operational in RoboFish.
 617 Its readings will be integrated in the final mission oriented control system. Distances
 618 read by this Rangefinder can be read from a displaying interface running on the topside
 619 computer. This window consists of four important components as shown in Figure 19:

620

- 621 • *Distance Readout:* The Distance Readout presents the distance to the target in the
 622 latest measurement. The reading that is shown in Figure 19 was the distance to the
 623 floor in a testing tank during RoboFish's initial trials. The confidence measurement
 624 for the newest range reading is presented below the distance reading and is colour-
 625 coded based on strength as follows: green = 100%, yellow = 50% and red = 0%.
- 626 • *Distance Axis:* This vertical axis represents the distance from the transducer built
 627 in the Echo-sounder. It starts from the top of the window which represents zero
 628 distance from the face of the transducer and runs down vertically with the distance
 629 to the farthest object being at the bottom. Its scale automatically adjusts to indicate
 630 a live scanning range of the rangefinder.
- 631 • *Return Plot:* The Return Plot presents the echo strength against the distance of the
 632 newest profile sample. The stronger an echo is the wider its trace appears.
- 633 • *Waterfall:* The Waterfall is a 3D trace presenting consecutive profile samples. The X
 634 axis is time; and Y axis is new distance reading shifting from right to left as a new
 635 echo arrives.

636 8. Future work

637 The RoboFish prototype is under continuing development. Future versions of a
638 smaller size RoboFish, with particular focus on the modularity of the body design and
639 easy connect/disconnect magnetic joints, will provide a flexible and dynamic platform
640 for numerical data validation and experimental investigation in hydrodynamic labo-
641 ratory testing. This will be highlighted in future projects as this work could not be
642 done under the pandemic restrictions. Anticipated investigations include the analysis
643 of the flow field influenced by different fin and body geometries and kinematic loco-
644 motion parameters, smart soft materials for passively deformed body parts as well as
645 analysis of different actively controlled body kinematics using linear, nonlinear and
646 CPG-based control. This will provide further insight to disseminate the hydrodynamic
647 performance under different flow conditions to prepare for application within complex
648 chaotic and harsh ocean environments. In practical sense, this will especially support
649 the targeted underwater docking, which requires accuracy and reliability of the swim-
650 ming motion. Another direction of future work is to investigate the use of networks or
651 *swarms* of RoboFish carrying out large-scale subsea monitoring or exploration missions,
652 e.g. seafloor mapping, marine archaeology. This will involve a significant challenge in
653 implementing underwater network protocols for cooperative acoustic localisation and
654 navigation, real-time remote control and data gathering from multiple RoboFish.

655 9. Conclusion

656 The work described in this paper led to the development of a fish-like AUV, namely
657 RoboFish, with a bending body that works as a spinal column and able to mimic
658 propulsion techniques of living fish. The first RoboFish prototype was built successfully
659 and was able to complete minimum lake trials. A substantial amount of knowledge
660 was gained from the construction of RoboFish about the technologies that a robotic fish
661 requires to be able to loiter with a camera around complex structures autonomously or
662 remotely controlled over an acoustic link. The use of modular electronics and actuator
663 control algorithms, the networking architecture, the 3D printing approach, and the
664 magnetic joint design are novel contributions to the state of the art that will enable new
665 opportunities. This represents opportunities for additional research arising from further
666 field tests of RoboFish and increases the likelihood of more advanced RoboFish versions.

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669 M.P., J.W. and J.G.; formal analysis, W.G., M.P., J.W. and J.G.; investigation, W.G., M.P., J.W., (M. W.)
670 Marvin Wright, (Y.L.) Yang Luo and (J.K.) Jongrae Kim; resources, M.P., (Q.X.) Qing Xiao and (P.M.)
671 Paul Mitchell; data curation, W.G., M.P., J.W. and J.G.; writing—original draft preparation, W.G.,
672 M.P., J.W., J.G., Y.L., J.K. and (N.M.) Nils Morozs; writing—review and editing, M.P., P.M. and
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691 Abbreviations

692 The following abbreviations are used in this manuscript:

693	AMBA	Advanced Microcontroller Bus Architecture
	AUV	Autonomous Underwater Vehicles
	ASA	Acrylonitrile Styrene Acrylate
	AXI	Advanced eXtensible Interface
	CAN	Controller Area Network
	CFD	Computational Fluid Dynamics
	CSI	Camera Serial Interface
	CPG	Central pattern generators
	FDM	Fused Deposition Modelling
	FSI	Fluid-structure interaction
	FPGA	Field Programmable Gate Array
	GPIO	General Purpose Input-Output
694	IC	Integrated Circuit
	IMU	Inertial Measurement Unit
	KPA	Key Performance Attributes
	MIPI	Mobile Industry Processor Interface
	ORE	Offshore renewable energy
	PCB	Printed circuit board
	PID	Proportional Integral Derivative
	PWM	Pulse Width Modulation
	ROV	Remotely Operated Vehicles
	SoC	System-on-Chip
	SoM	System-on-Module
	SONAR	Sound Navigation and Ranging
	SoC	System on a chip

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