



## Dual-mode terahertz extended interaction oscillator driven by a pseudospark-sourced sheet electron beam<sup>☆</sup>

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### ABSTRACT

A terahertz dual-mode extended interaction oscillator (EIO) driven by a pseudospark-sourced sheet electron beam (SEB) was presented. The major advantages of the newly developed circuit include 1) high-density SEB interacting with the TM<sub>11</sub> and TM<sub>31</sub> modes, respectively, and 2) high output power of over 1 kW at the sub-terahertz frequency range. Two different types of 2π modes and their output characteristics were studied, and the circuit was optimized to ensure efficient outputs of two standing-wave modes. The three-dimensional (3D) particle-in-cell (PIC) simulation predicts the maximum output power of 1.3 kW with a 3-dB bandwidth of ~0.5 GHz at 303 GHz when operating at the TM<sub>11</sub> mode, and 3.18 kW, 3-dB bandwidth of ~0.85 GHz at 364 GHz when operating at the TM<sub>31</sub> mode.

### 1. Introduction

In the recent decades, high-power radiation sources at the millimeter waves and terahertz (THz) radiation frequency bands from 100 GHz to 1 THz have gained significant interest due to their numerous exciting applications, such as broadband wireless and high data rate communications, high resolution radar and imaging, and biomedical and plasma diagnostics [1–6]. Driven by these applications, the THz radiation sources with high output power had made great progress. Among various THz radiation sources, vacuum electronic devices (VEDs) are intrinsically superior with handling high power or high power density due to the electrons moving in vacuum without scattering [2,7,8]. The sheet electron beam extended interaction oscillator (SEBEIO), as an important kind of VEDs achieving high output power and maintaining a compact structure, has gained considerable attention as a promising THz oscillation source due to its feasibility, stability, and high gain per unit length [2,9]. In the THz frequency band, one of the major factors limiting the development of THz devices is the maximum electron beam current density at the interaction region. In our design, a pseudospark-sourced (PS) electron beam was used to drive SEBEIO because of its high current density (10<sup>8</sup> A/m<sup>2</sup>), high brightness (10<sup>12</sup> A/(m<sup>2</sup>rad<sup>2</sup>)), low vacuum requirements, and its propagation with no need for any external focusing magnetic fields [10–14].

A number of SEBEIO experiments have been reported. For example, a W-band extended interaction klystron (EIK) was reported by Pasour et al., which produced 7.5-kW output power. It was driven by a 20-kV, 4-A sheet beam and the efficiency was ~17% [15]. At

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University of California, Davis, a W-band sheet beam klystron with 10-kW output power, 20-ms pulse duration, and 17-dB gain was presented [16]. An extended interaction oscillator (EIO) with  $\sim 10$ -W continuous-wave (CW) output power operated at 220 GHz–270 GHz and an EIK with 25-W pulsed power operated at 250 GHz–276 GHz have been designed by Communication & Power Industries [17]. The high-power W-band SEBEIO with 6-kW maximum output power driven by the 47.2-kV and 2.1-A sheet electron beam (SEB), and more than 1.2-kW average power has been designed and tested by Wang et al. at University of Electronic Science and Technology of China [18]. The researchers at University of Strathclyde presented the SEBEIO output power of over 10 W at a frequency of  $\sim 0.2$  THz and the W-band SEBEIO with the peak output power up to 1.2 kW [19,20]. As discussed in all of the above EIOs and EIKs, they have achieved excellent performance in a single frequency band. However, to develop SEBEIO using the same circuit to work in dual frequency bands is significantly beneficial for reducing the size, cost, and weight of THz sources. This paper introduces the design of dual-mode SEBEIO, which works at both 0.30 THz and 0.36 THz with the tuning bandwidth of 0.50 GHz and 0.85 GHz, respectively, and peak power of more than 1.3 kW.

## 2. Pseudospark-sourced sheet electron beam (PS-SEB)

In the recent decades, the PS-generated high-density and energetic-pulsed electron beam has attracted significant interest due to its potential and growing applications in the areas of high-power radiation generation, extreme ultraviolet (EUV) sources, intense X-rays, free electron masers, and so on [11–14,19–28]. The PS discharge is a self-sustained, transient, and axially symmetric discharge at the low-pressure (50 mTorr–500 mTorr) gas conditions. It has the ability to produce the electron beams combined the highest current density and brightness with low emittance of 15 mm mrad, fast current rise up to  $10^{12}$  A/s, and high power density of  $\sim 10^{19}$  W/cm<sup>2</sup>, which is catered to the requirement for high-power sources of millimeter waves and THz radiation, as well as accelerators, such as backward wave oscillators (BWOs), EIOs, and free-electron lasers (FELs) [29–31]. In recent years, the PS electron beam achieved further progress and various pencil PS discharge electron beams have been investigated by the particle-in-cell (PIC) simulations and experiments [32–36].

Nevertheless, one of the major factors limiting high-power vacuum microwave radiation sources to higher frequencies is the need of transporting beams with higher current density, due to the decrease of high-frequency circuit transverse dimensions with the wavelength. As the frequency of VEDs increasing to 100 GHz or beyond that, the beam diameter has to be approximately one-tenth of the wavelength or less in pencil-beam VEDs. While, the use of SEB can overcome this difficult owing to its larger cross-sectional dimensions. Compared with the pencil beam, the advantage of SEB is that the space charge effect is small and a higher current can be achieved by increasing the width of beam, which helps to increase the output power. It is a challenge for the thermionic cathode to generate a sufficiently high-perveance and uniform beam, since it needs a complicate focusing system to confine SEB. However, it is much simpler in a PS discharge system since a plasma channel formed in the system can confine SEB and has no need for an external magnetic field. In the experiment, a post-acceleration modulator with a cross-sectional size of 1.00 mm  $\times$  0.17 mm of SEB was used, and PS-SEB with a peak current of 21.5 A was measured without an external focusing magnetic field [20]. PS-SEB with the current density of  $\sim 1$  kA/cm<sup>2</sup> has been generated using a sheet beam plasma cathode electron gun [37]. The influence of geometrical design parameters on the high current density PS-SEB has been analyzed by the PIC simulation models and experiments [38,39]. In this article, SEB generated by PS is used to drive the dual-mode SBEIO structure. In our design of the PS discharge system, it has a four-gap PS discharge setup which consists of a hollow cathode (HC) with a central hole and an anode with an aperture to extract the electron beam, as shown in Fig. 1. The anode and HC are separated by the dielectric insulators. The PS discharge occurs under suitable low pressure (typically 50 mTorr–500 mTorr) in the system, as HC is applied with a negative high voltage and the anode is grounded. In the process of the PS discharge, an electron beam with a very large current can be generated. When the high current density and brightness beam propagates through the anode and the interaction circuit, the front edge of the beam ionizes the background gas and generates a plasma channel. Subsequently, beam electrons expel some of the plasma electrons, while the heavier ions remain fixed. Therefore, a positive ion channel is formed to focus the PS electron beam. PS-SEB can be extracted using a collimator with a rectangular aperture placed at the end of the anode. The rectangular aperture of the collimator should be located at the same axial center as the cylindrical aperture of the anode.

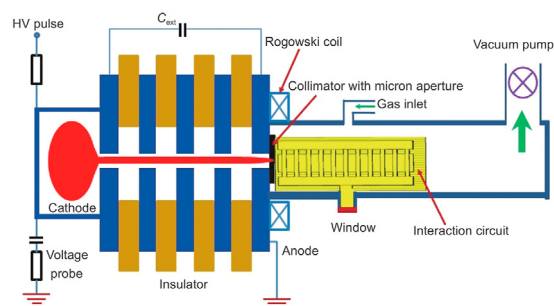


Fig. 1. SBEIO composed of a four-gap PS discharge system and the interaction circuit.

### 3. Design of the SEBEIO circuit

The SEBEIO circuit composes of eleven gaps and two symmetrical coupling cavities on both sides of the structure, as shown in Fig. 2. A 0.90 mm × 0.19 mm rectangular beam tunnel passes through the center of the slots and intersects with the slow-wave structure. It combines the advantages of traveling-wave tubes and klystrons and has the capacity of handling high output power in the millimeter-wave and THz-frequency regimes. EIO, typically, works at the fundamental mode (TM<sub>11</sub> mode), since it is the easiest mode to achieve the start-oscillation condition [20,30,40]. While in recent years, EIO working at the high-order mode has become more and more attractive due to its higher beam power and larger power capacity [41–43].

#### 3.1. Mode analysis

The three-dimensional (3D) SEBEIO model is shown in Fig. 2. The ladder cavity is a periodic standing-wave circuit along the longitudinal direction. Based on the distribution pattern of the axial electric field in the cavity along the transverse direction, the resonant modes of the ladder cavity are usually named as TM<sub>n1</sub> and the index  $n$  is determined by the variation in the distribution pattern of the axial electric field along the transverse direction. The axial electric field distributions of the fundamental mode TM<sub>11</sub> and the high-order mode TM<sub>31</sub> at the cross-section are shown in Fig. 3. The  $E_z$  fields in the TM<sub>11</sub> and TM<sub>31</sub> modes are unidirectional and concentrating at the beam area so that the interaction with the electron beam is effective. The beam-mode coupling is determined by the characteristic impedance  $R/Q$ , expressed as  $R/Q = \frac{\int_a^b E_z dl}{2\omega W}$ , where  $R$  is the equivalent resistance of cavity,  $Q$  is the quality factor,  $\omega$  is the resonant angular frequency, and  $W$  is the stored energy in the cavity, which is a measure of  $E_z$  fields interacting on the electrons. The TM<sub>31</sub> mode provides a stronger electric field concentrating at the tunnel area as well as high  $R/Q$ , as shown in Fig. 3. Table 1 lists the frequencies, inherent quality factors  $Q_0$ , and characteristic impedances  $R/Q$  of the cavity with different modes.  $R/Q$  indicates the strength of the interaction between the electron beam and the high-frequency field in the cavity. A cavity with higher  $R/Q$  has the potential to achieve higher output power. The electric field of the  $2\pi$  mode is in the same direction in each gap as shown in Fig. 4, which contributes to a higher  $R/Q$  value. The  $2\pi$  mode also provides the electric field with the same direction in each gap for sufficient beam-wave interactions, as shown in Fig. 5. The TM<sub>31</sub>- $2\pi$  mode has the highest  $R/Q$ , which is beneficial for SEBEIOs when operating at a high-order mode. Meanwhile, the  $2\pi$  mode corresponds to the largest fundamental spatial harmonic and consequently has the largest structure dimension along the axial direction [44,45].

#### 3.2. Dispersion characteristic

The key issue for EIO operating in a dual-mode condition is the mode competition. An effective method is to make the frequency interval between the operating modes wide enough. Due to the limited periodic structure of the multigap resonant cavity, the dispersion curve consists of a series of discrete frequency points. The dispersion curve of the designed radio frequency (RF) circuit computed by the CST Microwave Studio is shown in Fig. 6. It is an effective approach to identify the possible mode competition and self-oscillation. The red curve with dot markers represents the TM<sub>11</sub> mode, and the blue curve with triangular markers represents the TM<sub>31</sub> mode. The operating voltages of the TM<sub>11</sub>- $2\pi$  and TM<sub>31</sub>- $2\pi$  modes are 18.5 kV–22.5 kV and 27.5 kV–34 kV, respectively, and the synchronous beam voltages are 20 kV and 30 kV, respectively, as shown in Fig. 6. The operating voltage of the TM<sub>11</sub>- $2\pi$  mode is smaller than that of the TM<sub>31</sub>- $2\pi$  mode. As shown in Fig. 6, the 22.5-kV beam line is far away from the TM<sub>31</sub>- $2\pi$  mode point so the competition between these two  $2\pi$  modes can be suppressed. However, the 30-kV beamline intersects with the TM<sub>11</sub>- $17/10\pi$  mode, which indicates the mode competition between these two modes may occur as the oscillation startup condition is satisfied.

The normalized  $E_z$ -field distribution of the TM<sub>31</sub>- $2\pi$  mode along the beam tunnel is significantly stronger than that of the TM<sub>11</sub>- $17/10\pi$  mode, as shown in Fig. 7 (a). Through estimation using the axial electric field, the characteristic impedance  $R/Q$  of the TM<sub>31</sub>- $2\pi$  mode is about 10 times than that of the TM<sub>11</sub>- $17/10\pi$  mode, as shown in Table 1. The normalized  $E_z$ -field distributions of the TM<sub>31</sub>- $2\pi$

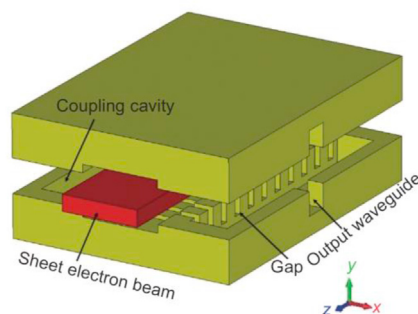


Fig. 2. Schematic drawing of the SEBEIO circuit with eleven gaps.

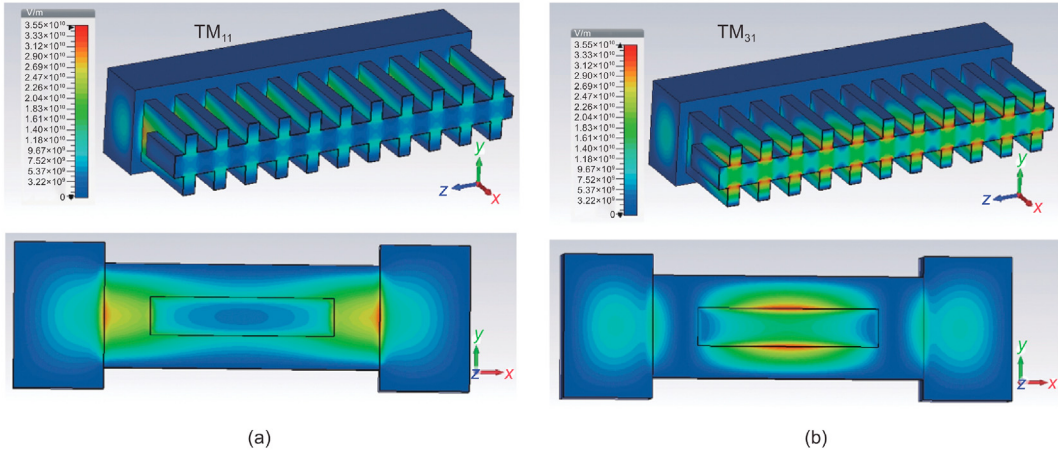


Fig. 3. Electric field magnitude for (a)  $TM_{11}$  mode and (b)  $TM_{31}$  mode at the cross-section.

Table 1

Basic parameters of the eigenmodes.

Mode	Frequency (GHz)	$R/Q$ ( $\Omega$ )	$Q_0$
$TM_{11}-2\pi$	304.1	91	675
$TM_{11}-19/10\pi$	304.9	74	671
$TM_{11}-17/10\pi$	312.1	85	712
$TM_{31}-2\pi$	366.7	865	837
$TM_{31}-19/10\pi$	367.6	702	825

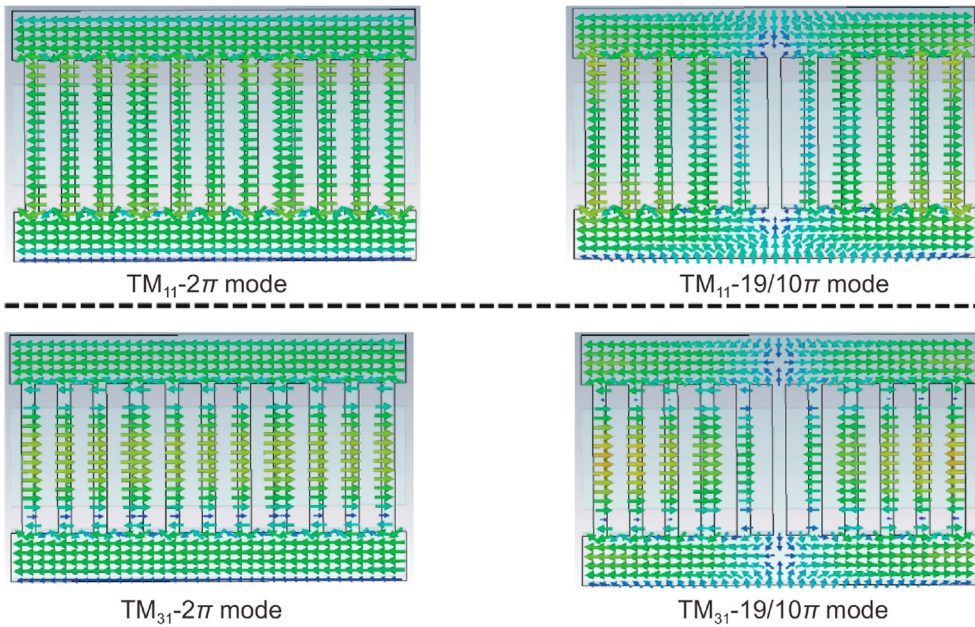


Fig. 4.  $E_z$ -field distributions of  $TM_{11}-2\pi$ ,  $TM_{11}-19/10\pi$ ,  $TM_{31}-2\pi$ , and  $TM_{31}-19/10\pi$  modes along the  $z$ -axis.

and  $TM_{11}-17/10\pi$  modes along the cross-section are illustrated in Fig. 7 (b). In the beam tunnel area, the  $E_z$  field strength of the  $TM_{31}-2\pi$  mode is stronger than that of the  $TM_{11}-17/10\pi$  mode. Reflected from the results of the  $R/Q$  values and field distributions of these two modes, the competition between the  $TM_{11}-17/10\pi$  mode and the  $TM_{31}-2\pi$  mode is hard to be excited.

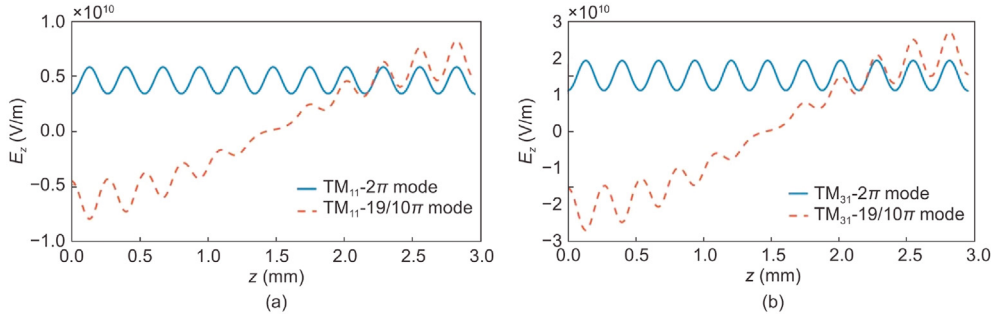


Fig. 5. Normalized  $E_z$  distributions along the  $z$ -axis of (a)  $TM_{11}-2\pi$  and  $TM_{11}-19/10\pi$  modes and (b)  $TM_{31}-2\pi$  and  $TM_{31}-19/10\pi$  modes.

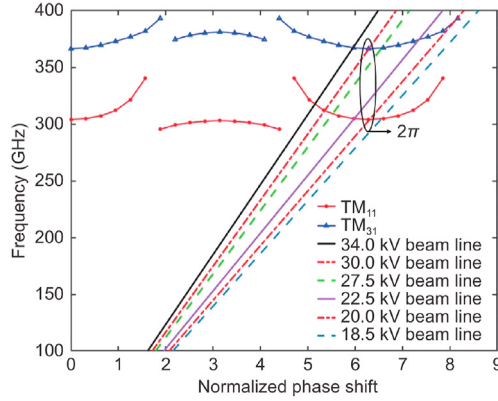


Fig. 6. Dispersion curve of the SEBEIO circuit.

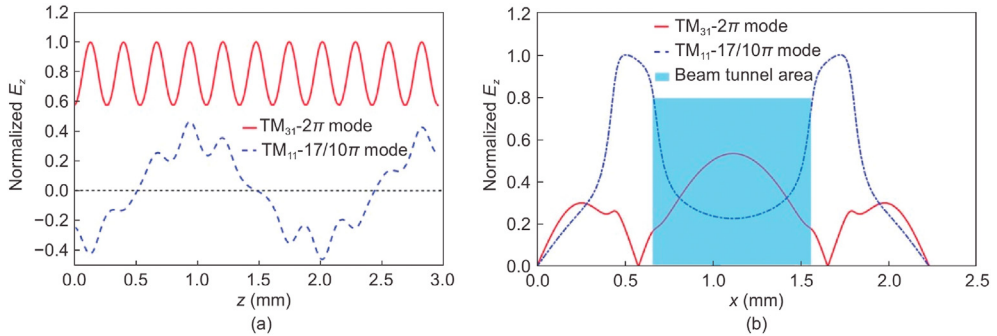


Fig. 7.  $E_z$ -field distributions of the  $TM_{31}-2\pi$  and  $TM_{11}-17/10\pi$  modes (a) along the beam tunnel direction and (b) along the cross-section of cavity.

#### 4. PIC simulation

To validate our design, the 3D PIC simulation was used to demonstrate the performance of the dual-mode SEBEIO. As the operating frequency of VEDs increasing up to the THz range, the Ohmic loss caused by the metal material has a significant impact on the performance. The copper conductivity at the THz frequency range is much smaller than that in the direct current (DC) case. The nonideal surface losses at the THz frequency caused by surface roughness have been reported in Ref. [46]. In our simulation, the conductivity  $\sigma$  of the background material was set as  $1.1 \times 10^7$  S/m ( $< \sigma_{Cu}/5$ ,  $\sigma_{Cu} = 5.8 \times 10^7$  S/m for copper), taking into consideration the Ohmic loss. A beam current of 3 A with the voltages of 24 kV and 37 kV is respectively injected into the interaction circuit. A stable output signal with 51.8 V/79.4 V (equivalent to output power of 1.34 kW/3.15 kW) is obtained at 303.4 GHz/364.5 GHz, respectively, as depicted in Fig. 8. The  $E_z$ -field distributions along the  $z$ -axis demonstrate SEBEIO can operate at the  $TM_{11}-2\pi$  and  $TM_{31}-2\pi$  modes without mode competition, which agrees well with the above theoretical analysis of the circuit's dispersion curve. Fig. 9 shows the output power, frequency, and the starting oscillation time versus the voltage. It predicts that the output power changes from 0.94 kW to 1.34 kW in the voltage range between 23.5 kV and 26.0 kV for the  $TM_{11}-2\pi$  mode, and the output power changes from 1.58 kW to 3.15 kW in the

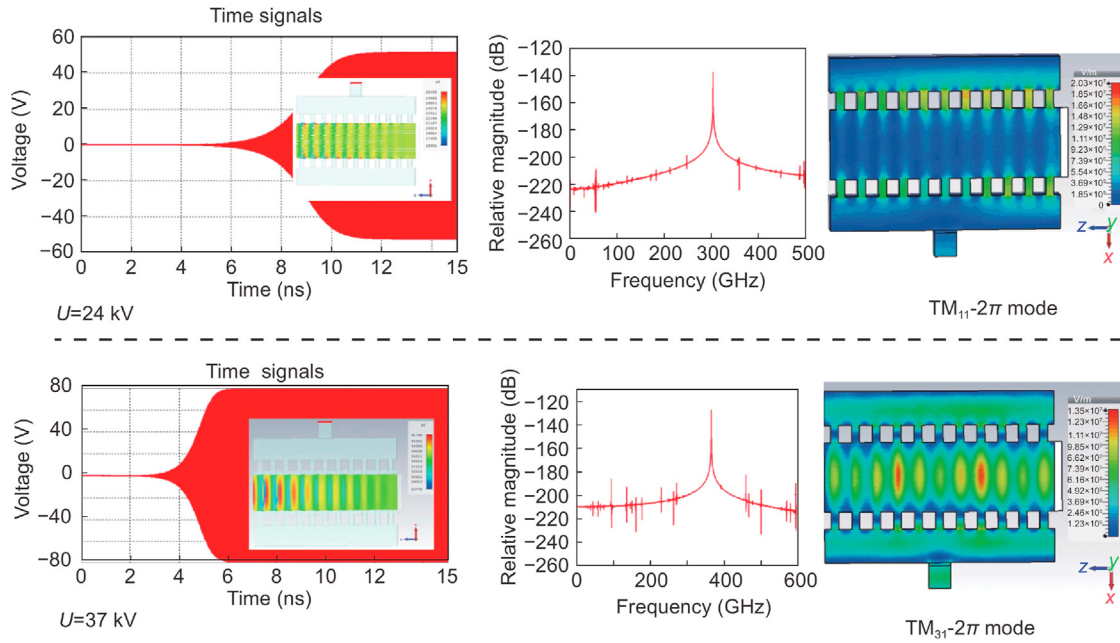


Fig. 8. Simulation results: Output voltage signals (inset: Trajectory of electrons), frequency spectra, and the electric field distributions at the operating voltages  $U = 24$  kV (upside) and  $U = 37$  kV (downside).

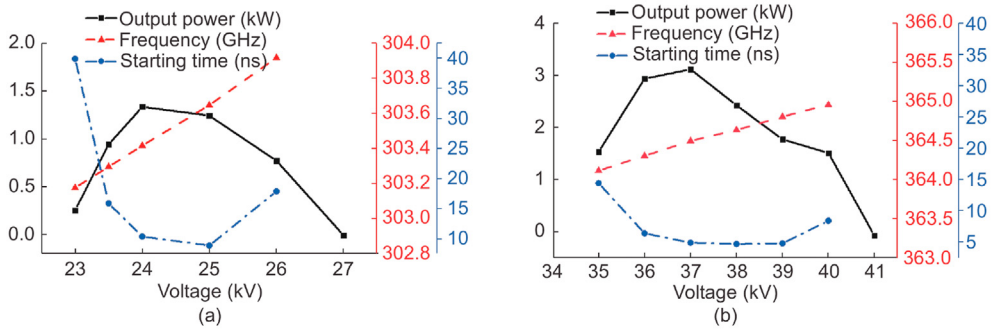


Fig. 9. Output power, frequency, and the oscillation starting time variations with the operating voltage: (a)  $TM_{11}-2\pi$  mode and (b)  $TM_{31}-2\pi$  mode.

voltage range between 35 kV and 40 kV for the  $TM_{31}-2\pi$  mode. The 3-dB tuning bandwidth is about 0.50 GHz and 0.84 GHz for the  $TM_{11}-2\pi$  and  $TM_{31}-2\pi$  modes with the maximum output power up to 1.34 kW and 3.18 kW, respectively. The simulation results show that the designed SEBEIO is stable for the  $TM_{11}-2\pi$  and  $TM_{31}-2\pi$  modes operation.

5. Conclusions

In this paper, the THz dual-mode EIO driven by PS-SEB was presented. Based on the analysis of the dispersion curve of the slow-wave structure and the electric field distribution in the cavity, the mode competition was studied. The PIC simulation predicts stable dual-mode operation, with the maximum output power of 1.34 kW, 3-dB bandwidth of  $\sim 0.50$  GHz at 303.4 GHz when operating at the  $TM_{11}-2\pi$  mode, and the maximum output power of 3.18 kW, 3-dB bandwidth of  $\sim 0.84$  GHz at 364.5 GHz when operating at the  $TM_{31}-2\pi$  mode, respectively. Our next step is to fabricate, assemble, and measure the designed dual-mode SEBEIO to verify the simulation results experimentally.

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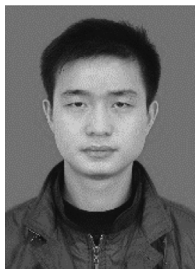
## Declaration of competing interest

The authors declare no conflicts of interest.

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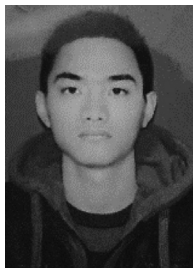




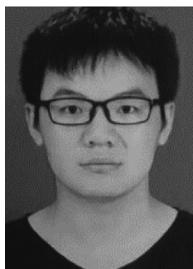
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