# A Controlled CO<sub>2</sub> Release Experiment in a Fault Zone at the In-Situ Laboratory in Western Australia

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#### 17 Abstract

- 18 A controlled-release test at the In-Situ Laboratory Project in Western Australia injected 38 tonnes of
- 19 gaseous CO<sub>2</sub> between 336-342 m depth in a fault zone, and the gas was monitored by a wide range
- 20 of downhole and surface monitoring technologies. Injection of CO<sub>2</sub> at this depth fills the gap
- 21 between shallow release (<25 m) and storage (>600 m) field trials. The main objectives of the
- 22 controlled-release test were to assess the monitorability of shallow CO<sub>2</sub> accumulations, and to
- 23 investigate the impacts of a fault zone on  $CO_2$  migration.
- 24 CO<sub>2</sub> arrival was detected by distributed temperature sensing at the monitoring well (7 m away) after
- approximately 1.5 days and an injection volume of 5 tonnes. The CO<sub>2</sub> plume was detected also by
- borehole seismic and electric resistivity imaging. The detection of significantly less than 38 tonnes of
- 27 CO<sub>2</sub> in the shallow subsurface demonstrates rapid and sensitive monitorability of potential leaks in
- 28 the overburden of a commercial-scale storage project, prior to reaching shallow groundwater, soil
- 29 zones or the atmosphere.
- 30 Observations suggest that the fault zone did not alter the CO<sub>2</sub> migration along bedding at the scale
- 31 and depth of the test. Contrary to model predictions, no vertical CO<sub>2</sub> migration was detected beyond
- 32 the perforated injection interval. CO<sub>2</sub> and formation water escaped to the surface through the
- 33 monitoring well at the end of the experiment due to unexpected damage to the well's fibreglass
- casing. The well was successfully remediated without impact to the environment and the site is
- 35 ready for future experiments.
- 36 **Key words:** CO<sub>2</sub> controlled-release; Western Australia, CO<sub>2</sub> geological storage; fault zone; CO<sub>2</sub>
- 37 monitoring
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#### 39 **1. Introduction**

40 Although adequate site selection and characterisation of a CO<sub>2</sub> storage project will make leakage of

41 CO<sub>2</sub> and migration to the shallow environment unlikely, storage project operators may need to provide

42 adequate monitoring systems for assuring regulators and the public that leakage could be confidently

43 detected, managed and remediated. One of the challenges is the timely identification of leakage, i.e. 44 the ability to detect small volumes of  $CO_2$  as early as possible on its migration path between the

45 storage complex and groundwater resources or the atmosphere (Jenkins et al., 2015). Therefore,

46 monitoring technologies need to be employed that are cost effective and have adequate depth,

- 47 temporal and spatial coverage.
- Previous field tests have focussed on shallow-release experiments performed at less than 25 m depth
  (Roberts and Stalker, 2017; Roberts et al., 2018) or CO<sub>2</sub> storage experiments at more than 600 m depth
  (Michael et al., 2010 and references therein). However, except for a few recent projects in Canada

51 (Macquet and Lawton, 2019) and eastern Australia (Feitz et al., 2018), experiments investigating the

52 migration behaviour and detectability of gaseous  $CO_2$  at intermediate depths between 25 m and 600

53 m have been lacking. More information for this depth interval would be helpful for improving

54 monitoring schemes of large-scale  $CO_2$  storage projects by demonstrating detectability of  $CO_2$  leakage

55 before it reaches potable groundwater or the atmosphere.

56 Furthermore, the identification and characterisation of potential leakage processes and pathways are

57 important for developing properly targeted monitoring schemes (Birkholzer et al., 2014, Michael et

al., 2016). For example, fault zones have been identified as a potential leakage pathway that may

59 concentrate or focus  $CO_2$  migration upward to the shallow subsurface, potentially accumulating in

60 groundwater aquifers or continuing to migrate to the atmosphere (e.g. IPCC, 2005; Lewicki et al., 2007;

Kaldi et al., 2013). Leakage from natural analogue CO<sub>2</sub> stores occurs along faults (e.g. Miocic et al.,
 2016, Roberts et al., 2019 and references therein). Studies of these natural analogues find that faults

are complex and channel fluids heterogeneously at depth and towards the surface (Roberts et al.,

2015) and so understanding of how faults might affect CO<sub>2</sub> leakage is poorly constrained.

65 The CSIRO In-Situ Laboratory Project (In-Situ Lab) is located at the eastern edge of the South West Hub 66 CCS Flagship project (SW Hub) in Western Australia (Figure 1), which has been identified as a potential area for commercial-scale CO<sub>2</sub> storage (Stalker et al., 2013). The storage concept of the SW Hub 67 involves injection of CO<sub>2</sub> into a more than 2000 m deep, 1000 m thick sandstone reservoir, the 68 69 Wonnerup Member of the Lesueur Sandstone, where up to 800,000 t CO<sub>2</sub>/year over 30 years are 70 predicted to be potentially contained, largely due to residual trapping and dissolution of CO<sub>2</sub> in 71 formation water (Sharma and Van Gent, 2019). Given the faulted nature of the storage complex and 72 lack of a conventional seal, it is important to understand the  $CO_2$  migration along faults and the ability

73 to identify and monitor potential leakage pathways for assurance purposes.

74 The In-Situ Lab addresses the two general science gaps related to monitoring leaks from a CO<sub>2</sub> storage 75 complex outlined above. It consists of two wells at approximately 400 m depth drilled into a major 76 fault zone (F10 Fault), which allows performing controlled-release experiments that can reduce 77 uncertainty regarding: 1) the monitorability of shallow, gaseous CO<sub>2</sub> accumulations that may result 78 from leakage from a storage complex, and 2) two-phase flow processes in a fault zone. The project 79 contributes to broadening the global portfolio of controlled CO<sub>2</sub> release tests, with the aim to increase 80 regulators' and the public's confidence in storage safety, and in the protection of groundwater 81 resources and the environment.

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Figure 1. Location of the existing well locations within the proposed greater storage complex. Harvey 2 was drilled in the east
of the study area, where major displacement along the F10 fault forms the eastern boundary to the storage complex. Harvey
2 was backfilled with cement (grey shading) up to a depth of approximately 400 m.

#### 87 1.1 Geological setting

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Previous seismic surveys and analyses of data from four wells (Harvey-1, -2, -3 and -4) drilled for the SW Hub project between 2011 and 2015 (Stelfox, 2017) were supported by a series of research projects (Stalker et al., 2014; Stalker and Van Gent, 2018) and new data from the ISL OB-1 well to provide more detail on the geology of the In-Situ Lab. Harvey-2 was drilled by the SW Hub in the vicinity of the large F10 fault as a data well for the geological characterisation beyond eastern edge of the storage complex.

94 The In-Situ Lab is centred around Harvey-2, which was intended to be recompleted as an injection 95 well. It is situated on a north-west trending broad basement high within the Southern Perth Basin. 96 Faulting is attributed to normal and strike-slip deformation of the Phanerozoic sedimentary cover 97 (Crostella and Backhouse, 2000). The Mesozoic sequence at the In-Situ Lab site comprises Triassic and 98 Jurassic sediments below a significant Early Cretaceous unconformity, overlain by later Cretaceous to 99 recent deposits (Figure 2a). The Middle to Late Triassic Lesueur Sandstone (composed of the lower 100 Wonnerup and upper Yalgorup members) and the Eneabba Formation, the injection interval, consist 101 of fluvial to shallow marine siliciclastic units in the southern part of the Perth Basin (Playford et al., 1976; Mory, 1995; Olierook et al., 2014). Palynology indicates that the base of the Eneabba Formation 102 is intersected in Harvey-2 somewhere between 610 and 730 m, though similarity between the 103 104 sediments of the Eneabba Formation and the Yalgorup Member and tectonic disruption make more 105 precise definition difficult.

Major fault reactivation, block rotation, uplift and erosion occurred across the Perth Basin during the Valanginian (~135 Ma) (Crostella and Backhouse, 2000; Bradshaw et al., 2003). At the In-Situ Lab, the unconformity currently lies at ~200 m below surface (Rockwater, 2015). Above the unconformity the Leederville Formation contains up to 100 m of horizontally bedded, Late Valanginian to Aptian, poorly consolidated, clastics, shales and lignite seams (Playford et al., 1976). The Pleistocene Guildford Formation lies below surficial sediments and disconformably on Leederville Formation strata 112 comprising alluvial sand and clay with shallow-marine and estuarine lenses, with a basal conglomerate

113 (Low, 1971).





115 Figure 2. Geology at the In-Situ Lab site: a. Gamma ray log, palynology and stratigraphy in Harvey-2 (Stelfox, 2017), and b. 116 W-E seismic cross-section through Harvey-2 and across the F10 fault (vertical scale in two-way-time).

117 The Eneabba Formation, the injection target, is interpreted to be a Jurassic continuation of the predominantly fluvial-alluvial to perhaps fluvio-deltaic environment of the Late Triassic Yalgorup 118 119 Member (Timms et al., 2015). Previous analyses of cores from wells in the area have demonstrated 120 that the Yalgorup Member is highly heterogeneous and consists of a lithofacies that can be ascribed mainly to fluvial moderate to high energy river channels and low energy floodplain settings, including 121 paleosols (Timms et al., 2012; Delle Piane et al., 2013; Olierook et al., 2014; Lim et al., 2017). Formation 122 123 Micro-imager (FMI) analysis on the nearby Harvey-4 well, integrated with the natural gamma ray spectroscopy (NGS) tool and bedding dip measurements data have been interpreted into depositional 124 125 environments such as braided bar, point bar, splays, overbank and paleosols, other descriptive

126 interpretation included evaporitic shale and siderite cementation (Roestenburg, 2016). The result is

an interlayered system of low- to high-permeability sandstones and low-permeability siltstones and
 paleosols. The Yalgorup Member and the Eneabba Formation contain lithology with highly variable

129 porosity and permeability (Figure 3).



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131 Figure 3. Porosity versus permeability core analysis data for the Yalgorup Member (modified from Bourdet et al., 2019)

compared to newly measured data from the Eneabba Formation (hollow circles). DMP identifies data provided by the
 Western Australian Department of Mines and Petroleum, which was renamed Department of Mines, Industry Regulations
 and Safety (DMIRS).

As part of the In-situ Lab Project core analyses of the Eneabba Formation from the Harvey-2 drill hole were undertaken. Air permeability was determined with a Hassler flow cell. The resulting porositypermeability values are notably high, with a mean exceeding 5 D and 28 % porosity for the sands (Figure 3). Unsteady-state CO<sub>2</sub>-brine relative permeability analyses were performed for five samples

in the injection interval.

## 140 1.2 Structural characterisation and local stress regime

The main structural feature in the project area is the F10 fault zone. It divides two structural blocks with Harvey-2 penetrating through F10 into the footwall block (Figure 2b) and the other Harvey wells to the west penetrating the hanging wall block (Figure 1). The faults in the Mesozoic sedimentary succession are truncated by the Early Cretaceous unconformity. The main F10 fault displacement is 1600 m at the top Sabina Sandstone, 1000 m at the top Wonnerup Member and 750 m at the top of the Yalgorup Member. Fault movement is interpreted on seismic reflection data as mostly normal. The faults have typical normal fault dips of around 60° to 70°.

148 Approximately 225 m of disaggregation have been interpreted in the ~650 m F10 fault zone 149 intersection in Harvey-2. Disaggregation occurs between lenses of less deformed lithology, including intersections of apparently undeformed sediments. The disaggregated units tend to be sandstones; 150 151 adjacent oxidised hardpans, silty paleosols and silts are more competent at the time of deformation. 152 Once reconstructed, the true thickness of the fault zone in F10 is 200 to 300m, which, based on 153 published data, is typical for a fault of the magnitude of F10 (Childs et al., 2009). Within the reconstructed fault zone there is approximately 70 to 100 m thickness of disaggregated fault rock, 154 155 constituting a guarter to a third of the fault zone thickness. The thickness of disaggregated fault rock would be towards the upper end of the range extrapolated from compiled published fault data (Childs 156 157 et al., 2009). This is potentially due to low effective stress conditions present during shallow faulting.

The occurrence of disaggregation as the dominant faulting mechanism, typical of shallow faulting at depths less than 1 km (Fulljames et al., 1997; Sperrevik et al., 2002; Bense et al., 2013) in Harvey-2 at 849 m depth suggests that, at the In-Situ Lab site, a maximum of not much more than 300 m of Jurassic sediments would have been eroded for the burial depth at the time of faulting to be in the vicinity of ~1000 m.

163 Based on the limited data and previous studies available for the area, the in-situ stress regime at 164 shallow depth in Harvey-2 is a strike-slip fault regime with the major horizontal stress slightly above 165 or equal to the vertical stress. King et al. (2008) determined the vertical, minimum and maximum horizontal stress gradients in the Northern Perth Basin at 400 m depth to be 21.6 kPa/m, 18.5 kPa/m 166 167 and 21.7 kPa/m, respectively. Slip tendency analysis (Morris et al., 1996; Lisle and Srivastava, 2004) was carried out on all the seismically mapped SW Hub faults, however given the orientation of the 168 169 principal stress (105°) in the strike-slip regime and the dominantly N-S orientation of the faults none 170 of the faults in the area are predicted to be close to reactivation (Langhi et al., 2013). In other words, 171 under increasing pressures, new faults would form in the direction of and constrained by the minimum 172 horizontal stress before reactivation of existing faults.

Rock mechanical tests were conducted on several core plugs obtained from the injection zone in Harvey-2. The core materials were extremely weak, and the test plugs had to be frozen during the sample preparation and experimental set up. The stress-strain curves for the two triaxial tests show a highly ductile/strain hardening plastic deformation behaviour. As such, no distinctive peak strength could be identified from the stress-strain curves.

## 178 2. Test design

The In-situ Lab project commenced in May 2018 with the concept of developing an enduring test site
 for controlled CO<sub>2</sub> release experiments in a shallow fault zone by the end of May 2019.

181 *2.1 Concept* 

A controlled CO<sub>2</sub> release test to mimic a shallow CO<sub>2</sub> accumulation in the vicinity of a fault zone was
 designed and conducted for:

- Demonstrating the detection and monitorability of shallow gaseous CO<sub>2</sub> accumulations by testing a comprehensive range of monitoring technologies, and
- Investigating the impact of faults and fault zone geometry on two-phase leakage processes by
   injecting CO<sub>2</sub> into a faulted interval in the Eneabba Formation and monitoring the plume
   behavior.

To achieve these objectives, the In-Situ Lab: 1) recompleted the existing Harvey-2 – primarily for  $CO_2$ injection; 2) drilled and completed a fibreglass geophysical monitoring well ISL OB-1, with behindcasing instrumentation, and 3) drilled and completed a groundwater well in the Surficial aquifer (Figure 4). It should be noted that the focus of the experiment was the monitorability of a  $CO_2$  plume in the shallow subsurface. In this context, the purpose of  $CO_2$  injection was to mimic leakage from a deeper reservoir and secondary accumulation along the leakage path. Therefore, the assessment of induced seismicity or potential fault reactivation, like for example in experiments by Guglielmi et al.

196 (2015), were outside the project scope.

A range of surface and borehole geophysical technologies were deployed to monitor the plume of
 injected CO<sub>2</sub>. Groundwater and soil gas sampling were undertaken for assurance monitoring purposes
 to detect any vertical CO<sub>2</sub> migration to the overlying shallow aquifer or the atmosphere.

- 200 The project planned to inject up to 40 tonnes of CO<sub>2</sub> over 4 days based on operational considerations,
- including the cost and transport of  $CO_2$  to the site, the time available for drilling and completion of the
- wells, as well as for conducting the injection experiment and performing associated monitoring
- 203 activities.
- 204





Figure 4. Schematic of the In-Situ Lab well configuration, experimental set up and monitoring activities (not to scale).

207 From core observations, an 11 m thick sandstone layer, overlain by a 3 m paleosol, was selected as 208 injection interval in Harvey-2 and was perforated in the upper 6 m between 336 and 342 m depth. Due to the resolution of the existing seismic and limited well data, large uncertainty existed regarding 209 210 the detailed fault zone geometry, and, more specifically, how disaggregation and drag has impacted 211 the contiguity and slope of lithostratigraphic layers within the fault zone. While core intersections with 212 visibly disrupted lithology are observed, it is not known whether fault displacements in the vicinity of 213 the release are significant, tens to hundreds of meters potentially, or minor, on the order of a few 214 meters or less. In other words, it was not clear to what extent the relatively low-permeability 215 paleosols would form baffles to the migration of CO<sub>2</sub>. Also, it was not known whether sub-seismic 216 faults, if present, would act as horizontal flow barriers or vertical conduits to CO<sub>2</sub> migration.

- A series of geological models was created to test the unknown fault geometry and properties. Three background lithology permeability scenarios were based on previously tested SW Hub core samples (Figure 3), three fault displacement and location scenarios and two fault permeability scenarios were combined to produce 18 models for simulation.
- A numerical simulation study was undertaken to inform the optimal location for ISL OB-1 and the vertical location of the downhole instrumentation, and to ensure breakthrough of CO<sub>2</sub> occurred within the project timeframe for the test specific CO<sub>2</sub> injection rates and volume.
- 224 The 18 geological model scenarios covering different ranges of permeability configurations for the 225 selected interval and a total injection of 40 tonnes, the extents of CO<sub>2</sub> saturation were computed (Figure 5). All models are based on gamma log correlations and core descriptions from Harvey-2. The 226 range of potential degrees of faulting was represented by varying permeability configurations to 227 reflect different degrees of continuity and structural tilt of the interlayered sandstones and paleosols 228 229 (Figure 4 and b). By the end of CO<sub>2</sub> injection, the most likely distribution of any plume (depicted by yellow colour) would be within 10 m around the well, and over the course of the experiment it was 230 231 predicted to move upwards to at least 325 m depth.
- Based on the likely extent of the CO<sub>2</sub> plume for an injection volume of 40 tonnes, the observation well
- $\label{eq:scalar} ISL \mbox{ OB-1} was located at \mbox{ 7 m from the injection well to maximise the likelihood the CO_2 plume would}$
- be intersected. The CO<sub>2</sub> plume was predicted to migrate vertically for at least 20 m above the injection interval into the paleosol section; hence instrumentation locations and spacings were planned
- 236 accordingly.
- Injectivity estimates based on the geological model and reservoir simulations confirmed that an average injection rate of 0.4 tonnes/hour and a maximum rate of 1 tonne/hour would be achievable. Reservoir pressures were predicted to stay below 4000 kPa and well below fracture pressure. No fracture testing had been performed at the site, and the fracture pressure was estimated from the regional minimum horizontal stress gradient to be approximately 6216 kPa at the top of the injection interval at 336 m depth.



Figure 5. East-west model cross-sections showing two end members of fault zone interpretation correlated with the gamma ray log in and above the injection interval in Harvey-2: A) layered, slightly tilted and B) disturbed layering and drag in faulting direction. C) Likely CO<sub>2</sub> plume distributions after 40 tonnes of injection based on 18 reservoir simulations. The colour scheme reflects the number of model scenarios that predict the presences of CO<sub>2</sub> in each cell. The injection interval is depicted by the red bar between 336 and 342 metres depth.

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250 *2.2 Project timeline* 

Due to a number of constraints the project had to be delivered within a strict timeframe between May 252 2018 and May 2019. For Harvey-2 and ISL OB-1, completion designs were developed that formed the 253 basis for extensive contracting and procurement activities. Permits were obtained for drilling and 254 injection activities by October 2018.

Site preparation and field deployment commenced in November 2018. Drilling and completion of ISL
 OB-1 and the shallow groundwater well, re-completion of Harvey-2, mobilising equipment on site, and

257 baseline monitoring all took place in the weeks leading up to the injection test in February 2019.

CO<sub>2</sub> injection was conducted in February 2019 when 38 tonnes of food-grade CO<sub>2</sub> were injected into
 Harvey-2 over a 4-day period. This was complemented by extensive subsurface and surface monitoring
 activities. While some monitoring activities have been continuing, CO<sub>2</sub> injection facilities were moved
 offsite, and Harvey-2 and ISL OB-1 were flushed with inhibited brine, leaving the In-Situ Lab field site
 ready for future experiments.

## 263 3. Experimental set up

264 The project footprint area is approximately 80 metres by 80 metres and centred around Harvey-2...

265 The surface infrastructure, including  $CO_2$  injection facilities, was installed on a prepared surface of

limestone to absorb spills and provide a uniform surface (Figure 6). The average depth of the

- 267 limestone pad was 30 cm. An on-site tank was installed to store up to 300 m<sup>3</sup> of formation water and
- 268 other wellbore fluids that were produced during well drilling and testing.

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- 271 272

Figure 6. Aerial photo of the In-Situ Lab field site during CO<sub>2</sub> controlled-release experiment.

3.1 Completion and instrumentation of wells

The Harvey-2 well was perforated from 336 m to 342 m depth and an air-lift water production test resulted in an initial average flow rate of 9 L/min. Injection tubing with fibre optic cable for distributed temperature sensing (DTS) and distributed acoustic sensing (DAS), and a pressure/temperature (P/T) gauge was run into the well. An inflatable packer was installed above the perforations.

The ISL OB-1 monitoring well was drilled with a water-based mud to 378 m depth, approximately 7 m to the northeast of Harvey-2. The well encountered some borehole stability issues in the Eneabba Formation identified as breakouts in the caliper log (Figure 7). Open-hole logging was conducted (gamma ray, resistivity, density, neutron porosity, sonic and borehole magnetic resonance) prior to completion activities. Individual sandstone intervals can be correlated at similar depths in Harvey-2 and ISL OB-1 according to the gamma ray responses (Figure 7), showing no obvious vertical structural displacement between the two wells.

The ISL OB-1 well was completed with fibreglass casing and behind-casing monitoring equipment including 4 lines: a) 8 level geophone system with 3C GS-32CT 10 Hz phones at 10 m spacing; b) Electrical resistivity tomography array with 32 S/S take-outs at 3 m spacing; c) TEC line with three piezo pressure & temperature gauges; and d) Dual mode fibre optics for DAS and DTS.



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Figure 7. Selected open-hole log data. Natural radioactivity (GR) log data from Harvey-2 (T1) and log data from ISL OB-1 well
 (T2-T5): Gamma ray (T2), deep (RLLD) and shallow (RLLS) resistivity (T3), caliper (T4) and density (T5). Correlations between
 the base of selected sandstone units (Ss1-Ss6) and depicted by dashed lines between T1 and T2. The location of the perforation
 interval in Harvey-2 is denoted by the red box and coincides with Ss1.

Unfortunately, the wiper plug failed during the cementing of the casing before the cement fully cured, allowing the cement slurry to move back into the well to a depth of approximately 285 m. After considering the risks and various options, a decision was made to slowly drill out the cement inside the casing and logging accessibility down to 350 m was restored. Some small pieces of fibreglass were recovered in the drilling mud, suggesting that the reaming out process caused some damage to the internal lining of the casing. The well was inspected with a camera during the reaming, but only minor

- 299 damage was noted.
- Towards the end of the cementing activity, the three pressure and temperature gauges in ISL OB-1 failed, most likely due to increased temperatures and strain during cement curing.
- A PVC cased shallow monitoring well was drilled to a depth of 27 m and instrumented with a fibreoptic
   cable outside the casing and a P/T gauge to provide continuous monitoring and groundwater sampling
   throughout the project.
- 305 *3.2 Surface injection system*

The surface injection system consisted of an ISO tank to supply liquid CO<sub>2</sub>, a pump to maintain the CO<sub>2</sub> in the liquid phase and provide sufficient pressure for injection; followed by a heater to vaporise the

- 308 pressurised CO<sub>2</sub> prior to entering the well (Figure 8).
- 309 The ISO tank contained food-grade gas supplied from BOC with a nominal pressure between 2000
- 310 and 2400 kPa. At 2400 kPa the vapour/liquid equilibrium temperature is approximately -13 °C. The 311 tank was refilled twice by tanker truck.

- 312 An air-compressor powered AGD-7 gas pump from Haskell which can handle both liquid and vapour
- 313 CO<sub>2</sub> was initially chosen based on piston volume and pressure rating. This pump ended up not 314 achieving the required pump rates and, after first combining it with an ASF-B10 liquid pump, was later
- 315 replaced by a larger ATV-8 liquid pump (Figure 8).
- As the initial reservoir conditions (T = 31 °C and p = 3300 kPa) were subcritical with CO<sub>2</sub> existing within
- the gas phase, a propane-fired atmospheric water bath heater exchange with a rating of 750000
- 318 Btu/hr was used for vaporization. The enthalpy difference at 2400 kPa between -18 °C liquid and 30
- 319 °C vapour is 265000 Btu/kg. At 0.8 tonnes per hour of CO<sub>2</sub>, this corresponds to 212000 Btu/hr of
- 320 heating.



321

322 Figure 8. Photograph showing the surface infrastructure and delivery pathway of the CO<sub>2</sub> injection system.

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## 324 3.3 Monitoring scheme

Monitoring activities during the controlled-release experiment included: 1. Pressure and temperature monitoring for real-time management of the injection operation; 2. Borehole geophysics, fibre optic sensing and logging for detection and spatial delineation of the CO<sub>2</sub> plume; and 3. Near surface assurance monitoring, including passive seismic, atmospheric, soil gas concentration and flux measurements, as well as groundwater sampling to detect any impacts from the operational activities or any anomalous CO<sub>2</sub> from the injection experiment at the surface (Figure 4).

## 331 Pressure and temperature monitoring

332 During the test, wellhead pressure, temperature at various points in the injection line and ISO tank

pressures were recorded and used to calculate CO<sub>2</sub> injection rates. Pressure and temperature were continuously monitored with the p/T gauge in Harvey-2 to ensure the appropriate conditions for

injection of gaseous  $CO_2$ . DTS measurements were taken continuously pre-, during and post-injection

in Harvey-2, ISL OB-1 and the groundwater well.

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#### 338 Borehole seismic

339 The seismic monitoring program was focused on the borehole approach as it is well recognised for the 340 time-lapse observations of a reservoir providing great repeatability (Pevzner et al., 2010; Tertyshnikov 341 et al., 2017; Tertyshnikov et al., 2018). It allows for comparatively fast acquisitions for the repeated 342 surveys and has limited land access issues. The monitoring surveys and a characterisation survey took place from 31<sup>st</sup> of January to 19<sup>th</sup> of February 2019. Both project wells (Harvey-2 and ISL OB-1) were 343 instrumented with fibre optic cables. In Harvey-2 the cable was deployed on production tubing. In ISL 344 OB-1 a hybrid cable containing fibre optics and eight three component geophones, was cemented 345 346 behind the casing. The single mode cores of these cables were utilised for the distributed acoustic 347 sensing (DAS).

Several borehole seismic techniques were applied and trialled during the experiment. The offset 348 349 vertical seismic profiling (VSP) monitoring acquisitions were set up as a series of lines extended from 350 around the ISL OB-1 well within the north-eastern guadrant (due to the permitted land access) and spaced every ten degrees (Figure 9). A low power light seismic source (a 45 kg accelerated weight 351 352 drop) was used for the surveys. The source delivered sufficient energy and frequency content 353 (examples of raw shots are shown in Figure 9) for the shallow depths of investigation and satisfied the 354 low-invasiveness requirements for the farmlands. In total, nine surveys were acquired including the 355 initial baseline dataset. Eight excitations per shot point were performed to increase the signal to noise 356 ratio. The recording parameters for the DAS acquisition were a pulse repetition frequency of 50 kHz,

357 2 seconds record length, and a channel step of 0.5 m.



#### 358

Figure 9. Left: Acquisition map of the offset VSP surveys at the In-Situ Lab research site. Blue points are the shot point
locations. The red point is the Harvey-2 well and the orange point is the location of ISL OB-1. Right: DAS data from the
monitoring well. Gathers (stack of 8 shots): top panel – from one of the near offsets – 40 m; bottom panel – from one of the
far offsets – 180 m.

A 1.2 kJ electrical sparker in ISL OB-1 was utilised to assess the feasibility of the cross-well seismic method paired with DAS in the Harvey-2 well, and data was acquired without interrupting the injection. Cross-hole data was collected daily; the sparker was at the depth range of 60-200 m (with a
 step of 20 m) for each survey, emitting thirty times at every level.

## 367 <u>Electric resistivity imaging (ERI)</u>

Time-lapse detection of changes in electrical properties around the instrumented monitoring well was performed by intensive monitoring immediately before and during the CO<sub>2</sub> injection phase, followed by less frequent post injection surveys. Although a large number of configurations were modelled, data acquisition with the fast dipole-dipole electrode configuration with reciprocal measurements (770 quadrupoles) was selected for deployment. Each survey took approximately 10 minutes, permitting rapid acquisition time and acceptable data quality. Some 145,920 electrode quadrupole measurements were acquired during 135 surveys.

'SYSCAL Pro' was used to acquire data. SYSCAL Pro electrical resistivity measurement equipment was
deployed to the site that accepted 72 channels (e.g. wires from 72 electrodes) via three militarystandard style plugs (i.e. each plug accepting 24 channels). Connection of the 32-channel downhole
electrode array to the SYSCAL Pro required design and manufacture of a "patch box". The patch box
splits wiring for electrodes 1 to 24 into the first plug (channels 1-24) and a further 8 wires to channels
25 to 32 onto the second plug. The patch box was designed to facilitate on-site modification to wiring
as required.

## 382 <u>Downhole logging</u>

Induction logs were obtained ten times in the cased ISL OB-1 well and pulsed neutron (PN) logging was obtained before and after the  $CO_2$  injection in Harvey-2 well (above the perforation zone) and in ISL OB-1 (post-injection only down to 280 m depth). The logs were used to monitor possible timelapse differences in water saturation.

## 387 Assurance monitoring

While deemed extreme unlikely based on the site geology, difference in water salinity between the injection interval and the surficial aquifer, and reservoir simulations, the potential for migration of CO<sub>2</sub> to groundwater or the atmosphere needed to be considered for regulatory compliance. Cement bond logs were run that confirmed contiguous cement fill along the wellbore. Continuous DTS monitoring as well as groundwater and soil gas sampling was performed for detecting potential CO<sub>2</sub> vertical migration along microchannels between the cement and the well casing or between the cement and the rock.

395 The air and soil monitoring activities commenced a month prior to injection and details are provided 396 by Myers et al. (2020). Data on both the  $CO_2$  concentration and flux was collected using a range of 397 automated and manual approaches. The carbon dioxide concentration in the air directly above the 398 soil surface was periodically measured around the site using a Picarro-based mobile system whereas 399 the CO<sub>2</sub> concentration in the vicinity of the injection and ISL OB-1 monitoring wells were determined 400 using permanently mounted Li-COR (Li-840A) analysers. In addition, gas sampling of the soil vadose 401 zone was performed and samples were submitted for carbon isotope and gas composition analysis. 402 In terms of soil flux measurements, these were made near the wells (i.e., injection, monitoring and 403 groundwater) and at a more distant reference location using a permanent solar powered/battery 404 system that comprises a Li-COR (Li-8100A) analyser with four semi-permanent flux chambers whereas regular soil flux surveys at gridded locations (typically 5-10 m spacing) were achieved with a West 405 Systems portable analyser over an area of approximately 50 m x 70 m located around the monitoring 406 407 well.

Three groundwater sampling campaigns took place before CO<sub>2</sub> injection started at Harvey 2 (between November 2018 and January 2019), three during the injection period and five after injection finished (February - March 2019). Analyses included field parameters, major and minor ion concentrations, alkalinity, dissolved CO<sub>2</sub> concentration, carbon isotopes, and total inorganic carbon (TIC)/total carbon (TC)/total organic carbon (TOC).

413 Three component seismic recorders were installed across the well site and on the nearby farmland to 414 monitor the injection-related seismicity and any other relevant seismic activity. Each of the seismic recorders was comprised of a three component (vertical, north and east) 15 Hz seismic sensor (GS-415 416 One), a digitizer with built-in GPS receiver (Geospace GSX), and a battery unit. The sampling rate of the signals in the digitizer was set to 500 Hz with continuous recording. The GPS unit regularly received 417 418 time-stamp from corresponding satellites and used this information to self-correct the electronic time 419 drift due to the heat fluctuations. Stations were distributed to cover both the immediate injection 420 area and far field to have an even coverage. Out of 30 stations, 9 were installed at a single point, with 421 an approximate distance of 400 m away from the injection point; a closer location was not feasible 422 due to existing infrastructure and disturbance by surface activities and on the well pad. These tightly 423 clustered stations were used to increase the signal-to-noise ratio of the recorded signals in the 424 analyses.

## 425 4. CO<sub>2</sub> controlled release experiment

This section describes the CO<sub>2</sub> injection experiment and presents some initial monitoring results and
 preliminary discussion, while detailed interpretation of the extensive monitoring data sets and
 modelling are ongoing activities to be reported in the future.

## 429 4.1 Injection operations

Injection started 5<sup>th</sup> February and concluded on 9<sup>th</sup> February with a total volume of 38 tonnes injected
over 101 hours, corresponding to an average injection rate of approximately 0.4 tonnes per hour.
Pressure measurements at the wellhead (WHP) and at reservoir level (BHP) in Harvey-2 were used to
monitor and guide injection operations (Figure 10). The anticipated injection pressures for the
experiment were modelled to be below 4000 kPa at the injection interval and an injection rate of up
to 1 tonne/hour.

After an initial pressure increase associated with the flushing of the water present in the well, the
WHP and BHP stabilised at around 3500 kPa and 4000 kPa, respectively (Error! Reference source not
found.). The WHP was higher than predicted (which minimized the presence of liquid in the pumping
system) indicating in a lower than desired injection rate (approximately 0.1 tonnes/hour).

The initial AGD-7 gas pump was combined with an ASF-B10 liquid pump approximately 24 hours after injection started without delivering an appreciable improvement in injection rate. Approximately 6 hours later (30 hours) this system was replaced by a larger ATV-8 liquid pump increasing injection rate initially to 0.4 tonnes/hour. However, the rate declined to 0.25 tonnes/hour due to operational problems related to the heater and pump. As a result of the initial increased injection rate, the WHP and BHP increased to 4000-4500 kPa and 5000 - 5500 kPa, respectively. No change of injection rate was observed after refilling the ISO tank (42 hours).

The BHP increased steadily until a leak in the injection line caused injection to be paused at 58 hours
for 8 hours. As expected, the BHP declined while injection was stopped. During this time a needle
valve connected to a redundant pressure gauge and impeding flow was removed from the wellhead.
Injection recommenced at 66 hours and an approximately 0.8 tonnes/hour injection rate was

achieved. Rates were reduced to 0.6 tonnes/hour to enable continuous injection prior to the second
refilling of the CO<sub>2</sub> tank. After the refill (at 88 hr), injection rates reached 1 tonne/hour at a maximum
WHP of 5500 kPa, corresponding to a maximum bottomhole pressure of approximately 6600 kPa
(Figure 10).





#### 456

457 Figure 10. History of wellhead pressure, cumulative injection volume and injection rate (top), correlated with observed
 458 reservoir pressure (bottom) in Harvey-2 and with operational activities and selected incidents.

Temperatures at the wellhead ranged widely between 85 °C at low injection rates and 20 °C at high injection rates (Figure 11). Bottom hole temperature remained relatively constant during injection between 27.5 and 30 °C, slightly lower than the initial reservoir temperature of 31 °C. For these temperatures and most of the observed pressures the CO<sub>2</sub> exists as a vapour. However, at bottomhole pressures above 6000 kPa, CO<sub>2</sub> is injected close to the liquid-vapour line and observed temperature decreasing to as low as 24 °C indicates occasional two-phase conditions for short time towards the end of injection.

- 466 At 94 hours, ISL OB-1 was observed to be flowing water, BHP had exceeded 6200 kPa at that point in 467 time. While monitoring of pressure, DTS and DAS continued, injection was stopped at 101 hours in 468 response to an eruptive release of formation water and CO<sub>2</sub>.
- All unnecessary personnel were removed from site and the well was allowed to depressurise naturally
  by a total of seven eruptive releases in form of geysering that occurred over a period of 12 hours. Once
  the periodicity of the expulsions had been ascertained, the well was closed with a high-pressure cap
  115 hours after start of injection.
- The well has since been remediated and cemented back above the leakage point to a depth of 280 m. 473 474 The CO<sub>2</sub> was back-produced from Harvey-2 to avoid corrosion of the tubing and casing, leaving largely 475 residual and dissolved CO<sub>2</sub> in the formation. Continuing monitoring includes surface CO<sub>2</sub> flux 476 measurements (particularly around the injection and monitoring well), groundwater sampling, 477 reservoir pressure and temperature in the injection well (Harvey-2) and downhole measurements in 478 ISL OB-1 using the fibre optics (DTS and DAS). There is no indication from DTS, induction or PN logging 479 of  $CO_2$  migration above the injection zone at 336 m depth. Six months after ceasing injection, no  $CO_2$ 480 concentrations above baseline have been detected in the groundwater well or at the ground surface.



#### 482



Figure 11. Variation of pressure and temperature during CO<sub>2</sub> injection. Left: Pressure versus temperature variations measured at the wellhead and bottom of Harvey-2 showing impact on CO<sub>2</sub> density (CO<sub>2</sub> density contours and vapour-liquid line are based on Span and Wagner, 1996). Right: DTS data along the length of Harvey-2 for various times during the controlledrelease experiment. 0 hrs: start of injection, 54 hrs: during injection of hot CO<sub>2</sub> gas, 97 hrs: during high-rate injection of relatively cool CO<sub>2</sub> (< 30 °C) and liquid phase event, 101 hrs: towards the end of the experiment, and 125 hrs: one day after the end of injection.

489

#### 490 4.2 Distributed temperature sensing (DTS)

491 The DTS provided very accurate, robust and detailed information about each stage of the CO<sub>2</sub> injection test. The installation at Harvey-2 provided insides into the temperature profile and variation of CO<sub>2</sub> 492 493 properties in the injection well (Figure 11, right). The observed temperature changes correlate very 494 closely to the pressure, flow rates and the heater performance. When the heater is delivering a 495 gaseous  $CO_2$  at high temperature, the excess temperature is dissipated in the upper section of the well (54 hrs in Figure 11, right). The temperature profile then follows a similar gradient as the baseline 496 temperature. Occasionally, with high flow rate and heater not performing at maximum capacity, the 497 injection temperature gradient is steeper than the baseline gradient with temperatures as low as 25 498 499 degrees at the bottom of the well (97 hrs in Figure 11, right), indicating the presence of a liquid phase at bottom hole depth. This condition is present in the well for several hours but then injection of pure 500 501 gaseous CO<sub>2</sub> is reinstated as reflected by the temperature profile at 101 hours the end of injection. 502 One day after injection has ceased (125 hrs in Figure 11, right), the temperatures have returned to 503 baseline conditions for the lower 200 m of the well.

504 DTS in ISL OB-1 (Figure 12) allowed the identification of CO<sub>2</sub> arrival as well as the characterization of 505 the in-well leakage events in both time and space. The evolution of temperature changes (expressed 506 relative to baseline) is presented for a selection of depths from the ISL OB-1 data set (Figure 12). At 507 30 hours after start of injection, the first increase in temperature occurred at 335 m (immediately below the sealing paleosol) indicating the first arrival of  $CO_2$  after approximately 5 tonnes of injection. This coincides with a sharp increase in bottom hole pressure by approximately 1000 kPa in response to the higher injection rates after replacing the pump (Figure 10). Joule-Thomson heating due to the increase in pressure in the injection interval could explain why  $CO_2$  arriving at ISL OB-1 is warmer than at the point of injection. No temperature changes were observed above the paleosol at 331 m, indicating a lack of vertical  $CO_2$  migration beyond the injection interval at that time.

514 After 54 hours, increased temperatures can be seen at 341m and 356 m and the rate of temperature 515 began to increase between 335 and 341 m, which is interpreted as an up to 5 m thick accumulation of 516 warm CO<sub>2</sub> below the paleosol. A sharp temperature increase can be observed at 88 hours at 331 m depth, corresponding to a slight drop in temperature at 341 and a decline in temperature from 356, 517 518 while the temperature at 335 continued to rise steadily. This event is interpreted to coincide with CO<sub>2</sub> 519 and formation water entering the well through the damaged fibreglass casing. Cooling at the top of the well (1 m depth in Figure 12) is probably due to opening of the wellhead and water flowing from 520 the well (at 88 hours in Figure 10). The 7 expulsion events of formation water and  $CO_2$  are reflected 521

522 by cyclic temperature changes (from 100 – 115 hours) at all depths at and above the injection interval.





524

Figure 12. Temperature difference at selected depths in ISL OB-1 during and post injection from 5<sup>th</sup> February to 11<sup>th</sup>
February 2019. The 1 m, 51 m and 152 m data are chosen to show the general temperature range down hole at 50 m
intervals. The data gathered at 335 m is just below the paleosol interval and near the top of the perforated interval. Data
for 341 m is within the perforated interval and 356 m is some 14 m below the base of the perforated interval.

529

The well geysering can be explained by a two-phase flow process (flashing) in which CO<sub>2</sub> comes out of
 solution as the fluid rises in the well. CO<sub>2</sub> solubility in water is observed to decrease with reduction in

532 pressure and temperature as the water rises (Lu et al., 2005; Watson et al., 2014).

533 4.3 Borehole seismic

The pressure data, physical observations and distributed temperature data observations are supported by the borehole seismic results. Offset VSP data are of good quality and a high level of repeatability was achieved that enabled the detection of a small amount of the injected  $CO_2$ , even in anticipation of a relatively low signal. The signal to noise ratio was significantly improved by stacking the shot points located around the monitoring well at the constant nearest offset (40 m) to produce an effective zero-offset VSP geometry in a single ensemble. The reliability of the time-lapse seismic

images depends on many factors: changes in the media, the fidelity of sources' and receivers' 540 541 positions, and consistency of the source signature. The normalised root mean square (NRMS) 542 parameter is a measure of consistency. The NRMS is 0 when two datasets are identical, 140 in the 543 case of random noise, and 200 for a dataset with opposite polarity (Kragh and Christie, 2002). The 544 NRMS estimate between the baseline and the eighth monitor dataset (after injecting 38 tonnes of 545  $CO_2$ ) in Figure 13d are attributed to the high repeatability rate reached, even considering relatively low power seismic source used for the survey. The wavelet for deconvolution was estimated for each 546 547 shot location and vintage separately. Figure 13 (a-c) shows deconvolved gathers of the baseline data, 548 data from the eighth monitor vintage) and their difference. Data is normalised over all three sections 549 for display purposes, and the remains of the direct on the difference section are visible but very 550 insignificant with respect to initial amplitudes. A clear manifestation of the time-lapse signal is 551 observed on the difference section at the target depth (highlighted by the red arrow). Slight 552 differences in the images to baseline can be seen as early as the fourth monitor vintage at which point 553 7 tonnes of CO<sub>2</sub> had been injected after 44 hours.

554



555

Figure 13. Time-lapse images of the CO<sub>2</sub> plume on VSP sections. a) baseline seismogram; b) monitor 8 seismogram; c)
differences of the baseline and monitor data; d) NRMS estimate between baseline and monitor 8 datasets. Red arrow
indicates clear response from the injected gas.

559

560 Due to issues related to faulty connections during the installation of the hybrid cable, the cemented 561 geophones were not active for every survey, and as such data analysis was primarily focused on DAS 562 data. It would be desirable to increase signal to noise ratio of the active seismic data to elevate the level of detectability that could be achieved by introduction of a more powerful source. In the future, 563 continuous recording with the behind-casing sensors would provide significant advantages for 564 565 observation of various aspects of the experiment as well as microseismic monitoring. Alternative approaches of reverse VSP for similar shallow rapidly developing processes should be discussed as it 566 567 allows extremely fast acquisition of a single vintage and use of high frequency downhole sources.

568 Implementation of the cross-well approach suffered from operational noise caused by the injection

569 process in Harvey-2 impacting the signal, hence the analysis of these data has been problematic.

570 Alternatively, the cross-hole approach should be considered in a number of passive observation wells,

571 or during breaks in the injection operations.

## 572 *4.4 Electrical resistivity imaging*

573 Excellent survey repeatability was achieved by this method and details are provided by Harris et al. 574 (2019). Significant changes in dipole-dipole apparent resistivity were observed at the injection interval 575 from 82 hours after the injection of 25 tonnes of  $CO_2$ , and it is possible to identify changes in apparent 576 resistivity close to the injection depth interval (336 – 342 m). Whether these resistivity changes are 577 due to the presence of  $CO_2$  or flow of formation water is under investigation. It should be noted that 578 the limitation of these results is largely due to the electrode spacing having been designed for

## 580 4.5 Downhole logging

581 Induction logs showed no changes in either deep or shallow resistivity above 345 m between the 582 baseline log and the first six runs during the injection. The log obtained post injection shows significant 583 change in resistivity due to the change of the environmental parameters. However, the calibrated log 584 shows no difference with the baseline obtained prior to CO<sub>2</sub> injection down to the 330 m.

585 Pulsed neutron logs obtained in ISL OB-1 and Harvey-2 show only small changes in water saturation 586 above the injection zone. This may be interpreted as CO<sub>2</sub> saturation of less than 10% at each well, 587 however, this is unlikely as other observations do not show any sign of vertical CO<sub>2</sub> migration. If those 588 changes are caused by CO<sub>2</sub> migration, one would expect the differences to increase over time and be 589 more reliably detectable above the perforation zone.

#### 590 *4.6 Assurance monitoring*

Apart from the elevated CO<sub>2</sub> levels which were observed for a very short period in the soil surface around the ISL OB-1 monitoring well due to the well geysering, no anomalous CO<sub>2</sub> has been detected up to two months post injection. The measured CO<sub>2</sub> soil flux and concentration four weeks post injection are within the range of baseline levels observed prior to injection. Parts of the surface monitoring program (i.e., Li-COR, West Systems, soil-gas sampling) will continue for a significant period after injection.

597 Based on the groundwater monitoring results, groundwater in the Superficial aquifer within the study 598 has a salinity above 5000 mg/l and is suitable for irrigation and livestock purposes only. In contrast, 599 formation water salinity in the  $CO_2$  injection interval, the Eneabba Formation, is on the order of 25,000 600 mg/L and too high to be suitable for any use. No significant changes in the water chemistry in the In-601 Situ Lab groundwater well were observed during the monitoring period suggesting that injection of 602  $CO_2$  into the Eneabba Formation had no impact on the Superficial aquifer.

The discharge from ISL OB-1 during geysering was initially borehole fluid (freshwater), followed by formation water (~25,000 mg/L) and  $CO_2$  plus some minor amounts of drilling fluid and formation sand. Based on the volume of the well and  $CO_2$  solubility, the total volume of formation water which spilled onto the limestone pad was estimated to be <20,000 L and the volume of  $CO_2$  emitted to atmosphere less than 2 tonnes.

The relatively high levels of ambient seismic noise and low number of sensors prevented passive seismic from picking the onset of any events during the injection experiment. In the future, the number of elements of the array should be increased and augmented with three components downhole sensor deployment. The deployment of a large N type array will help the identification of the coherent energy packet with higher confidence.

613

## 614 **5. Discussion**

## 615 5.1 Fault zone structure

616 Stratigraphic correlations using log data from Harvey-2 and ISL OB-1 do not show any structural vertical displacement between the two wells at the depth of injection. This confirms that in this area 617 618 the paleosol at the top of the injection interval is contiguous and forms a barrier to vertical  $CO_2$ 619 migration. Concentration of carbon dioxide within a thin interval is also confirmed by the borehole 620 seismic as there is only a reflection like time-lapse signal observed at the injection depth, but no 621 signal above. However, the new well and the controlled release experiment did not provide further 622 details on fault zone geometry. Additional high resolution seismic targeting the 0-400 m depth 623 interval is required for improving the structural interpretation of the test site.

## 624 5.2 Injectivity estimation

Based on the limited data from the short water production and injection tests prior to CO<sub>2</sub> injection,

a productivity index (PI) for the perforation interval was estimated to be on the order of 0.01

m<sup>3</sup>/day/kPa. This compares to a theoretical PI of 1.5-2.0 m<sup>3</sup>/day/kPa assuming a 5 Darcy
 permeability and 6 m thickness of the perforated interval.

629 Applying the analytical method from Mathias et al. (2008,2009) confirms that a reduced

630 permeability on the order of 30 mD is needed to explain the high bottomhole injection pressures

during the controlled-release experiment. Bottomhole pressures for average rates of 0.1, 0.4, 0.6

and 0.8 tonnes/hour were estimated at 3922, 5307, 6100 and 6830 kPa, respectively for a 6 m

633 injection interval, a constant temperature of 29 °C, an initial reservoir pressure of 3300 kPa, and a

634 porosity of 25 %. These pressure values fall within a comparable range to the observed reservoir

pressures in Figure 10 for the respective injection rates. It should be noted that this analysis assumes

constant fluid and rock properties, does not account for thermodynamic effects and buoyancy, and
 the high compressibility of gaseous CO<sub>2</sub> may lead to a slight overestimation of bottomhole pressures

638 (Mathias et al., 2009).

The reasons for the very high skin factor above 100 were assessed by investigating the drilling

history of Harvey-2. Harvey-2 was initially drilled for collecting geological data including core, and
 the well was not planned to be used as a fluid producer or injector. The well was left uncased below

642 207 m for an extended period of time for logging and coring activities, and wellbore stability issues

643 were managed by increasing mud weights to up to 1.17 SG. The resulting mud cake in the injection

interval is estimated to be up to 750 mm in diameter, which is more than double the 290 mm target
 penetration of the perforating gun. Future experiments will require remediation of the injection

646 interval (e.g. air lift juttering, acidization) or establishment of deeper perforations beyond the mud

647 cake.

648

# 5.3 Pressure and temperature evolution

The understanding of the injected gaseous CO<sub>2</sub> has greatly benefitted from the downhole and 649 650 geophysics monitoring. However, the lower than expected injectivity has created interesting well 651 thermodynamics challenges that would need to be taken into consideration in the interpretation and the integration of the downhole dataset in view of the interpretation of CO<sub>2</sub> injectivity and the 652 CO<sub>2</sub> plume imaging. The temperature monitoring shows that thermal effects are non-negligible and 653 must be considered in reservoir simulations, at least close to the injector. A preliminary analysis of 654 the pressure and temperature evolution from Harvey-2 shows that phase transition occurs in the 655 wellbore during later stages of injection. As already pointed out when listing the limitations of the 656

- analytical reservoir calculations in the previous section, coupled non-isothermal wellbore-reservoir
   simulations are required to adequately model the observed pressure and temperature evolution,
   and the migration of CO<sub>2</sub> during the controlled-release experiment.
- 660 5.4 Contribution to the Shallow Release Portfolio
- The test at the In-Situ Lab addressed several gaps regarding shallow-release experiments noted inRoberts and Stalker (2017), with respect to:
- Depth; the test was conducted significantly deeper than most shallow release experiments;
   336 m rather than <25 m.</li>
- Top seal; the absence of a thick regional shale in this area means that industry, regulators and public all have an interest in understanding the behaviour of a potential leak and how the top seal, in this case paleosols, might behave if CO<sub>2</sub> leaked, if the site becomes a future commercial-scale operation.
- Volume; 38 tonnes in this single experiment is approximately 4 times larger than for any previous site where shallow release experiments took place (Ginninderra; Roberts and Stalker, 2017 and references therein). Of the reviewed experiments, 82.8 tonnes CO<sub>2</sub> had been injected in total. Only the CaMI project in Canada has been injecting at comparable rates of approximately 0.4 t/day over a longer timeframe at a depth of approximately 300 m (Goodarzi et al., 2019).
- Identification of leakage; as little as 7 tonnes CO<sub>2</sub> was imaged at a depth of 336 m in one of the earlier seismic vintages and the 38-tonne plume was observed in the later seismic vintages. First arrival was observed within 30 hours by DTS.
- 678 One of the main issues identified in Roberts and Stalker (2017) was the leakage of  $CO_2$  along wellbores 679 or pipelines constructed to introduce the  $CO_2$  or to monitor it underground. In this experiment 680 wellbore leakage was encountered in the fibreglass cased ISL OB-1 monitoring well. DTS and DAS 681 provide a comprehensive data set for better understanding and ongoing modelling of the thermo-682 hydrodynamics of flow processes inside a well, and for monitoring the remediation operations.

## 683 6. Summary and conclusions

The objectives of the In-situ Lab CO<sub>2</sub> controlled-release test were to assess the monitorability of shallow, gaseous CO<sub>2</sub> accumulations, and to investigate two-phase flow processes in a fault zone.

## 686 6.1 Monitorability of shallow gas accumulations

- The test has demonstrated that DTS and downhole seismic were able to detect a plume of less than 687 688 38 tonnes of gaseous CO<sub>2</sub> at approximately 336 m depth. To this point, it is a qualitative observation and more work is needed for determining the lateral extend of the plume and its thickness away from 689 690 the observation well. It still provides a valuable complement to the existing suite of shallow release 691 data sets by investigating the processes associated with the accumulation of gas in the overburden 692 above a potential commercial-scale injection site. It demonstrates the ability to monitor CO<sub>2</sub> 693 accumulations previously not investigated in very near surface release experiments or deep storage 694 test.
- The detectability of the plume has been largely successful by casing-conveyed instrumentation, while wireline time lapse logging and ERT could not be adequately assessed due to limited access to or

697 insufficient vertical resolution across the interval of interest during the test. The continuously 698 recorded pressure and temperature data at the injection depth in Harvey-2 and DTS data from Harvey-699 2 and ISL OB-1 provide a comprehensive data set for detailed interpretation of  $CO_2$  behaviour during 700 the shallow release experiment and calibration of reservoir simulations. Coupled non-isothermal 701 wellbore-reservoir simulations will be performed to adequately model the observed pressure and 702 temperature evolution, and the migration of  $CO_2$  during the controlled-release experiment.

The detectability of such a small amount compared to a commercial scale injection (i.e., 800,000 t/year over 30 years has been deemed feasible for the SW Hub; Sharma and Van Gent, 2019) is a promising achievement regarding the monitorability of potential leaks in the shallow subsurface before detection at the ground surface. However, the controlled release experiment was focussed on a relatively small area and an engineered location. More research needs to be done on improving detectability but also monitoring instrumentation for detecting more dispersed leakage, both laterally and vertically.

No anomalous  $CO_2$  has been detected in the groundwater or the soil up to two months after the injection test. DTS data in the three wells and PN logging in ISL OB-1 have not detected any  $CO_2$  above

injection test. DTS data in the three wells and PN logging in ISL OB-1 have not detected any  $CO_2$  above the injection interval, suggesting that the injected  $CO_2$  has not migrated vertically from the injection

zone in the vicinity of the wells.

## 7146.2 Impacts of the fault zone geology

715 The second part of the experiment was to investigate two-phase flow processes in a fault zone. The

geological data and the simulations predicted the injected  $CO_2$  to migrate vertically through the

paleosol due to the fault related disturbed nature of the sediments. However, the paleosol at the top of the injection interval proved less permeable than expected from core testing and, in contrast to the

719 modelling predictions, the injected CO<sub>2</sub> did not migrate vertically.

While existing seismic and observations from Harvey-2 core show that the main fault displacement lies between approximately 400-600 m depth at the location of the controlled-release experiment, the location and configuration of smaller faults in the wider fault zone remains uncertain. Higherresolution seismic would provide a more detailed model of the fault zone structure.

Lower than expected injectivity and lack of vertical hydraulic communication resulted in higher than
 expected injection pressures, temporarily rising to within the fracture pressure range. However, no
 fracturing events have been recorded by the deployed monitoring techniques.

## 727 6.3 Well leakage

The high injection pressures, laterally focussed migration of the injected CO<sub>2</sub> along the base of the paleosol, and likely weakening of the fibreglass integrity during the cement drilling, resulted in a casing leak at 336 m depth in ISL OB-1.

Although the leak in the fibreglass casing was accidental, there were no adverse environmental impacts. The resulting geysering of the well provides important information to inform the risks associated with CO<sub>2</sub> accumulations in the shallow subsurface environment (approximately 50 times volume increase of CO<sub>2</sub> between 400 m depth and the ground surface) and contains valuable insights into quantifying the volumes of CO<sub>2</sub> and water that may be produced in such an event.

## 736 *6.4 Concluding remarks*

The In-Situ Lab forms an enduring and unique research facility for further research into the monitoring
 and characterisation of CO<sub>2</sub> migration in fault zones and from the shallow groundwater environment
 to the ground surface. Near-term improvements to the site include well remediation activities to

improve injectivity and new, high-resolution seismic for better characterisation of the fault zone
 geometry. Demonstration of successful monitoring technologies in such setting is important for
 increasing public and regulator confidence in the ability to confirm the safety of CO<sub>2</sub> geological
 storage.

744

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