

# 9 W average power, 150 kHz repetition rate diamond Raman laser at 1519 nm, pumped by a Yb fibre amplifier

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Commercially available pulsed fibre lasers at  $\sim 1.5 \mu\text{m}$  have many uses in imaging, defense, communications and light radar (LIDAR) [1]. For 3D scanning LIDAR, higher signal-to-noise ratio requires lasers with high average power and high pulse repetition rate (ideally several MHz) for faster scanning rate, whereas to improve distance resolution requires pulse durations  $< 10 \text{ ns}$  [2,3]. One limitation of the pulsed fibre lasers at  $\sim 1.5 \mu\text{m}$  is scaling to high average powers [4]. Raman frequency conversion of high average power fibre master oscillator power amplifier (MOPA) systems at  $\sim 1 \mu\text{m}$  is a potential alternative. The large Raman shift and Raman gain of diamond allows two-stage Raman conversion to  $\sim 1.5 \mu\text{m}$  for  $\sim 1 \mu\text{m}$  pumping [5]. Excellent thermal properties make diamond suitable for high average powers [6]. Much work has been done on conversion of  $1.064 \mu\text{m}$  lasers to  $1.485 \mu\text{m}$  using diamond [7]; however, the “eye-safety” requirements for LIDAR typically call for wavelengths above  $1.5 \mu\text{m}$ , due to the order of magnitude higher Maximum Permissible Exposure limit [8]. Developing such a diamond Raman laser (DRL) was the major motivation for this research.

Experimentally a DRL at  $1.519 \mu\text{m}$  was pumped by a maximum of 50W of power from an Yb fibre MOPA emitting polarized 15-ns pulses at  $1.082 \mu\text{m}$  with 150 kHz repetition rate [9]. The MOPA’s linewidth of 0.18 nm was comparable to the diamond’s Raman linewidth. The pump beam was focused to  $90 \mu\text{m}$  radius in a 4 mm long diamond crystal. The 15 mm long DRL cavity consisted of a plane input coupler and a 50 mm radius of curvature output coupler. The input coupler was highly reflective at  $1.2 \mu\text{m}$  and  $1.5 \mu\text{m}$  and highly transmissive at  $1.08 \mu\text{m}$ . The output coupler had a transmittance of 70% at  $1.52 \mu\text{m}$  and was highly reflective at  $1.2 \mu\text{m}$ . The diamond was supplied by Element 6 (UK) Ltd. and had an absorption coefficient of  $< 0.005 \text{ cm}^{-1}$  at  $1 \mu\text{m}$  and was oriented for propagation along the  $\langle 110 \rangle$  axis. The pump was polarised along the  $\langle 111 \rangle$  axis of the diamond and the mode sizes for 1<sup>st</sup> and 2<sup>nd</sup> Stokes were  $90 \mu\text{m}$  and  $100 \mu\text{m}$  respectively.

The maximum power achieved from the DRL at  $1.52 \mu\text{m}$  (Fig. 1 (b)) was 9 W (Fig. 1 (a)) with a pulse duration of 7 ns (Fig. 1 (c)). The maximum conversion efficiency was 23% (Fig. 1 (a)). The slope efficiency was 29% before the plateau at 40W of pump power. The high-power roll-over may have been caused by the pump beam quality degradation, either in the MOPA or in an isolator that was used to block the back reflected pump emission. Funding: EP/P00041X/1, EPSRC EP/P001254/1. Research data: doi.org/10.15129/b17b6db6-7c52-46a3-b13a-f89b61e38c0c

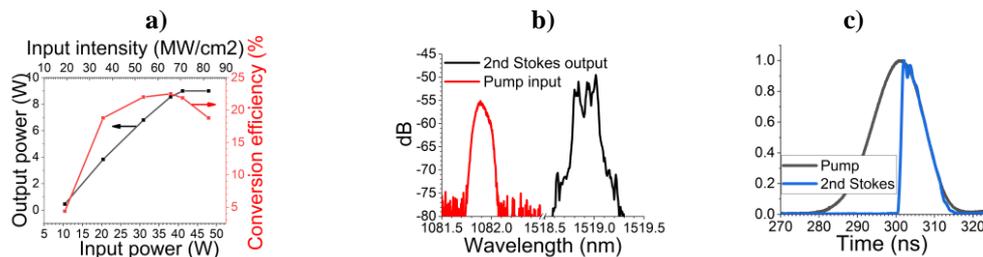


Fig. 1 Power transfer and energy conversion (a), pump and output spectra (b) and 2<sup>nd</sup> Stokes pulse (c)

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