



Radice, G. and McInnes, C. R. (2003) Autonomous behavioural algorithm for space applications. Aeronautical Journal, 107 (1074). pp. 521-527. ISSN 0001-9240 ,

This version is available at <https://strathprints.strath.ac.uk/6242/>

Strathprints is designed to allow users to access the research output of the University of Strathclyde. Unless otherwise explicitly stated on the manuscript, Copyright © and Moral Rights for the papers on this site are retained by the individual authors and/or other copyright owners. Please check the manuscript for details of any other licences that may have been applied. You may not engage in further distribution of the material for any profitmaking activities or any commercial gain. You may freely distribute both the url (<https://strathprints.strath.ac.uk/>) and the content of this paper for research or private study, educational, or not-for-profit purposes without prior permission or charge.

Any correspondence concerning this service should be sent to the Strathprints administrator: strathprints@strath.ac.uk

Autonomous behavioural algorithm for space applications

G. Radice and C. R. McInnes

Department of Aerospace Engineering

Glasgow University

Glasgow, UK

ABSTRACT

The purpose of this paper is to present a new approach in the concept and implementation of autonomy for autonomous spacecraft. The one true ‘artificial agent’ approach to autonomy requires the spacecraft to interact in a direct manner with the environment through the use of sensors and actuators. Rather than using complex world models, the spacecraft is allowed to exploit the dynamics of its environment for cues as to appropriate actions to take to achieve its mission goals. The particular artificial agent implementation used here has been inspired by studies of biological systems. The so-called ‘cue-deficit’ action selection algorithm considers the spacecraft to be a non-linear dynamical system with a number of observable states. Using optimal control theory a set of rules is derived which determine which of a finite repertoire of behaviours the spacecraft will perform. A simple model of a single imaging spacecraft in low polar Earth orbit is used to demonstrate the algorithm.

NOMENCLATURE

b	battery charge deficit
C	cost function
H	Pontryagin state function
\mathbf{I}	inertia matrix
k	resource accessibility

m	data recording deficit
Q	resilience
r	resource availability
t	data transmission deficit
u	control function
\mathbf{x}	state vector
λ	co-state vector
θ	attitude angle vector
$\dot{\theta}$	attitude rate vector
$\dot{\omega}$	angular velocity vector

1.0 INTRODUCTION

The development of autonomy technologies is the key to three vastly important strategic technical challenges facing future spacecraft missions. The reduction of mission operation costs, the continuing return of quality science products through increasingly limited communications bandwidth and the launching of a new era of solar system exploration, beyond reconnaissance, characterised by sustained presence and in depth scientific studies. New deep space missions, coupled with the challenge to do things ‘faster, better, cheaper’ have highlighted the need for increasingly more autonomous spacecraft and rovers. Spacecraft autonomy will bring significant advantages by improving

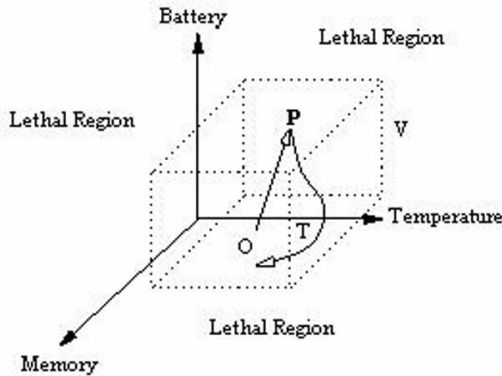


Figure 1. An example of a possible three-dimensional state space with local origin O . The current state is indicated by the vector P . The boundary volume V separates the possible state values from the lethal limits. T is a possible trajectory the satellite could take within the region.

resource management, increasing fault tolerance and simplifying payload operations. Also, when considering the communication delays in deep space missions, the requirement for autonomy becomes clear. Ground stations and controllers will not be able to communicate and control distant spacecraft in real-time to guarantee precision and safety. There is a need therefore to provide autonomous and semi-autonomous computational capabilities to enable further deep space missions.

One approach to autonomy is concerned with the modelling and building of adaptive autonomous agents, which are systems that inhabit a dynamic, unpredictable environment in which they try to satisfy a set of goals. This behaviour oriented approach is appropriate for the class of problems that will face the new generation of micro-satellites currently under development for Earth monitoring and interplanetary missions. These missions will require a high degree of autonomy to meet stringent cost and performance goals. An autonomous micro-spacecraft has multiple integrated tasks such as navigation, battery charging, etc. Similarly neural network, fuzzy logic and expert systems, although successful in some terrestrial fields, such as camera focusing, automobile cruise controls and subway automation, are extremely difficult to validate to ensure the survival of the spacecraft and are software intensive. In contrast recent developments in Artificial Agents borrow heavily from ethology where the agents respond directly to environmental stimuli. The satellites are situated in their environment, orbiting a planet, and connected to its problem domain directly through sensors and actuators. It then has to monitor the environment and determine in isolation what the next problem or goal to be addressed is.

In the approach presented in this report such an artificial agent is proposed that provides a method for action selection that balances the demands of the satellite users – gathering or transmitting data – and the actions necessary to guarantee the survival of the spacecraft – charging the battery and thermal control. The spacecraft is modelled as a non-linear dynamic system with a state space consisting of key internal parameters such as battery charge, memory level and internal temperature. The state space will have a set of lethal limits that define the useful operating domain. A finite repertoire of behaviours is then used to generate a set of actions to control the internal dynamics of the spacecraft. A cost function, which provides the measure of the deviation of the spacecraft from its normal equilibrium state space operating point is then generated. Applying Pontryagin's maximum principle from optimal control theory we obtain a set of optimal action selection rules. The action selection algorithm must then maintain this equilibrium in the presence of perturbations due to the spacecraft's own behaviour or from environmental change. For example switching on the heater during eclipse will maintain the internal temperature level, but at the same time drain the battery charge.

2.0 THE AGENT AS A STATE SPACE

The state space model for agents was proposed by Sibly and McFarland^(1,2) and further developed by McFarland and Houston⁽³⁾. Within this framework the agent is characterised as possessing a minimal set of internal variables that can completely describe its state. In such a description of a biological system we could possibly identify hunger, thirst, temperature, hormone level, etc, as essential physiological state variables. The first to develop this model for a spacecraft was Gillies *et al.* who identified three state variables as being essential: energy, measured through battery level, internal temperature and memory level⁽⁴⁾. These variables sit within an Euclidean vector space with the states as its orthogonal axes as shown in Fig. 1.

Within this space there will be regions that the satellite can physically never encounter, for instance negative memory or negative battery level, and regions, that should the satellite cross into, it would cease to function, such as below the lower or above the upper possible operating temperatures. The boundaries that separate the regions that are fatal to the satellite from those that are not are called lethal limits. The task of the spacecraft within such a model is therefore to maintain the homeostasis (equilibrium) of its state variables under the perturbation of its own behaviour, and the environment's impact on its resources. For example during eclipse the satellite must activate the heater to stay above the lower lethal temperature, while also draining the battery. In the robotics literature each axis is associated with a specific task the agent has to perform⁽⁵⁻⁷⁾. However this is not the case for the spacecraft model. The temperature axis bounds the operational limits for the different subsystems, but is not directly part of the action selection algorithm.

The spacecraft will be able to perform useful work to sustain its viability, by either obtaining images through a payload camera, or gathering data through some appropriate payload instrument, and then storing the data on a hardware device, or downloading, by means of a transmitter, the recorded data to an Earth ground station. Both activities do however require a certain amount of energy to be consumed, draining the battery level. To replenish its energy source the spacecraft must point its solar array towards the Sun, thus recharging the depleted battery. We can see therefore that the spacecraft is subjected to three different types of behaviour: target pointing, ground station pointing, and Sun pointing. The temperature seems to bear no importance within the state space since it is not directly related to any particular behaviour. However, it has to be noted that temperature plays a fundamental role in space mission design. All hardware devices work within well-defined temperature limits. It is therefore vital for the mission's success that the internal temperature is kept within a predefined range to ensure that all subsystems function properly. The spacecraft is therefore equipped with a heater, which automatically switches on when the temperature reaches a certain lower limit; clearly this requires a certain amount of energy. The temperature therefore is not linked directly to a behaviour, but indirectly affects the spacecraft's behaviour selection.

3.0 THE OPTIMALITY CRITERION

It has been shown that the spacecraft's state can be represented in an n -dimensional space. The state can be thought of as a specification of the value of n variables, where n is large enough to characterise the satellite. The model incorporates a very simple relationship between behaviour and state. It is assumed that when the spacecraft is performing activity u_i , the rate of change of the state x_i ($i = 1-n$) is given by:

$$\dot{x}_i = -r_i = -c_i u_i \quad \dots (1)$$

This means that activity u_i , has consequences only along axis x_i . The value of r_i in this model represents the 'return' the satellite gets from performing activity u_i mediated through a constant parameter c_i which links the sensitivity of a variable in relation to an activity.

It seems reasonable to assume that the risk of failure, must increase steeply the nearer a state variable is to its lethal boundary. For example it is obviously dangerous to allow the battery charge to approach lethal levels if a future energy supply is not guaranteed. This suggests a cost function of the form:

$$C(x) \propto x^2 \quad \dots (2)$$

The choice of a quadratic function has been made for mathematical simplicity, although clearly any convex function may be used⁽⁸⁾. It has to be noted that the cost function has the desirable property that the cost of possessing any particular deficit increases more rapidly the further away from the homeostatic equilibrium point the satellite's variable lies. When more than one state is being considered, some assessment of the total cost $C(x)$ must be made. If $C(x)$ can be represented as the sum of the cost associated with each x_i in x ($i = 1-3$), then $C(x)$ is said to be separable. This means that the risk associated with the value of one variable is independent of the values of the other variables. So the cost $C(x)$ of being in state z is a weighted sum of the squares of the displacements that constitute x . For example if $x = [x_1, x_2, x_3]$ then:

$$C(x) = \frac{x_1^2}{Q_1} + \frac{x_2^2}{Q_2} + \frac{x_3^2}{Q_3} \quad \dots (3)$$

where the weighting parameters Q_i ($i = 1-3$) are referred to as the resilience of the state variable⁽⁹⁾. The optimality criterion then amounts to requiring the spacecraft to spend its time in such a way that the displacements from the homeostatic position results in the smallest possible cost.

To complete the specification of the optimisation problem we then have to resort to Equation (1) to link the satellite's behaviour to consequences for its state. If during some time span the duration of time spent performing activity u_i is d_i then the total consequence of such a behaviour for axis x_i will be $d_i r_i$. In other words if x_i began at a value $x_i(0)$, its value at the end of the time span considered $x_i(T)$ will be given by $x_i(T) = x_i(0) - d_i r_i$. Therefore at the end of the time span considered the state of the spacecraft will have resulted in a deficit for that axis. As will be seen d_i plays a fundamental role in the action selection algorithm

3.1 Dynamic optimisation

We will now consider dynamic problems, in which any action taken at any given time has consequences, which are evaluated over some period of time into the future. In this case the problem is to look at the cost associated with different paths through some state space. The optimal solution will be the one along which the total accumulated cost is least. Finding this total cost involves the mathematical operation of integration.

The optimal control problem can now be defined. We have an objective function $C(x, u, t)$ dependant on the state variable x , and the behavioural control u . The aim is to move the system, to a specified state or for a specified amount of time, such that the integral of the objective function is minimised. A technique that is applicable in such cases was developed by Pontryagin in the 1950s⁽¹⁰⁾. Pontryagin approached the optimal control problem by defining a state function called the Pontryagin (also know as Hamiltonian) function denoted by H . Pontryagin's maximum's principle states that the problem of finding the path of least cost is equivalent to the more direct problem of instantaneously maximising the function H – the principle can also be considered as an instantaneous minimisation.

A constraint is however introduced by the method itself as the dynamic problem of optimal control must represent the fact that the state variable x and the control variable u that constitutes the instantaneous cost function cannot be varied independently. The reason for the dependence is the fact that u controls x , the nature of this control being given by the system equation – Equation (1).

Pontryagin's function can therefore be thought of as the gradient of the cost functional, that is to say H indicates how cost varies with

a chosen control at any given position of time. Let us now sum up the principle: In order to minimise the total cost $\int_{t=0}^T C(x, u, t) dt$, the control the control law u must be chosen in such a way as to instantaneously maximise the Pontryagin function:

$$H = \lambda^T f(x, u, t) - C(x, u, t) \quad \dots (4)$$

where $C(x, u, t)$ is the objective function giving the total cost, $f(x, u, t)$ represents the system equation. Here λ represents the change in total future cost along the optimal trajectory that results from a small change in state and is called the costate vector. It is, in effect, a set of Lagrange multipliers, introduced to satisfy the system equation constraint. The rate of change of both the state and costate vectors are then given by the following equations⁽¹¹⁾:

$$\dot{x} = \frac{\partial H}{\partial \lambda} \quad \dots (5)$$

$$\dot{\lambda} = -\frac{\partial H}{\partial x} \quad \dots (6)$$

This formulation will be used later to determine the spacecraft's optimal behaviour.

3.2 Availability and accessibility

Two parameters, the availability r and the accessibility k model the resources in the environment. This duality may seem arbitrary, and r and k should be united into one single variable. However, these two parameters provide a powerful way with which to consider the environment. The availability is associated with the density of the resource in the environment. The accessibility is associated with the ease with which an agent can obtain the resource through its own behaviour. Applying these definitions to the spacecraft problem allows us to assess the environmental resources at hand for the spacecraft. The availability and accessibility will be associated with the different behaviours the spacecraft is capable of performing. Charging the battery, recording and transmitting data, will therefore all have an assigned accessibility and availability. The spacecraft is equipped with sensors – Sun sensor, and GPS – that determine the availability r_i of any resource ($i = 1-n$). For example when the satellite detects, via its Sun sensor, that it is in sunlight $r_{sun} = 1$, while we will have $r_{sun} = 0$ if the satellite is in the eclipsed arc of its orbit. The ground station availability will be $0 < r_{ground\ station} \leq 1$ when the satellite detects through a global positioning system or up-link signal, that the ground station is present, otherwise $r_{ground\ station} = 0$. Similarly if the satellite is in sight of the target area $0 < r_{target} \leq 1$ and $r_{target} = 0$ if not. The rate at which the satellite can perform a certain task is modelled by the accessibility k_i ($i = 1-n$) and is associated with the ease with which the spacecraft can obtain a resource through its behaviour. For example the rate k_{sun} at which the satellite can charge the battery by pointing towards the Sun is the maximum array power output. If the solar array is damaged then k_{sun} is lowered: for example if 50% of the array fails at $t = t_{failure}$, then $k_{sun}(t_{failure}) = 0.5k_{sun}(t_{launch})$. Similarly we will have $k_{ground\ station}$, and k_{target} which are defined by hardware constraints before launch and determined by the maximum data rates for acquiring and down-linking data. Should the satellite suffer an antenna, transmitter or payload instrument failure, these parameters would be lowered accordingly.

3.3 Optimal behaviour

We now have all the tools to determine the optimal behaviour the agent will perform at any given time. The solution obtained from Pontryagin's maximum principle (the optimal behaviour) depends on the conditions constraining the satellite's behaviour⁽⁸⁾. There are four

important constraints that need to be considered:

1. The impossibility of performing behaviour at a negative rate implies that $u_i(t) \geq 0$.
2. Behaviours are rate limited, so that the agent cannot work faster than some limiting rate defined by the accessibility k_i , therefore $u_i \leq k_i$.
3. The rate of performing a behaviour is defined by $\dot{x}_i = -r_i u_i$, for availability r_i where \dot{x}_i is the rate of change of the state x_i ($i = 1-n$).
4. The satellite can perform only one behaviour at a time. For example, if the spacecraft is pointing towards the Sun for battery charging it cannot downlink to the ground station or activate the payload.

This last point is worth looking at more closely. Let us consider the case of an animal which allocates a proportion of time s to feeding; then a proportion $(1-s)$ will be available for drinking. This, assumes that drinking and feeding are the only two behaviours that the animal performs. If feeding occurs at a maximum rate, then the rate of feeding at that stage is sk_1 . In general, considering condition two we can say that $u_1 \leq sk_1$ and $u_2 \leq (1-s)k_2$, which can be expressed, taking into account condition one as:

$$0 \leq \frac{u_1}{k_1} + \frac{u_2}{k_2} \leq 1 \quad \dots (7)$$

The optimal behaviour therefore requires the controls u_i to maximise H subject to the constraints 1-4 introduced previously. The optimal control strategy is to set $u_1 = k_1$ and $u_2 = 0$ if the current state of the agent is to the left of the switching line and $u_1 = 0$ and $u_2 = k_2$ if the current state is to the right. Therefore we will have the two following situations:

Perform behaviour 1 at rate k_1 if $\lambda_1 r_1 k_1 > \lambda_2 r_2 k_2$

Perform behaviour 2 at rate k_2 if $\lambda_2 r_2 k_2 > \lambda_1 r_1 k_1$

Thus the optimal trajectory heads towards the switching line – where $\lambda_1 r_1 k_1 = \lambda_2 r_2 k_2$ – and then follows it to the origin. Moreover if we look at how we defined the Pontryagin function, Equation (10), and how the costate vector λ is defined, Equation (8), we can introduce a new parameter called deficit which is defined as⁽¹²⁾:

$$d_i = \frac{\partial C}{\partial x_i} \quad \dots (8)$$

and therefore if we consider the two competing behaviours as eating and drinking we will have:

Eat at rate k_1 if $d_1 r_1 k_1 > d_2 r_2 k_2$

Drink at rate k_2 if $d_2 r_2 k_2 > d_1 r_1 k_1$

This solution combines the agent's state with the parameters that describe the environment. The interesting property to note is that the structure of the rule does not change depending on the type of cost function chosen. The cost function acts simply as a scaling factor to the state variables. We can therefore say that the optimal behaviour is to perform an activity at the maximum rate at which it is available and a choice made between behaviours. Therefore, the choice between feeding and drinking should be made according to whether the product of deficit \times availability \times accessibility is greater for food or water. Several examples of this motivational behaviour have been studied in the animal kingdom⁽¹³⁻¹⁶⁾. This switching rule now forms the basis for the spacecraft action selection algorithm.

3.4 Satellite action selection algorithm

We can now apply what we have introduced previously to the case of an autonomous agent, and in particular to the case of an autonomous satellite. For a spacecraft possessing the three essential state variables discussed earlier: battery charge, memory level and internal temperature, the cost function has been determined to have the following expression⁽⁴⁾.

$$C = b^2 + t^2 + m^2 \quad \dots (9)$$

Where b represents the battery charge deficit, t represents the data transmission deficit and m represents the recording deficit. A deficit is defined as being the magnitude of the difference between some current state variable and its nominal equilibrium value. The deficits have the following expression:

$$b = \frac{b_{max} - b_c}{b_{max} - b_{min}} \quad \dots (10a)$$

$$m = \frac{m_{max} - m_c}{m_{max}} \quad \dots (10b)$$

$$t = \frac{m_c}{m_{max}} \quad \dots (10c)$$

where the subscript c identifies the current value of a state variable – b , battery charge, and m , memory level – and the subscripts max and min , identify the upper and lower lethal values for the state variable. It can be noted how the deficit for the battery charge increases as the value of the current battery charge decreases. Similarly the deficit for recording data is greatest when the current available memory space, identified by m_c , is zero, and decreases as the storage device fills with recorded data. Opposite is the behaviour of the transmission deficit t , which is highest when the memory is full, and decreases as data is down-linked to the ground station freeing up storage space. Essentially, the state variable deficits determine how far away from the origin that state variable is. Finally, it must be noted that a quadratic cost function has the desirable property that the cost of possessing any particular deficit increases more rapidly, than linearly, the further away from the homeostatic equilibrium point the spacecraft's variable lies. This is important because the closer the spacecraft is to a lethal limit, the more likely it is that it will suffer a failure and cease to operate.

The system equations, which link the rate of change of a state variable with a behaviour for the satellite are:

$$\dot{b} = -r_{sun} u_s \quad \dots (11a)$$

$$\dot{t} = -r_{transmit} u_t \quad \dots (11b)$$

$$\dot{m} = -r_{record} u_r \quad \dots (11c)$$

with the constraint on the behaviours given by:

$$0 \leq \frac{u_s}{k_{sun}} + \frac{u_t}{k_{transmit}} + \frac{u_r}{k_{record}} \leq 1 \quad \dots (12)$$

To ensure its survival, the spacecraft must never drain its battery below the lower lethal limit. The satellite energy deficit b , is the measure of how much the batteries have discharged. Pointing the solar panels towards the Sun and charging the battery reduces this deficit. The spacecraft must also produce useful work, by recording data from its payload and transmitting it back to Earth. The payload will be associated with a work deficit composed of a recording deficit m , and a transmitting to Earth ground station deficit t . By storing data, the spacecraft may reduce the recording deficit, while downloading data back to Earth will reduce the transmission deficit. It has been shown earlier that the behaviour to be performed by the spacecraft is the one associated with the highest drk product. In this formulation the deficits from the state variables combine with stimuli from the environment to determine a behavioural sequence. The stimuli are considered to be a cue to resources that will have consequences to the agent's state variables.

The decision to perform a particular behaviour is made by calculating the tendencies to perform all the various activities the spacecraft may exhibit and choosing the behaviour that possesses the highest tendency as explained in Section 3.3. Empirical evidence

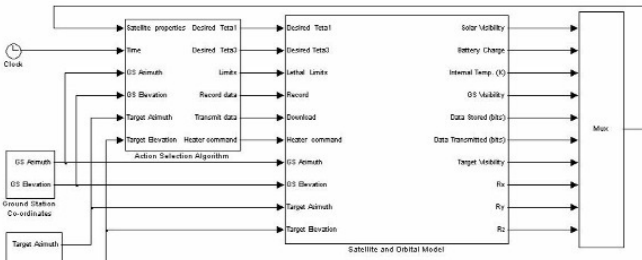


Figure 2. Complete simulink model.

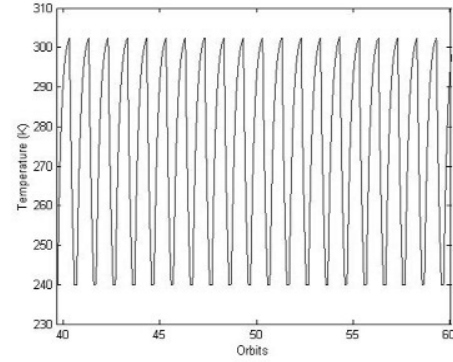


Figure 3. Internal temperature.

that this occurs in animals has been discussed at length⁽¹⁷⁻¹⁸⁾. In addition, the cost function model predicts that such a multiplicative combination rule, when applied to the deficit and cue, should generate optimal behaviour sequencing. We can therefore finally summarise the problem of optimal control for the spacecraft as:

$$\text{behaviour} \Rightarrow \text{Max}[\text{deficit} \times \text{availability} \times \text{accessibility}].$$

$$\text{Max}[b \times r_{\text{sun}} \times k_{\text{sun}}] \Rightarrow \text{Charge the battery} \quad \dots (13a)$$

$$\text{Max}[m \times r_{\text{target}} \times k_{\text{target}}] \Rightarrow \text{Record data} \quad \dots (13b)$$

$$\text{Max}[t \times r_{\text{ground station}} \times k_{\text{ground station}}] \Rightarrow \text{Transmit to Earth ground station} \quad \dots (13c)$$

The satellite selects the optimal behaviour by computing the various deficits, taking environmental cues to assess availability and accessibility of the resources and finally calculating the *drk* product associated with each behaviour. The optimal behaviour at any time is therefore the one which yields the highest of the above products. This algorithm also shows a degree of opportunism, because it considers environmental factors together with internal deficits. For example even if the battery deficit is low and the work deficit is high, the satellite may still opt to charge the batteries if sunlight is available and cues for doing work – visibility of ground station or target area – are low. Such opportunism is one of the major benefits of this algorithm and it is difficult, if not impossible, to code into conventional artificial intelligence engines. Another significant advantage of such a method is that the spacecraft measures environmental parameters (such as the presence of sunlight or ground station) and internal parameters (such as battery charge and memory level) so that complex models of the environment are not required to select the appropriate behaviour. Also, it is not necessary to have complex models of the spacecraft and its internal subsystems. If we consider the battery charge as an example, the model used for it is not directly relevant to the performance of the action selection algorithm; the algorithm uses the direct measure of battery charge rather than a model of the battery. Therefore, we can expect that the modelling of more complex and numerous spacecraft subsystems will not change the qualitative behaviour of the algorithm. This method however may easily incorporate additional tasks which will either form part of the action selection process, or which can be scheduled at a particular time by setting the *drk* product to equal unity at a fixed time. Adding extra tasks is straightforward; each new behaviour will be given a deficit, availability and accessibility. The resulting behaviour will always be the one with the highest *drk* product.

4.0 CASE STUDY

The satellite will operate in different orbits and is considered to have three rotational degrees of freedom that can be controlled by reaction wheels. The spacecraft is modelled as a cube and to provide pointing constraints the antenna, camera and solar panel are placed on different sides of the spacecraft. The electrical power system consists of a

solar array, battery and several electrical loads. The payload is a camera that records at a steady rate when active and a radio transmitter to broadcast data to the ground station. The individual subsystems are coupled together: switching the transmitter on drains the battery and reduces the amount of stored data. The spacecraft is controlled by switching the camera, the transmitter and an internal heater on or off, and commanding the attitude control subsystem to track one of the three targets – Sun, Earth ground station and Earth target – by activating the reaction wheels. The spacecraft has an internal heater which may be switched on or off independently of what other task the spacecraft may be performing; the heater is automatically activated when the temperature drops below a certain threshold value fixed at 240K and is not commanded by an action selection algorithm. The heater however drains the battery, and therefore indirectly influences the action selection process. The spacecraft selects the optimum behaviour at any time by evaluating the deficits of the state variables – battery and memory level – assessing the availability and accessibility of the environmental resources – Earth ground station, Sun and Earth target – and finally computing the *drk* product. The spacecraft will switch between different behaviours when the difference between two *drk* products surpasses a fixed threshold. The user selects the ground station and target co-ordinates (azimuth and elevation) within the appropriate blocks. Other parameters that can be defined by the user are the orbital parameters – apogee, perigee, inclination, ascending node and perigee argument – the inertia moments⁽¹¹⁻¹³⁾ of the spacecraft and the free parameters α_i and β_i ($i = 1-3$) which influence the pointing control algorithm; all these variables can be modified from within the satellite block. Finally the user can change the state variables lethal limits – internal temperature, memory space and battery power – within the action selection block. In Fig. 2 we can see the complete Simulink model.

To test the action selection algorithm the spacecraft is inserted into a low Earth polar orbit. The orbit is circular with a 500km altitude, and an inclination of 85-95°. There is one single ground station present placed at 57.3° latitude, the latitude of Glasgow. There are also six different target areas situated at 80° latitude and evenly spaced in longitude between each other. The simulation runs for just over 90 orbital periods, which equates approximately to six mission days. In Figs 3-9 we can see the results of this.

As can be noted from Figs 3-5 the temperature oscillates as the spacecraft goes in and out of the eclipse part of the orbit – the temperature increases while the spacecraft is in direct sunlight, while the temperature decreases while the spacecraft is in eclipse. When the internal temperature reaches the threshold value of 240K the heater automatically switches on to maintain the temperature above the minimum lethal level. The threshold value is selected by the user and is quite arbitrary although this value is linked to different spacecraft components which have an optimal operational range. It can also be noted how the spacecraft charges the battery when in direct

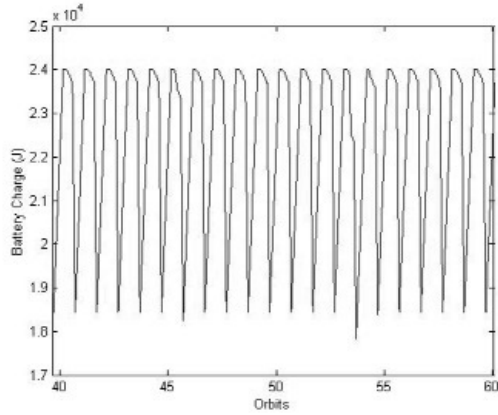


Figure 4. Battery charge.

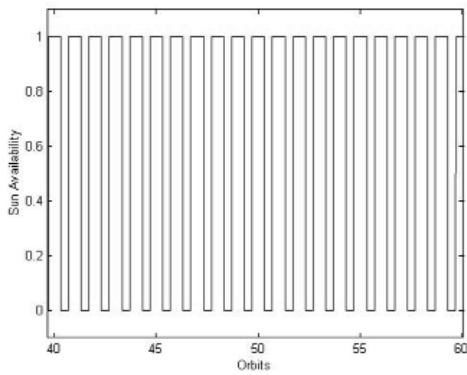


Figure 5. Sun availability.

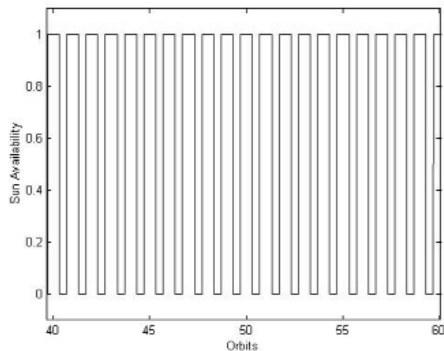


Figure 6. Stored data.

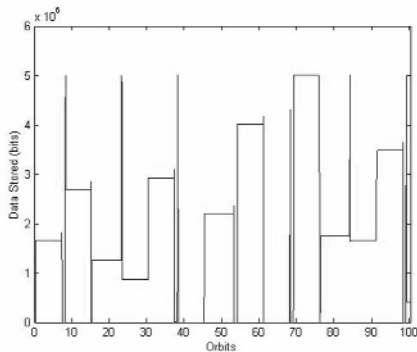


Figure 7. Target availability.

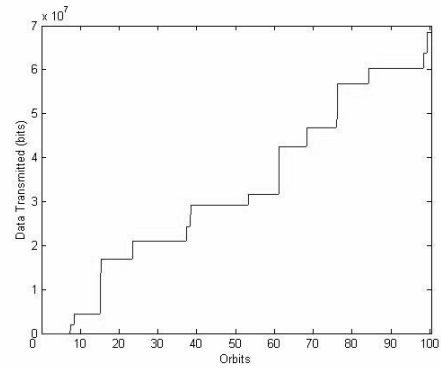


Figure 8. Transmitted data.

sunlight by pointing the side mounted with the solar array towards the Sun. It is interesting to note what happens during the eclipse phase of the orbit to the battery charge level. We can see different slopes as the battery charge level decreases. This is due at first because the transmitter or payload are active; when either is operational there is a demand on the battery for their activation. After that, there is a period during which the transmitter or payload are not active and the discharge in the battery level proceeds at a lower rate. When the heater is then turned on to maintain the internal temperature, the battery is discharged at an increased rate.

Several interesting comments can be made by looking at Figs 6 and 7. First of all it should be noted that the spacecraft does not fly over the six different target areas during one orbit period. Also the target availability varies during each orbit as previously. There are then two interesting differences that we can highlight when looking at the stored data and the target availability. When the availability of the resource is high the spacecraft records significant data. However when the availability of the target area is low the spacecraft may opt not to image as highlighted by the amount of data stored in the memory remaining constant. This is because the spacecraft may have more pressing needs; i.e. charging the battery or downloading recorded data, or because recording data during a low availability flyby is not an efficient activity from an energetic point of view. Similar considerations can be made by looking at Figs 8 and 9. Again the spacecraft does not see the ground station during each orbit, and it actually goes approximately five orbits without ever passing over it. The non-periodic nature of the ground station availability and target availability is due to the fact that the orbit period of the spacecraft in a 500km circular orbit is 94.62mins, and therefore not repeatable during the 24hr rotation period of the Earth. We can see how, when the ground station has a good availability the spacecraft transmits significant data. On the other hand when the ground station availability is poor there is not much data transmitted back to Earth.

4.0 CONCLUSIONS

We have introduced a scheme for sequencing tasks on a spacecraft. The action selection algorithm is easily implemented by virtue of its computational simplicity. Moreover, the strategy is derived from optimal control theory. The model is however somewhat simplified, and an actual spacecraft may have several more operational tasks that may be autonomously controlled or be scheduled or commanded by ground control. This method however may easily incorporate additional tasks which will either form part of the action selection process, or which can be scheduled at a particular time by setting the *drk* product to equal unity at a fixed time. Adding extra tasks is straightforward; each new behaviour will be given a deficit,

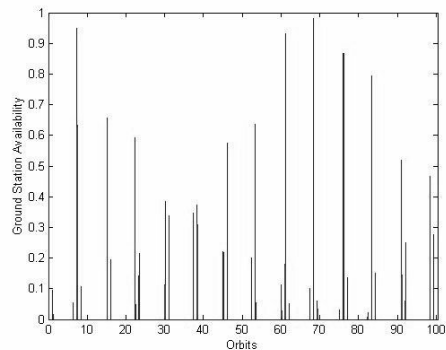


Figure 9. Ground station availability.

availability and accessibility. The resulting behaviour will always be the one with the highest drk product. A significant advantage of such a method is that the spacecraft measures environmental parameters (such as the presence of sunlight or ground station) and internal parameters (such as battery charge and memory level). Complex models of the environment are not required to select the appropriate behaviour. Also it is not necessary to have complex models of the spacecraft components and subsystems. If we consider the battery charge as an example, the model used for it is not directly relevant to the performance of the action selection algorithm; the algorithm uses the measure of the battery charge rather than using a model of the battery charge. Therefore we can expect that the modelling of more complex and numerous spacecraft subsystems will not change the qualitative behaviour of the algorithm. The study of such a method can be extended to a constellation of satellites, in which the individual spacecraft co-operate with each other. The co-operation may be as simple as passing data to each other when the memory level is full and the ground station is not available, or as complex as having one master spacecraft commanding the other slave spacecraft in the constellation. The method, because of its computational simplicity, can also be easily applied to planetary rovers and future 'satellites-on-a-chip', where the algorithm and behaviours can be hard-wired into the spacecraft.

REFERENCES

1. SIBLY, R.M. AND MCFARLAND, D.J. *A State Space Approach to Motivation, Motivational Control System Analysis*, 1974, Academic Press.
2. MCFARLAND, D.J. AND SIBLY, R.M. *The Behavioural Final Common Path, Philosophical Transactions of the Royal Society, (Series B)*, 1975, **270**, pp 265-293.
3. MCFARLAND, D.J. AND HOUSTON, A.I. *Quantitative Ethology: The State Space Approach*, 1981, Pitman.
4. GILLIES, E.A., JOHNSTON, A.G.Y. AND MCINNES C.R. Action selection algorithms for autonomous micro-spacecraft, *J Guidance Navigation and Control*, 1999, **22**, (6), pp 914-916.
5. BLUMBERG, B. Action-selection in Hamsterdam: lessons from ethology, From animals to animats 3: Third international conference on the simulation of adaptive behaviour, 1994, Brighton, UK.
6. STEELS, L. A case study in the behaviour-oriented design of autonomous agents, From animals to animats 3: third international conference on the simulation of adaptive behaviour, 1994, Brighton, UK.
7. SPIER, E. AND MCFARLAND, D.J. A finer-grained motivational model of behaviour sequencing, From animals to animats 4: Fourth international conference on the simulation of adaptive behaviour, 1996, Boston, MA.
8. SIBLY, R.M. AND MCFARLAND, D.J. On the fitness of behaviour sequences, *The American Naturalist*, 1976, **110**, (974), pp 601-617.
9. HOUSTON, A.I. AND MCFARLAND, D.J. *Behavioural Resilience and its Relation to Demand Functions, Limits to Action: The Allocation of Individual Behaviour*, 1980, pp 177-203.

10. PONTRYAGIN, L.S., BOLTYANSKII, V.G., GAMKRELIDZE, R.V. AND MISHCHENKO, E.F. *The Mathematical Theory of Optimal Processes*, 1962, John Wiley and Sons, New York.
11. DIXIT, A.K. *Optimization in Economic Theory*, 1976, Oxford University Press.
12. ELGERD, O. *Control Systems Theory*, 1967, McGraw-Hill, New York.
13. BOLLES, R.C. *Theory of Motivation*, 1967, Harper and Row, New York.
14. SCHOENER, T.W. Theory of feeding strategies, *Annual review of ecological systems*, 1971, **2**, pp 369-404.
15. MCCLEERY, R.H. On satiation curves, *Animal Behaviour*, 1978, **25**, pp 1005-1015.
16. Krebs, J.R. *Behavioural Aspects of Predation, Perspectives in Ethology*, 1973, pp 73-111, Plenum Press, New York.
17. BAERENDS, G.P., BROWER R. AND WATERBOLK H.T. Ethological studies of *Lebistes Reticulatus* (Peters). 1. An analysis of the male courtship patten, *Behaviour*, 1955, **8**, pp 249-334.
18. Sibly, R.M. *How Incentive and Deficit Determine Feeding Tendency*, *Animal Behaviour*, 1975, **23**, pp 437-466.