

Double-Resonance Magnetometry in Arbitrarily Oriented Fields

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Overview

- Quantum Technology Hub
 - Practical focus: apply QT to sensors
- Design choices
 - Unshielded sensor
- B_0 orientation
 - Signal amplitude and phase effects
- Exploitation
 - Demonstrator system



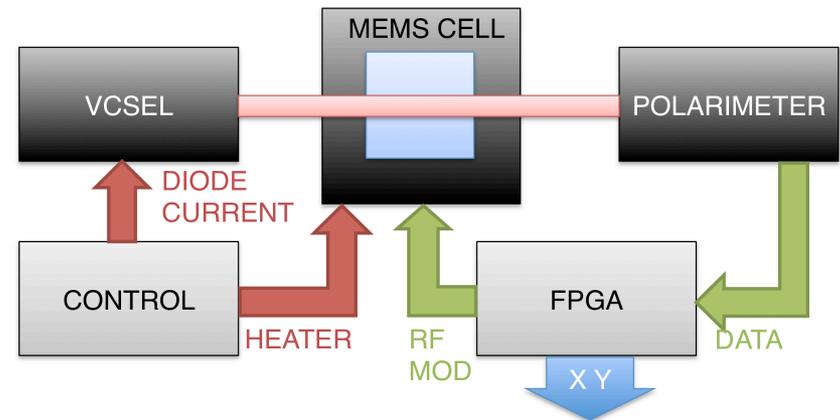
UK National
Quantum Technology Hub
Sensors and Metrology

- Led Birmingham University
 - Includes Strathclyde, Nottingham, Sussex, Southampton, NPL & industry
 - Started Jan 2015
- Unshielded portable sensor
 - Geophysical measurement
 - Low size, power requirement
 - Sub-pT sensitivity



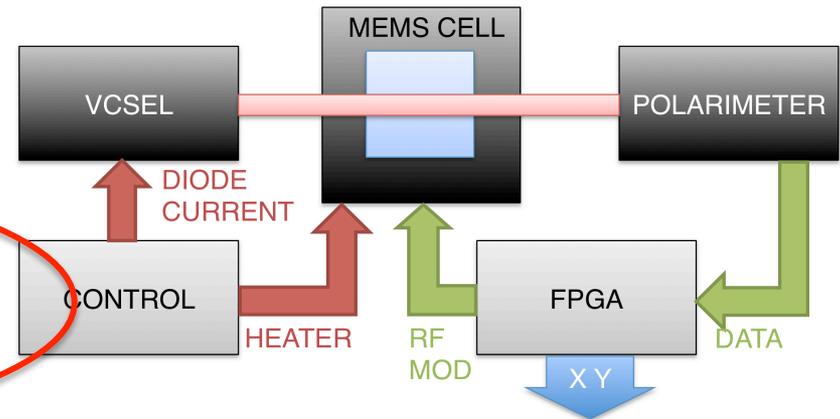
Unshielded Double Resonance Sensor

- **Dynamic range - yes**
 - No requirement for μT compensation
- **Noise rejection - yes**
 - Homodyne detection
 - Polarimetry
 - Gradiometry
- **Arbitrary B_0 orientation - ?**
 - Dead-zones
 - Heading errors
- **Portability - yes**
 - Single frequency pump-probe
 - Firmware signal processing



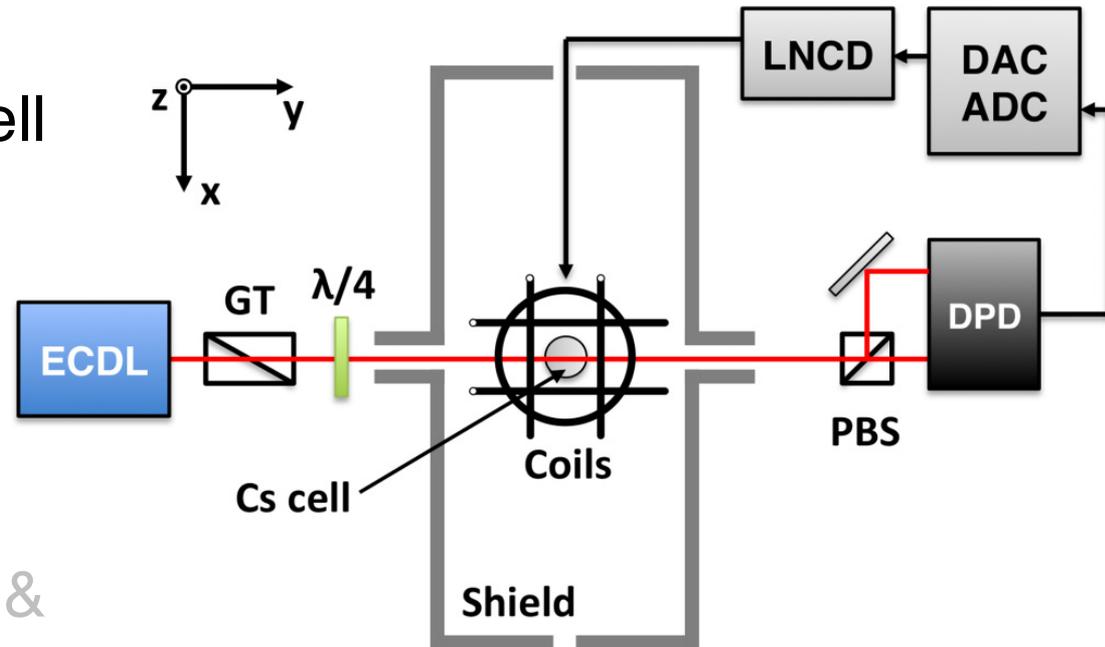
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B_0 Orientation: Shielded Test System

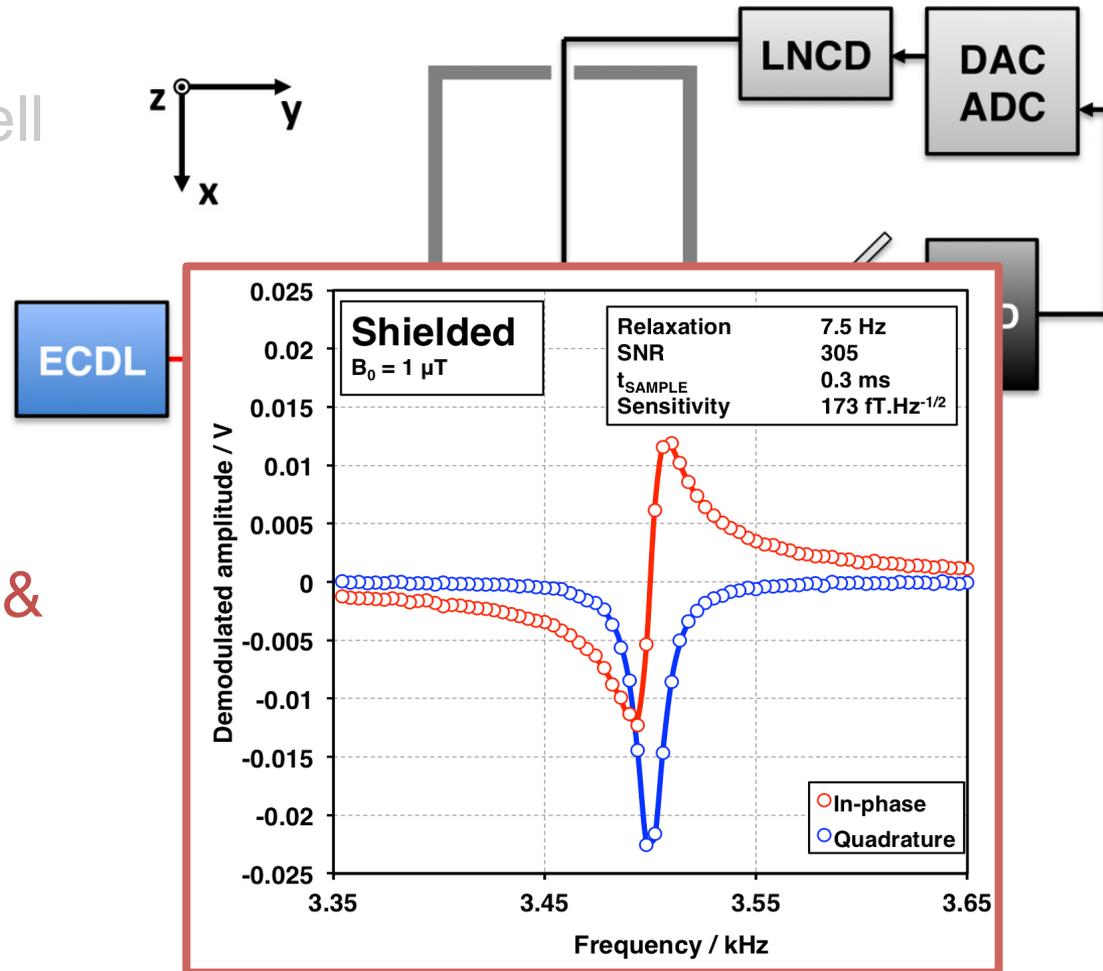
- M_x configuration
- Paraffin-coated Cs cell
 - Weis group [1]
- B_0 control
 - Software-controlled coils
 - Iterative calibration
- Software modulation & demodulation
 - Lineshape fitting



[1] N. Castagna *et al.*, Appl. Phys. B: Lasers Opt. **96**, 763 (2009)

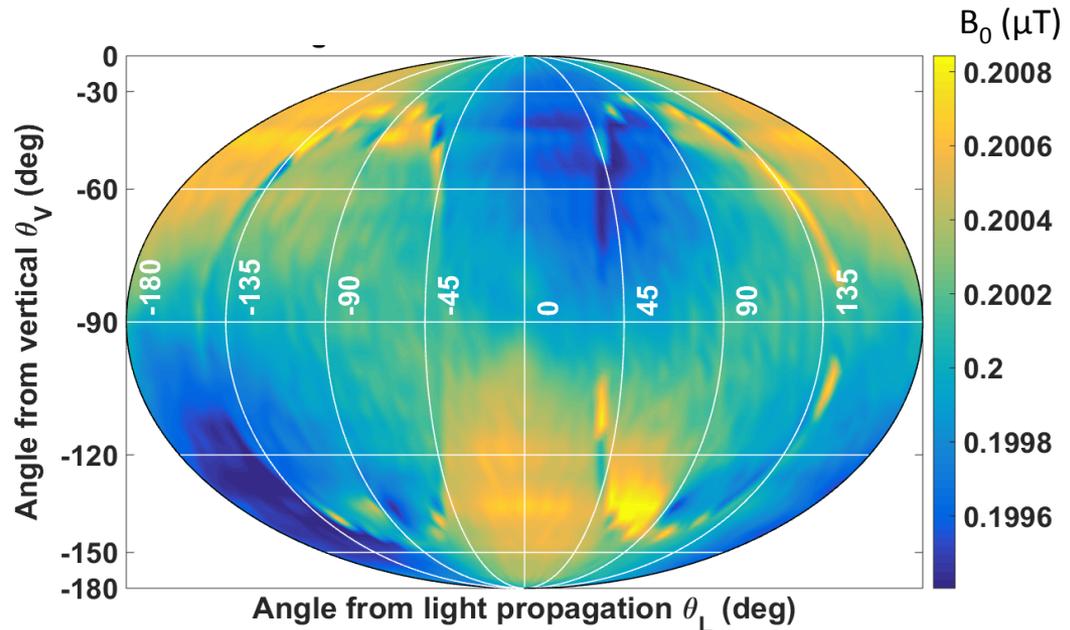
B₀ Orientation: Shielded Test System

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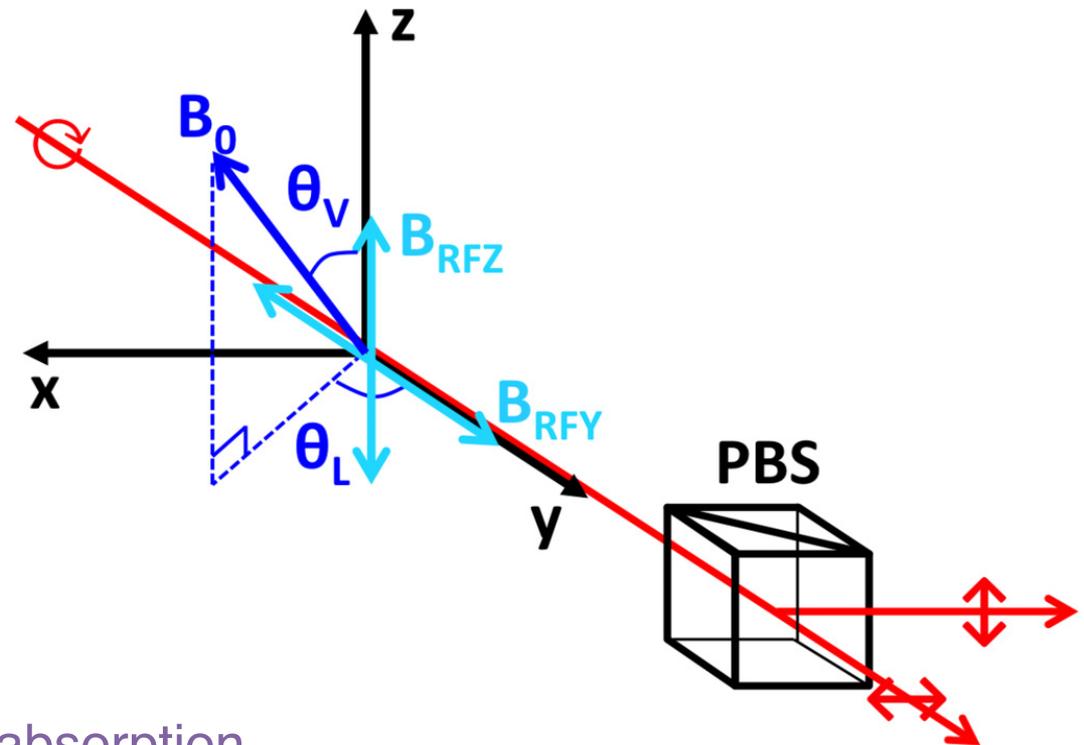
- B_0 control
 - Low-noise current drivers
 - Shield degauss
 - Single-axis calibration [2]
 - 3D calibration [C. O'Dwyer poster]
- 200 nT B_0
 - $\delta|B| = 0.24$ nT
 - $\delta\theta = 0.23$ mrad



[2] S. J. Ingleby *et al.*, Rev. Sci. Instrum. **88**, 043109 (2017)

B_0 Orientation: Theory

- Pump
 - Cs D1 4-3
 - σ -polarised
 - $20 \mu\text{W}$
 - $\Gamma_{\text{PUMP}} \ll \Gamma$
- Evolution
 - $B_0 \gg B_{\text{RF}}$
 - $\Omega_{\text{RF}} \sim \Gamma$
- Probe
 - Polarimeter signal
 - Linear dichroism
 - Cancellation of \odot absorption



B₀ Orientation: Theory

Multipole moment model [3][4]

- Pump

- Creation of $k = 1, 2, \dots$
- Equilibrium $q = 0$
 - B₀ frame

- Evolution

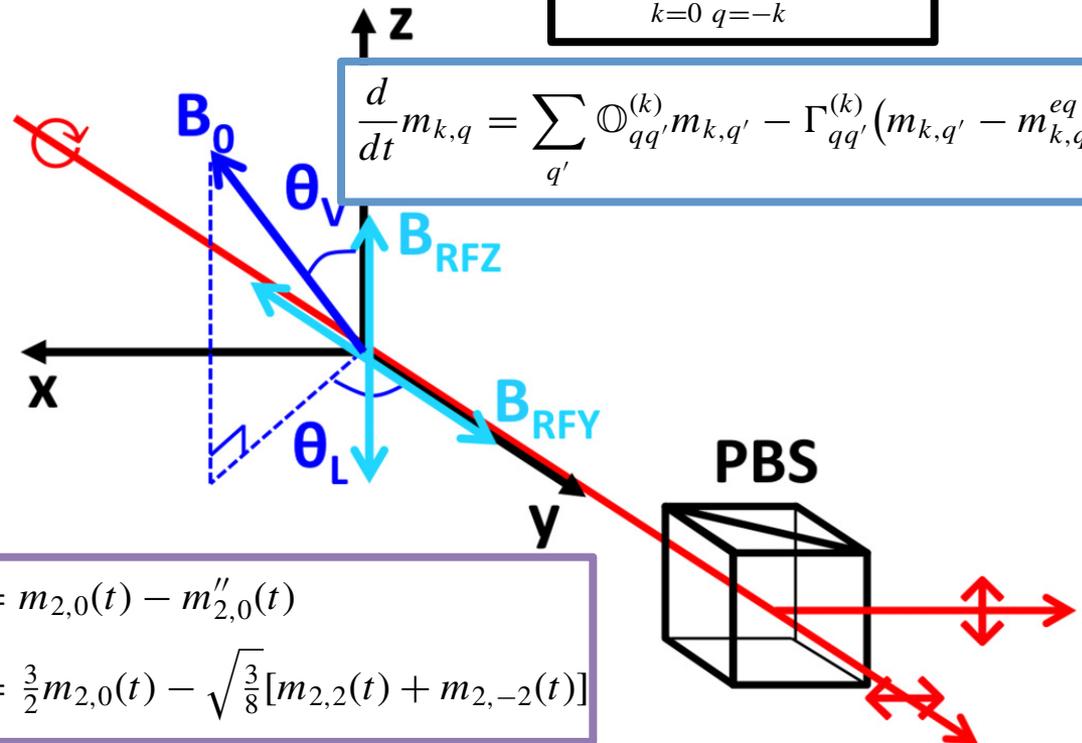
- RW frame
 - B₀ // z
 - B_{RF}(t=0) // -x
- Obtain $m_{kq}(t)$

- Probe

- Difference in \uparrow and \leftrightarrow

$$\rho = \sum_{k=0}^{2F} \sum_{q=-k}^k m_{k,q} T_q^{(k)}$$

$$\frac{d}{dt} m_{k,q} = \sum_{q'} \mathbb{O}_{qq'}^{(k)} m_{k,q'} - \Gamma_{qq'}^{(k)} (m_{k,q'} - m_{k,q'}^{eq})$$

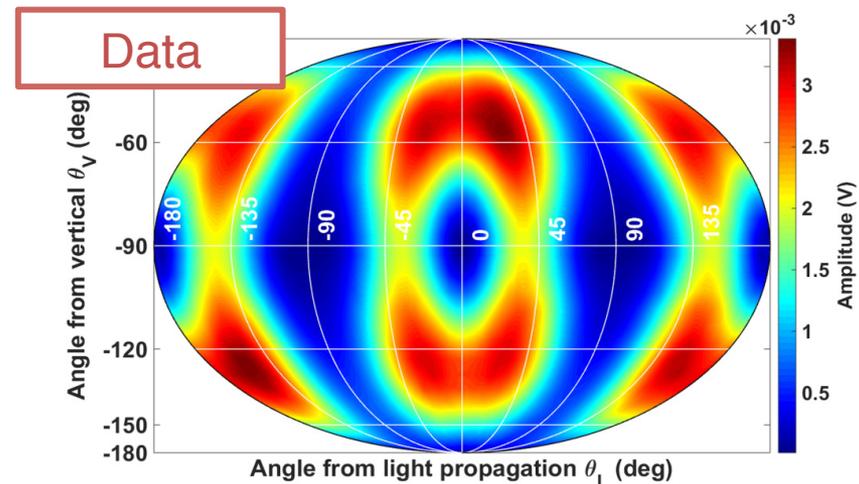
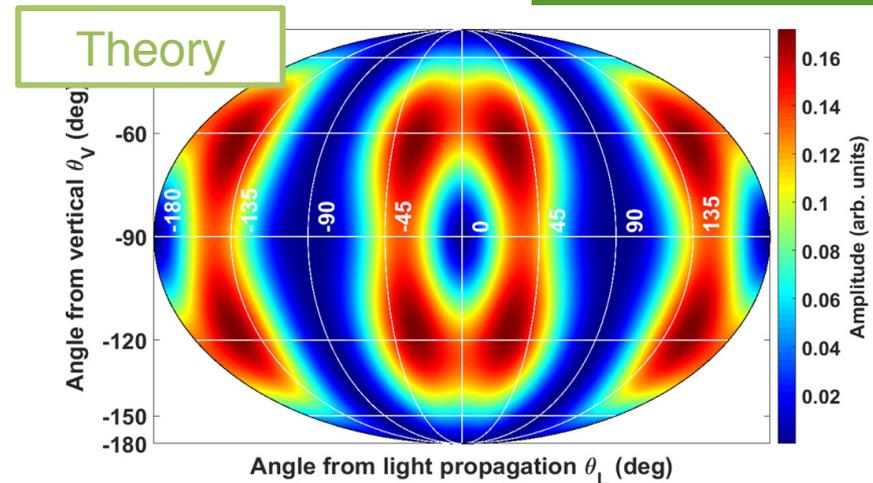


$$f(t) = m_{2,0}(t) - m''_{2,0}(t) = \frac{3}{2} m_{2,0}(t) - \sqrt{\frac{3}{8}} [m_{2,2}(t) + m_{2,-2}(t)]$$

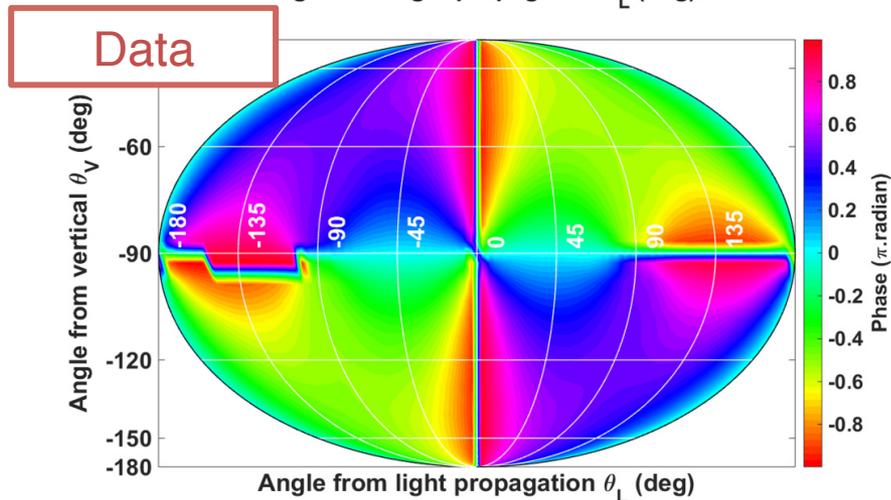
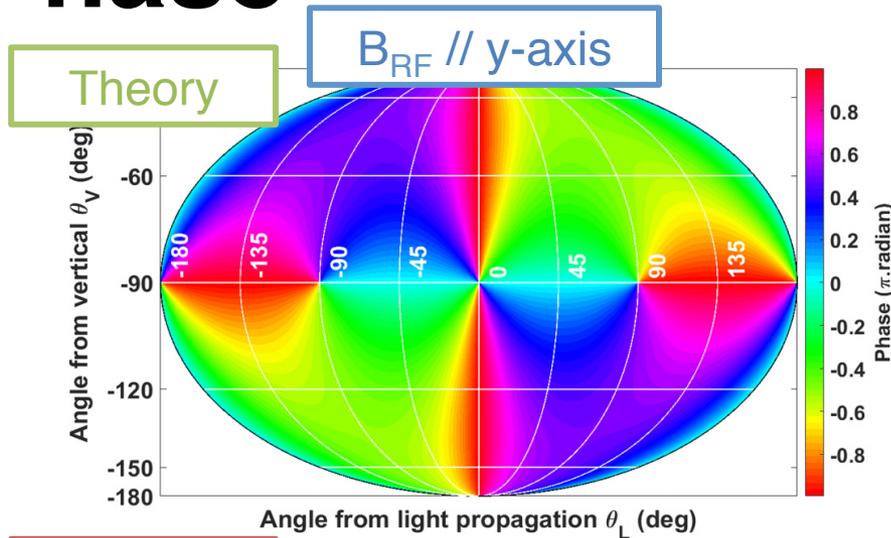
[3] A. Weis, G. Bison, A. S. Pazgalev, Phys. Rev. A **74**, 033401 (2006)
 [4] M. A. Morrison and G. A. Parker, Aust. J. Phys. **40**, 465 (1987)

B₀ Orientation: Amplitude

- 4π angular scan
 - 1646 resonance fits
 - 3½ hours
- $R^2 \equiv X^2 + Y^2$
 - Extract X and Y from $f(t)$
- Dead-zones



B₀ Orientation: Phase

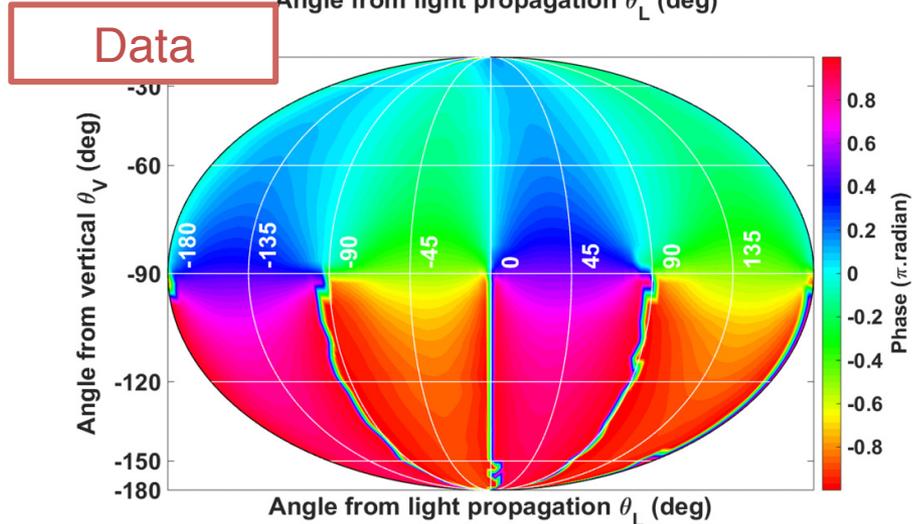
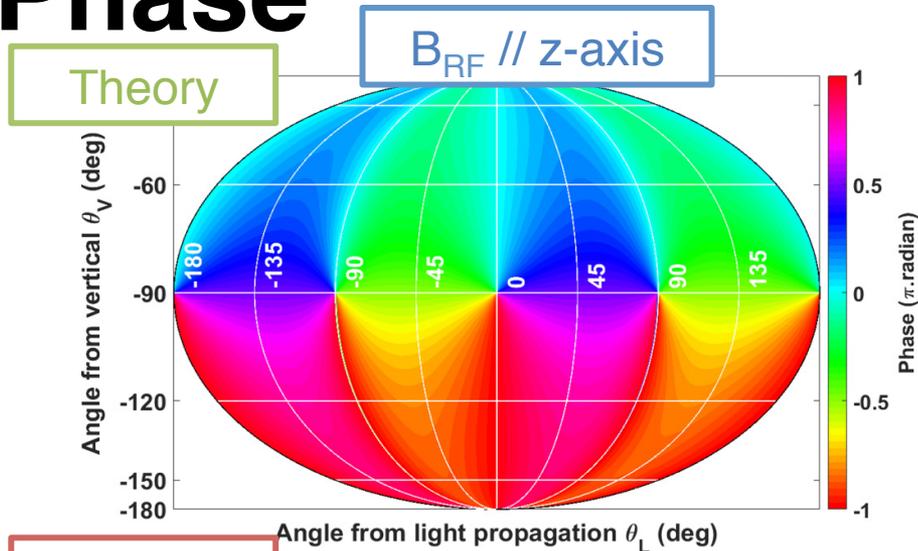


- On-resonance phase
 $\tan \phi \equiv X/Y$
- Strong dependence
 - B₀ orientation
 - B_{RF} orientation

$$\tan \phi_{RFy} = \frac{2 \sin \theta_L \tan \theta_V}{(\sin^2 \theta_L \tan^2 \theta_V - 1) \cos \theta_L \sin \theta_V}$$

$$\tan \phi_{RFz} = \frac{-\sin 2\theta_L \sin \theta_V}{(1 + \cos^2 \theta_L) \sin 2\theta_V}$$

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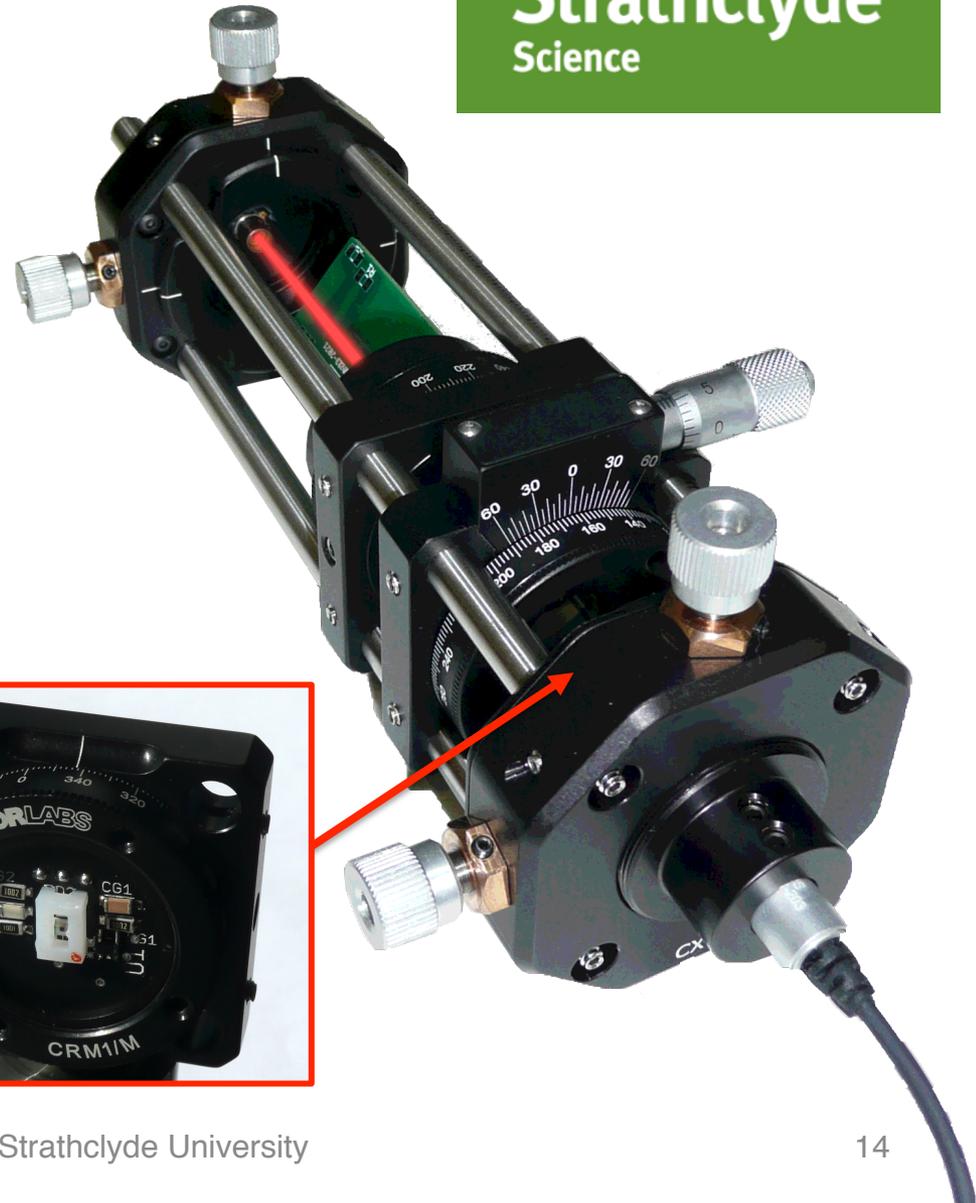
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Portable Demonstrator System

- Minimal hardware
 - VCSEL
 - MEMS cell
 - Heater PCB
 - Polarimeter PCB
- Component testing
 - FPGA
 - MEMS cell
 - Geometry
 - Buffer gas



Summary

- Understanding B_0 orientation effects
 - Model & measurement agree
 - Optimal sensitivity axes
 - Phase-vector information
 - Exploit using signal processing

Strathclyde Magnetometry People



Erling Riis, Aidan Arnold, Paul Griffin, Stuart Ingleby, Dominic Hunter, Carolyn O'Dwyer, Iain Chalmers