

## SHELTER MODELS FOR CONSEQUENCE ANALYSIS AND RISK ASSESSMENT OF CO<sub>2</sub> PIPELINES

J.M. Race<sup>a</sup>, K. Adefila<sup>a</sup>, B. Wetenhall<sup>b</sup>, H. Aghajani<sup>b</sup>, B. Aktas<sup>b</sup>

<sup>a</sup> Department of Naval Architecture, Ocean and Marine Engineering, University of Strathclyde <sup>b</sup> School of Marine Science and Technology, Newcastle University

### **Presentation content**



- Requirement for a shelter model
- Description of models developed
  - Analytical model
  - Computational Fluid Dynamics (CFD) model
- Model validation single room
- Sensitivity study
- Effect of partitions and half height clouds
- Conclusions and recommendations

## What is the CCS transportation challenge?



To transport anthropogenic  $CO_2$  of varying composition from multiple capture sites (power plant and industrial) to multiple storage sites in a safe, reliable and efficient manner in compliance with appropriate design standards and regulatory requirements.

## Consequences of CO<sub>2</sub> pipeline failure



- CO<sub>2</sub> is not explosive or inflammable like natural gas and is odourless.
- CO<sub>2</sub> is denser than air and might accumulate in depressions or valleys.
- CO<sub>2</sub> is toxic and above concentrations of ~10% can have long term effects or cause fatality.

#### Therefore

- Need to be able to calculate CO<sub>2</sub> concentrations around a failure in order to define separation distances from pipelines using a Quantitative Risk Assessment approach.
- Requires a pragmatic infiltration model to predict effect CO<sub>2</sub> exposure on humans in buildings.

## Consequences of CO<sub>2</sub> pipeline failure





## Analytical model description



- Based on the principles of natural building ventilation (Etheridge and Sandberg, 1996).
- Model described in outline in Lyons et al 2015 and in detail in future publications
- Considers wind driven and buoyancy driven air flow.

#### **Assumptions:**

- Initial concentration of CO<sub>2</sub> in building is same as atmosphere.
- Building is engulfed in a cloud of CO<sub>2</sub> following a release



Etheridge, D. W. & Sandberg, M.. 1996. Building Ventilation: Theory and Measurement, New York: John Wiley and Sons.

Lyons, CJ, Race, JM, Hopkins, HF & Cleaver, P 2015, Prediction of the consequences of a CO<sub>2</sub> pipeline release on building occupants. in *Hazards 25: Edinburgh International Conference Centre, Edinburgh; United Kingdom; 13 May 2015 through 15 May 2015.* vol. 160, Institution of Chemical Engineers Symposium Series, Red Hook, Hazards 25, Edinburgh, United Kingdom, 13-15 May.

## Air flow – wind driven



- Wind blowing outside.
- Pressure difference between internal and external environments.
- Air flows from high to low pressure in at front face, out at rear.
- Air flow straight through building.



## Air Flow – buoyancy driven



#### In the absence of a release:

- Increased internal air temperature reduces internal air density.
- Steeper pressure gradient outside the building than inside (as density is greater outside).
- Creates pressure difference across openings at top and bottom of building.
- Warm, less dense air leaves and is replaced by colder more dense air at base, with upward drift of warmer air inside.



#### Dr Julia Race

## CFD model

- Based on conservation equations for mass, momentum, energy and chemical species
- k 
  *e* turbulence model was corrected to incorporate the effect of buoyancy driven flows with low Reynolds number
- Four different models tested Lag Elipptic Blending (EB) k – ε model gave best results relative to the experimental data
- Meshed using polyhedral mesh within solution domain with a prism layer mesher used to improve the CFD simulation in near-wall regions







## Model input data

#### **Cloud conditions**

- CO<sub>2</sub> concentration profile
- Temperature profile



#### Centreline of release

![](_page_9_Picture_6.jpeg)

#### **Atmospheric conditions**

- Wind speed
- Wind incident direction
- Internal temperature
- Internal CO<sub>2</sub> concentration

Dr Julia Race

## Model comparison – single room totally engulfed

![](_page_10_Picture_1.jpeg)

**University** of

Strathclyde Engineering

## Toxic dose

![](_page_11_Picture_1.jpeg)

 A generalised equation for toxic dose of exposure to some contaminant is given by:

$$D = \int c(t)^n dt$$

Where

- c(t) the concentration of the contaminant a person is exposed to in parts per million (ppm),
- *t* the time of the exposure in minutes
- *n* is the toxic index = 8 for  $CO_2$
- Dangerous Toxic Loads
  - The Specified Level of Toxicity (SLOT). The SLOT dose for CO<sub>2</sub> is 1.5 x 10<sup>40</sup> ppm<sup>8</sup>.min.
  - The Significant Likelihood of Death (SLOD). The SLOD dose for CO<sub>2</sub> is 1.5 x 10<sup>41</sup> ppm<sup>8</sup>.min.

## Model comparison – single room totally engulfed

![](_page_12_Picture_1.jpeg)

![](_page_12_Figure_2.jpeg)

## Sensitivity study – wind speed dependence

![](_page_13_Picture_1.jpeg)

![](_page_13_Figure_2.jpeg)

### Partitions and half height clouds

![](_page_14_Picture_1.jpeg)

![](_page_14_Figure_2.jpeg)

### Conclusions

![](_page_15_Picture_1.jpeg)

- Two shelter models have been developed as part of this work; an analytical and a CFD model.
- The models compare favourably with experimental test data
- It has been demonstrated that the ability of buildings along a pipeline route to provide shelter can be determined using these models.
- The wind speed has been shown to have the greatest impact on concentration profiles within the building.

### Conclusions

![](_page_16_Picture_1.jpeg)

- Calculations have been conducted for worst case direction.
- SLOD times would be different (and less severe) for different directions throughout the cloud.
- In conducting a full QRA a failure frequency analysis would be incorporated with these results to calculate the risk at any particular location.
- However, it has been shown that dose received by an individual in a building would not reach the levels of toxicity experienced in shelter were not considered.

### Acknowledgement

![](_page_17_Picture_1.jpeg)

This work has been funded by the UK Carbon Capture and Storage Research Centre within the framework of the S-Cape project (UKCCSRC-C2--179) and the National Grid COOLTRANS research programme.

The authors would also like to thank National Grid and DNV-GL for the provision of the experimental input data for the validation study.

![](_page_17_Picture_4.jpeg)

The Don Valley Power Project is co-financed by the European Union's European Energy Programme for Recovery The sole responsibility of this publication lies with the author. The European Union is not responsible for any use that may be made of the information contained therein.

# University of **Strathclyde** Glasgow

The University of Strathclyde is a charitable body, registered in Scotland, with registration number SC015263