

# Latest development of a W-band Gyro-TWA based on a Helically Corrugated Interaction Region

**W. He, C. R. Donaldson, L. Zhang, P. McElhinney, K. Ronald,  
A. W. Cross and A. D. R. Phelps**

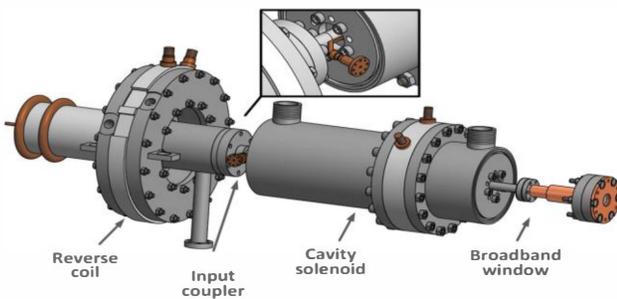
Department of Physics, SUPA,  
University of Strathclyde, Glasgow, G4 0NG, UK  
Email: w.he@strath.ac.uk

**Abstract:** Latest development and experimental study of a W-band gyro-TWA with a helically corrugated waveguide and a cusp electron gun are presented. With an input seed signal from an 1.5 W, 90-96 GHz solid state source a gain of 27 dB was measured from the experiment. The bandwidth of the gyro-TWA was measured to be at least 5 GHz.

**Keywords:** helically corrugated waveguide, gyrotron, gyro-TWA, W-band gyro-devices, cusp electron gun.

## Introduction

The gyro-devices are high power coherent microwave sources that excel at high frequencies (up to the terahertz range). There are a number of applications for such devices including high resolution RADAR, plasma diagnostics, communications and medical imaging, and accurate material analysis based on electron spin resonance in conjunction with magnetic resonance and terahertz spectroscopy. Recently gyro-devices in the form of both a gyro-TWA [1] and a gyro-BWO [2,3] have been developed at the University of Strathclyde. In this paper the latest development and experimental results of a W-band gyro-TWA are presented. A CAD drawing of the gyro-TWA including its components such as input coupler, output window and magnetic coils is shown in Fig. 1.



**Figure 1.** A CAD drawing of the W-band gyro-TWA.

## Interaction region

When the interaction region has a helical corrugation on the inner surface there exists an “ideal” eigenwave giving many benefits that can be exploited in novel gyro-devices and in pulse compression [4]. For the gyro-devices the eigenwave has an almost constant value of group velocity over a wide frequency band in the region of small axial

wave numbers [5]. This dispersion can be designed to match the dispersion line of an electron cyclotron mode or its harmonics. This allows broadband microwave amplification to be achieved in a gyrotron travelling wave amplifier [6].

To drive the beam-wave interaction in a helically corrugated interaction region (HRIC) it is necessary to use an axis-encircling electron beam. The HCIR resonantly couples the  $TE_{11}$  and  $TE_{21}$  modes and results in a ‘ $TE_{21}$ -like’ eigenmode. This eigenmode therefore can efficiently interact with the second harmonic of the electron cyclotron frequency. An axis-encircling electron beam is ideal for harmonic operation of gyro-devices as the mode selectivity nature of such a beam requires that the harmonic number is equal to the azimuthal index of a waveguide mode for effective beam wave coupling, which leads to a reduced possibility of parasitic oscillations. Such an axis-encircling electron beam can be generated by a cusp [7]. The maximum output of the gyro-TWA was predicted to be 5 kW with a 3 dB frequency bandwidth of 90-100 GHz and a saturated gain of 37 dB.

The coupling of the beam and the eigenwave in the gyro-TWA that exists inside the helically corrugated waveguide can be described by the following equation [5]:

$$[(h^2 - 2\delta)(h + \Delta_g - \delta/h_0) + 2\sigma^2/h_0][h - (\delta - \Delta_H)/\beta_{z0}]^2 \\ = C^3(h + \Delta_g - \delta/h_0) \left\{ 1 + \frac{2s}{\alpha_0^2 \beta_{z0}} [h - (\delta - \Delta_H)/\beta_{z0}] \right\}$$

## Cusp electron gun

The cusp electron gun has been simulated and experimentally measured [8] to show the generation of a 1.5 A, 40 keV axis-encircling electron beam. The alpha value has been measured over a range from 1.0 to 3.0. The results agree well with the simulations.

The reverse field coil is located behind the cathode and the main cavity coil is in front. When the magnetic field is varied between 1.65 T and 2.1T the reverse coil’s magnetic field can be adjusted to keep a constant beam pitch angle.

## Input and output of the wave

The input signal was inserted using an input coupler, which operated from 84 GHz to 104 GHz. It consists of a pillbox window with a brazed ceramic disk to seal the UHV vacuum. The coupler was improved from previous version and optimized to allow for mechanical robustness and

larger machining tolerances. To allow maximum beam transportation in the coupler region, the beam tunnel incorporated a Bragg reflector at the diode side of the coupler so that input wave would propagate downstream into the interaction region. The input coupler achieved -10 dB reflection in the frequency band.

The improved output window consisted of 3 disks, with the middle ceramic disk serving as the vacuum boundary and two quartz disks on each side [9]. It achieved a low reflection of -30 dB or better in the 90-100 GHz frequency band.

### Experiment

The gyro-TWA experiments proved successful. A photograph of the device is shown in Fig. 2. Many components have been measured including: broadband input coupler, corrugated quasi-optical mode converter, dispersion of the helical interaction region and broadband microwave window. The output microwave radiation was detected by two crystal detectors situated inside screened boxes. The output power was calibrated using a known microwave source. The experimental results including the output powers and operating frequency bands are measured. With an input seed signal from an 1.5 W, 90-96 GHz solid state source a gain of 27 dB was measured from the experiment. The bandwidth was measured to be at least 5 GHz.



**Figure 2.** A photograph of the W-band gyro-TWA experiment.

### Conclusion

Theory and numerical simulations of the operating parameters of helical waveguide W-band gyro-devices have been confirmed by the experimental measurements.

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