

Grand-Canonical Monte Carlo Adsorption Studies on SBA-2 Periodic Mesoporous Silicas

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ABSTRACT

SBA-2 and STAC-1 are periodic mesoporous silicas with slightly different structures whose pore networks consist of spherical cavities interconnected by windows. This feature makes them attractive for adsorptive separation processes where the selectivity originates from molecular sieving. Recently, we were able to obtain realistic atomistic models for these materials by means of a kinetic Monte Carlo (kMC) method. In this paper, we evaluate the ability of the model to predict adsorption of both non-polar (methane and ethane) and polar (carbon dioxide) adsorptives. Predictions are in good agreement with experimental data, demonstrating the potential of these kMC-based models for use in the design of adsorption processes and the materials used in them. In particular, we show that surface roughness is a key feature for predicting adsorption in SBA-2 materials at low pressures; this is especially relevant in prospective applications such as carbon dioxide capture.

KEYWORDS

Grand Canonical Monte Carlo Simulation, Mesoporous Silicas, Adsorption, Carbon Dioxide, Ethane, Methane

INTRODUCTION

Periodic mesoporous silicas (PMSs) are promising adsorbents,¹ as they offer a combination of high adsorption capacity and the scope to adjust both the size and the surface chemistry of the pores.² SBA-2, a PMS with spherical cavities interconnected by windows,³⁻⁵ has been synthesized and characterized by different groups.^{3-4, 6-8} Since the calcination temperature influences the size of the connecting windows, SBA-2 shows promise as an adsorbent for size- and shape-selective separations. The cavities in SBA-2 are hexagonally close-packed (hcp), reflecting the arrangement of the micelles in the precursor solution. That is, there is a sequence of two hexagonally packed layers, A and B, where the latter is slightly offset with respect to the former. A second, very similar, material is also produced as a result of this synthesis,³ differing from SBA-2 by having cubic close packed (ccp) symmetry, characterized by an A-B-C sequence of layers. In both cases the shape and size of the pores is the same, and the material characteristically exhibits a sharp pore size distribution around the mean pore diameter.⁷ Because of its different symmetry, the ccp material has a separate designation, St Andrews-Cambridge-1 (STAC-1).³ In practice, neither material is synthesized as a pure phase, so that it is best to think of pure SBA-2 and pure STAC-1 as end-points of a spectrum of mixed materials.

Because PMSs are not crystalline, models for these materials cannot be based on knowledge of atomic coordinates from X-ray or neutron diffraction. For this reason, the first models used to represent these adsorbents were simplified, smooth-pore representations^{4-5, 9-12} with surfaces that are regular at the atomic level, capturing the main structural characteristics such as pore size and shape but disregarding other important features such as the structure of the pore surface or the nature of the pore connectivity. For SBA-2, Pérez-Mendoza *et al.* proposed a model^{4-5, 13} consisting of a system of smooth spheres and cylinders where the adsorption was considered to occur independently in each pore (i.e. ignoring their connections with each other) and then integrated by means of a pore size distribution (PSD). However, it is known that in reality the pore surface in PMS materials is not smooth but rather has significant

roughness¹⁴⁻¹⁵ and there is a distribution of pore sizes.⁷ For these reasons more realistic models are needed in order to make accurate predictions of the performance of the material in adsorption and other applications.

A different approach to modeling the structure of PMSs was taken by Schumacher and co-workers,¹⁵⁻¹⁶ who developed a kinetic Monte Carlo (kMC) method that leads to atomistically realistic models of MCM-41, a PMS containing cylindrical pores. In a previous paper¹⁷ the present authors and others extended the approach of Schumacher and co-workers to SBA-2 and STAC-1. This kMC technique mimics the key steps of the synthesis of the real materials by following the silica condensation and aggregation mechanism, according to which randomly arranged micelles accumulate layers of silica around them before spontaneously aggregating to give the long-range order of the final material.¹⁸ A full account of this method is given in our earlier publication.¹⁷ The model pores obtained this way show good agreement with the degree of polymerization, density, and unit-cell parameters of experimental samples. In addition, nitrogen adsorption isotherms were predicted quantitatively when compared with experimental results, which is further evidence of the realism of the kMC approach. Also, we learnt from our models that pore-connectivity in SBA-2 and STAC-1 is likely to occur through windows rather than by channels,¹⁷ as was previously assumed.^{3, 5, 8, 19} The window-like nature of the pore connections means that adsorption takes place mainly in the spherical cavities.¹⁷ Figure 1a shows an example of an SBA-2 simulation cell, obtained by kMC simulation; the windows between the pores are also shown. Figure 1b shows the atomistic surface of the model pore, which arises naturally from the kMC simulation and mimics the roughness of the real materials.

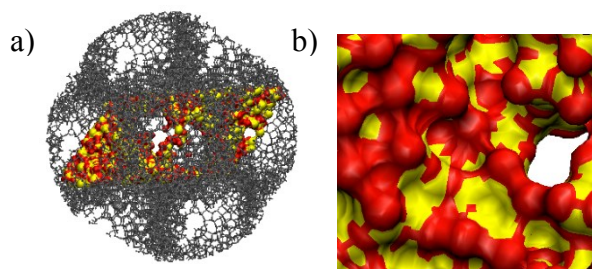


Figure 1: a) Example of a single pore in the model SBA-2 material obtained using the kMC technique. What appear to be large voids in this image are the windows connecting the cavity to its neighbors. b) Close-up of the pore surface of an SBA-2 model pore. Silicon atoms are indicated in yellow, and oxygen atoms in red. Hydrogen atoms are omitted for clarity.

In this work, we investigate the ability of our kMC-based model material to predict adsorption. This analysis, which involves a combination of Monte Carlo simulation of adsorption and experimental adsorption measurements, is of interest for two reasons. Firstly, adsorption allows us to further investigate the realism of the model material, which is of fundamental interest in the study of the synthesis and structure of SBA-2. Adsorption at low pressure is very sensitive to surface roughness and (for polar adsorptives) to surface polarity, while adsorption at high pressure explores pore size and pore geometry. Secondly, we evaluate the applicability of the model materials to adsorption technology; if it can be demonstrated that the adsorption of a range of gases can be reliably predicted, these models can be applied to the design of gas storage and separation processes, and to the tailoring of PMS-based adsorbents for use in such applications. To this end, we use these kMC-generated model pores to study the adsorption of non-polar (CH_4 and C_2H_6) and polar (CO_2) fluids on SBA-2/STAC-1, exploring the predictive capability of these models for adsorptives with different properties.

We also investigate the adsorbent force-field for these materials, and in particular the question of the transferability of parameters – an issue that is critical to the prediction of adsorption using molecular simulation. The Lennard-Jones potential-well depth parameter for the silanol oxygens, $(\epsilon_o/k_B)_{\text{solid}}$,

commonly used for simulating adsorption in PMSs is 185 K,^{4-5, 9, 15-16, 20} but this parameters was obtained by studying ethane adsorption on a smooth-pore representation of MCM-41,⁹ while our SBA-2 model pores exhibit realistic pore roughness. For this reason, we study its transferability to our model pores, acknowledging that, along with surface roughness, $(\epsilon_0/k_B)_{\text{solid}}$ has a great impact on adsorption at low pressure. The simulated adsorption isotherms are compared to experimental results obtained by Pérez-Mendoza and co-workers⁴⁻⁵ on a sample calcined at 550 °C.

SIMULATION METHOD

The kMC simulation method is presented in full in our earlier paper.¹⁷ Here we focus on aspects that are relevant to the modeling of adsorption in the model materials and the comparison of the adsorption predictions with experimental data. As we indicated earlier, the real material is in practice a mixture of SBA-2 (with hcp symmetry) and STAC-1 (with ccp symmetry).³ In order to obtain the hcp symmetry of SBA-2, the simulation cell must contain two cavities while for the ccp symmetry of STAC-1 a single cavity is sufficient.¹⁷ Henceforth we refer to the “single-cavity” model as SC, and TC for the “two-cavity” model, both representative of the distinct phases in the mixed material produced experimentally. We compare our simulated adsorption results with experimental data reported by Pérez-Mendoza,⁴⁻⁵ who estimated a pore size of ~ 47 Å for the experimental material sample.

Table 1 summarizes the main characteristics of the model pores used for this study. The diameter of each of the cavities, the variation of the local pore surface from a spherical shape (expressed as a standard deviation), and the connections of the cavities via the windows to their neighbors were studied by means of the random walk technique described elsewhere.¹⁷ The accessible surface area of these materials was determined by simulating rolling a probe molecule across the surface.²¹ In both these computations, a probe with a diameter of 3.3 Å was used.

The SC model pore used for this study has a mean cavity diameter of 47.2 Å and standard deviation of 3.7 Å, while the two pores in the TC model have mean cavity diameters of 47.6 and 48.9 Å with standard deviations of 1.8 Å and 2.5 Å respectively. The higher standard deviation of the SC model is already an indication of its higher surface roughness when compared to the TC pore model. The pores in the SC and TC models have a similar surface area.

Table 1: Properties of the SC and TC models used in this study.

	SC	TC
Unit cell parameter (Å)	52.1 / 53.3 / 50.1	53.2 / 53.2 / 85.5
Unit cell mass (g/mol)	5.17×10^4	1.09×10^5
Number of Si atoms	810	1693
Number of silanol oxygen atoms	341	797
Pore diameter (Å)	47.2 (± 3.7)	47.6 (± 1.8) / 48.9 (± 2.5)
Surface area (m²/g)	1290	1245
Skeletal density (g/cm³)	3.31	3.29

Adsorption was simulated using grand canonical Monte Carlo (GCMC) simulation.²² In this method, the thermodynamic state is defined by constant temperature T , constant volume V , and constant chemical potential for each adsorptive species i , μ_i , which was related to the pressure using the Peng-Robinson equation of state.²³⁻²⁴ We modeled Coulombic interactions using the Ewald summation technique²² and dispersive interactions using the 12-6 Lennard-Jones (LJ) potential, with the Lorentz-

Berthelot mixing rules being used to calculate mixed Lennard-Jones parameters. The LJ parameters and partial charges used in this work are given in Table 2.

Table 2: Interaction parameters used in the GCMC adsorption simulations.

	Site	ϵ_i/k_B (K)	σ_i (Å)	q_i (e_0)	Reference
	Si	0.0	0.0	1.2805	
Pore wall	bO	165-200 [§]	2.708	-0.6402	9, 15-16
	nbO		3.000	-0.5261	
	H		0.0	+0.2060	
He	He	10.90	2.640	-	25
CH ₄	CH ₄	147.90	3.730	0.0	26
C ₂ H ₆ *	CH ₃	139.80	3.775	0.0	26
CO ₂ **	C	29.00	2.79	0.66450	27
	O	82.00	3.06	-0.33225	

* The CH₃-CH₃ bond length in ethane molecules is 1.53 Å

** The C-O bond length in CO₂ molecules is 1.161 Å

§ Range of values studied in this work

A value of 185 K for the LJ potential-well depth of the oxygen atoms in the adsorbent is widely used in the literature for simulating adsorption in PMSs,^{4-5, 9, 15-16, 20} particularly in the case of MCM-41. However, this parameter was originally derived for MCM-41 using experimental data for the adsorption of ethane and model pores with smooth walls.⁹ Unlike in the MCM-41 model originally used to set the value of the LJ potential-well depth, the kMC-generated pores are rough, and spherical in shape rather than cylindrical. It is thus likely that the appropriate LJ potential-well depth will be different for the model pores studied here, since the oxygen-adsorptive potential would be expected to more closely reflect the true interatomic interactions, without having also to compensate for an unrealistically smooth surface. This would be in line with recent simulation results for neopentane adsorption in kMC-

generated MCM-41 pores, which showed this value had to be changed to get good agreement between simulation and experiment.²⁰

GCMC simulations give the absolute amount adsorbed, N_{abs} , as a function of pressure. Experimentally, however, the excess amount adsorbed, N_{ex} , is measured. The transformation from one to the other is done through^{9, 25}

$$N_{ex} = N_{abs} - \rho_{bulk} V_{He} \quad (1)$$

where V_{He} is the pore volume, which is obtained by the GCMC simulation of helium adsorption (mimicking the use of helium to measure the pore volume in adsorption experiments), and ρ_{bulk} is the density of the bulk adsorptive at the simulated temperature and pressure, which is calculated using the Peng-Robinson equation of state.

The isotherms predicted by our models are scaled by the ratio of the maximum amount adsorbed measured experimentally and that predicted by simulating adsorption in the model pores, thus accounting for the difference in pore size between the model pores and the pores in the experimental sample (since they are not an exact match), and also for any non-porous defects such as pore blocking that are present on real samples but are not accounted for in the pore models.

RESULTS

First we determined the optimal value of $(\epsilon_o/k_B)_{solid}$ for predicting adsorption in the SC model by using a non-polar adsorptive, ethane, and assigning different values of this parameter for the oxygen atoms in the pore wall. We used the experimental ethane isotherm at 273 K, a relatively low temperature, because the location of the point of inflection, which is a sensitive measure of the strength of the solid-fluid interaction, becomes more prominent as the temperature is reduced. We studied values of $(\epsilon_o/k_B)_{solid}$ from 135 K to 200 K.

Figure 2 shows the predicted ethane isotherms using three different values for $(\epsilon_o/k_B)_{\text{solid}}$ compared with the experimental SBA-2 isotherm measured by Pérez-Mendoza *et al.*⁴⁻⁵ Using 185 K, the value widely used for MCM-41 simulations, as the potential well depth in the SC model leads to slight overpredictions of ethane uptake in the low-pressure range, suggesting that this value is too high. Thus, in Figure 2 we also present isotherms for $(\epsilon_o/k_B)_{\text{solid}}$ equal to 165 K and 135 K.

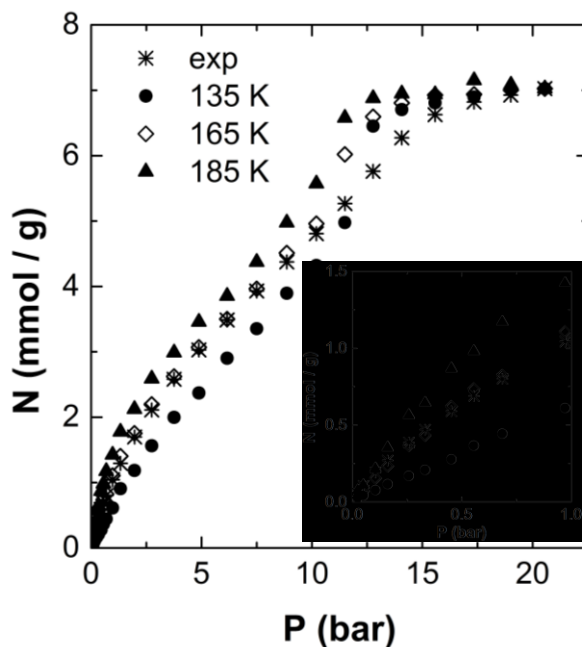


Figure 2: Experimental and simulated ethane adsorption isotherms at 273 K for different values of $(\epsilon_o/k_B)_{\text{solid}}$ in the SC model. The inset shows the low pressure region of the adsorption isotherms.

A reduction in $(\epsilon_o/k_B)_{\text{solid}}$ to 165 K improves the overall isotherm prediction including the low pressure region of the isotherm, which is a very sensitive measure for the fluid-solid interaction, while a further reduction to $(\epsilon_o/k_B)_{\text{solid}} = 135$ K gives much poorer results. This suggests that the optimal value is in the region of 165 K; this is confirmed by the calculation of the mean-squared errors in predicting the experimental isotherm, shown in Figure 3.

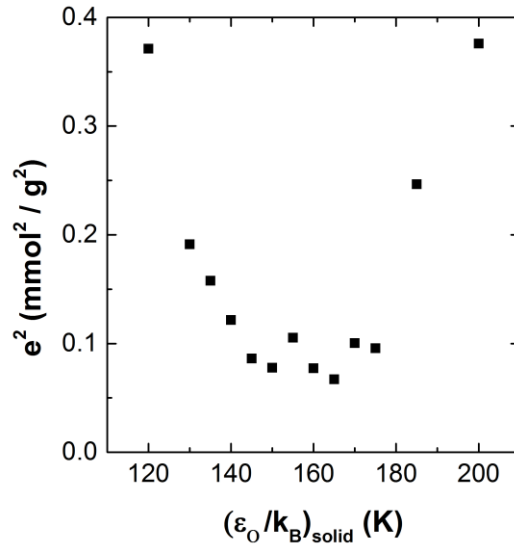


Figure 3: Mean-squared error for the deviation of the predicted ethane isotherms from the experimentally measured isotherm as a function of $(\epsilon_0/k_B)_{\text{solid}}$.

The observation that decreasing the value of the LJ parameter ϵ from the one originally derived for atomistically smooth model pores of MCM-41⁹ leads to overall improvement in adsorption predictions reflects the fact that the rough surface of our model pores results in a stronger overall solid-fluid interaction than would exist with a smooth surface. It is worth noting that, even with the optimal value of $(\epsilon_0/k_B)_{\text{solid}}$, pore filling in the model pores consistently occurs at $P \sim 12$ bar, slightly lower than the value measured experimentally. This indicates that the size of the model pore is somewhat smaller than that of the experimental sample.

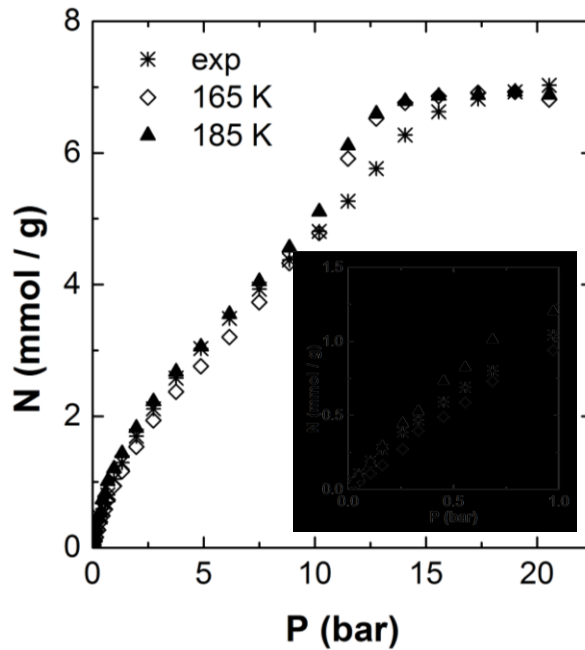


Figure 4: Ethane isotherms at 273 K predicted with the TC model for two values of $(\epsilon_o/k_B)_{\text{solid}}$. The inset shows the low pressure region of the adsorption isotherms.

To further investigate the role of the LJ parameter $(\epsilon_o/k_B)_{\text{solid}}$, in Figure 4 we present the predicted ethane isotherms at 273 K, now using the TC model. As in the SC model, there is good agreement in the low pressure region between the simulated and experimental adsorption isotherms. The pore filling pressure (the pressure at the point of inflection of the isotherm) is slightly underestimated, and whilst the difference between using the potential well depth for the adsorbent as 185 K or 165 K is not as marked as in the case of the SC model it can still be seen that the latter provides a better overall approximation to the experimental isotherm. We hypothesize that, since the pores in both the SC and TC models have comparable sizes, this is due to the smoother pore surfaces in the TC model pores (as indicated by the smaller standard deviations in the pore diameters reported in Table 1), resulting in an effective decrease in the solid-fluid interaction.

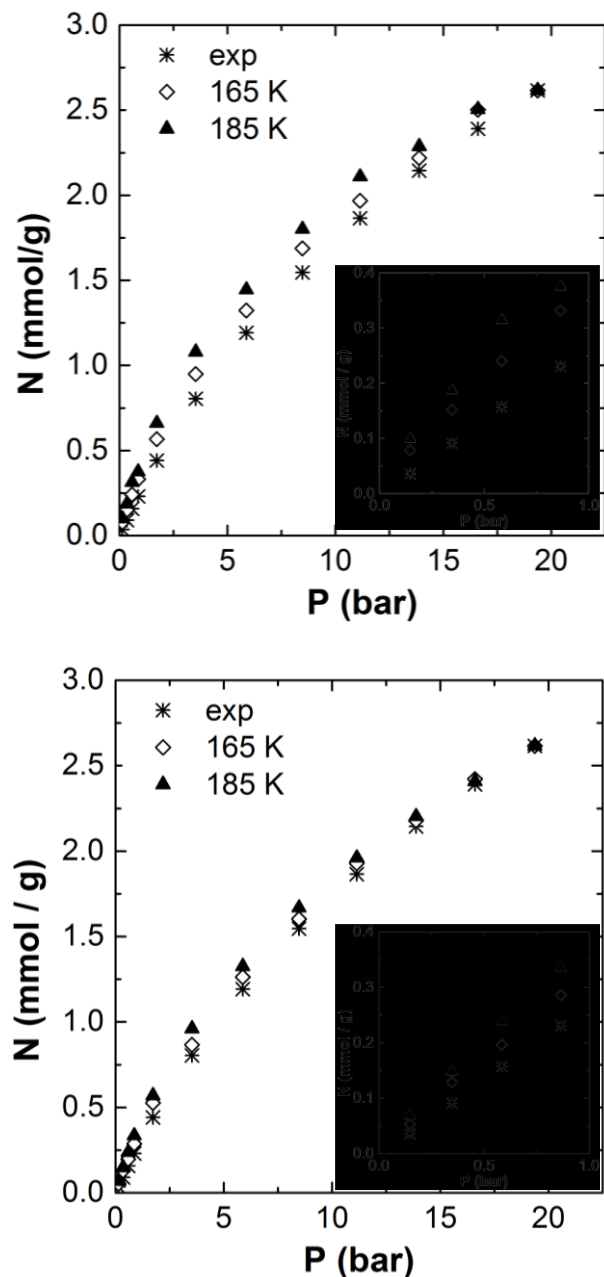


Figure 5: Methane isotherms at 263 K for two values of $(\epsilon_o/k_B)_{\text{solid}}$ using the SC model (top) and the TC model (bottom). The insets show the low pressure regions of the adsorption isotherms.

Given the overall improved adsorption predictions by the newly proposed value for the LJ parameter, we now use this new value in simulating the adsorption of other species. Since the SBA-2 experimental sample is not phase-pure, Figure 5 shows methane adsorption predictions at 263 K using both the SC (Figure 5 a) and TC (Figure 5 b) models. While both predicted isotherms are very close to

the experimental results over the whole pressure range, the better match is obtained with the TC model. The new value of 165 K leads to better predictions in the low pressure range thus providing further evidence that for both pore models the new Lennard-Jones parameter gives a better representation of the solid-fluid interactions than the commonly used value of 185 K, supporting the transferability of this parameter. [To be clear, by “transferability” we mean in this context the applicability of a fixed parameter value to different model materials of the same general class – in this case, models for PMS materials generated by kMC simulation. Of course, this is not to say that the same parameter value should be used for a smooth-pore model of the same PMS.] These results could be further improved by lowering $(\epsilon_o/k_B)_{\text{solid}}$ further, but this would compromise the prediction at higher pressures. Since the shape of the cavities in both the SC and the TC models is the same and methane adsorption in neither model material reaches pore filling, the difference in the predicted adsorption isotherm must be due to differences in the fluid-wall interactions, which in turn reflects the degree of surface roughness on the model pores. The fact that the predicted adsorption at low pressure is lower in the TC model than in the SC model again points to the surface of the TC model being less rough. The interaction of the methane molecules with the pore surface is illustrated in Figure 6, which shows that the small methane molecules can reside within nooks in the pore wall that are just big enough for them to enter; these are not accessible to larger molecules such as ethane.

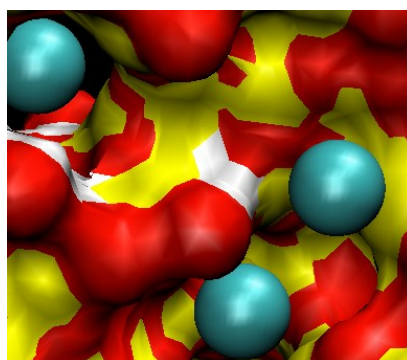


Figure 6: Snapshot showing methane molecules trapped in nooks in the surface of the SC model pore. Color code: yellow- Si atoms; red- oxygen atoms; white- hydrogen atoms; and blue- methane molecules.

Having studied systems with non-polar adsorptives, we now look at the predictive performance of the models when the adsorptive is polar in nature and both dispersive and electrostatic interactions play an important role. Figure 7 presents carbon dioxide predictions for both $(\epsilon_o/k_B)_{\text{solid}}$ parameters at 263 K in the SC and TC model pores.

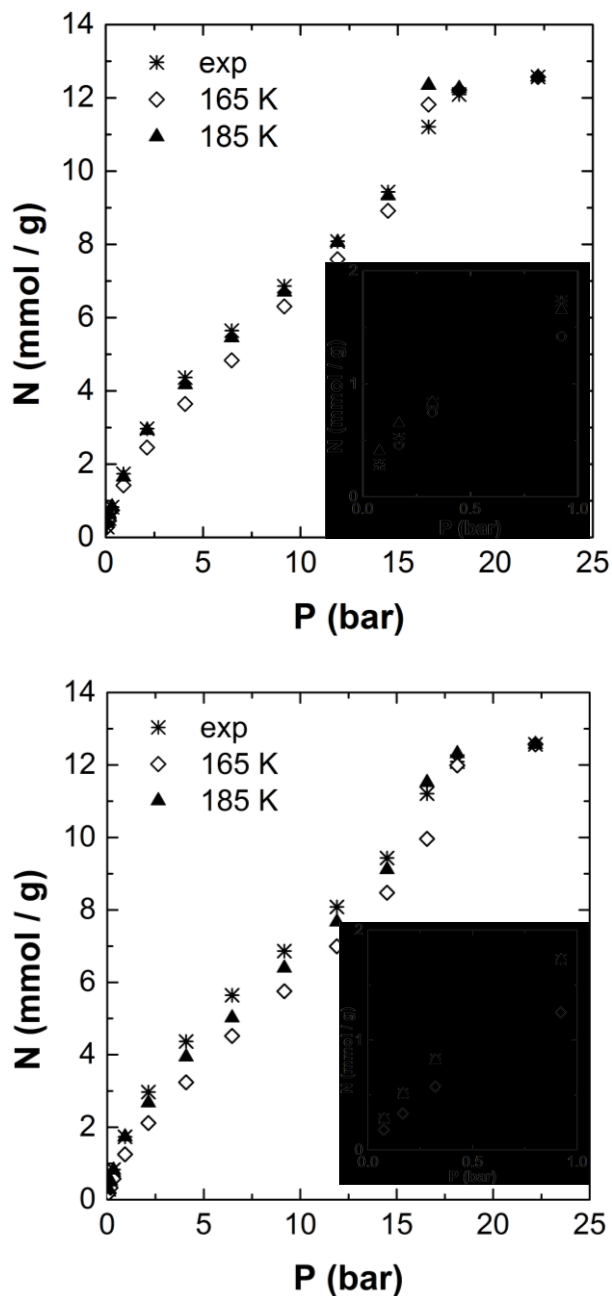


Figure 7: CO₂ isotherms at 263 K for two values of $(\epsilon_o/k_B)_{\text{solid}}$ using the SC model (top) and the TC model (bottom). The insets show the low pressure regions of the adsorption isotherms.

As illustrated in Figure 7a, the use of $(\epsilon_o/k_B)_{\text{solid}} = 165$ K for CO₂ in the SC pore model shows no improvement in the low pressure region predictions as well as a more marked inflection in the isotherm. The mean-squared error for the deviation between simulated and experimental isotherm is 0.0271 mmol² / g² for $(\epsilon_o/k_B)_{\text{solid}} = 165$ K and 0.0099 mmol² / g² for $(\epsilon_o/k_B)_{\text{solid}} = 185$ K. Also, as expected, the value of $(\epsilon_o/k_B)_{\text{solid}}$ has little impact on the accuracy of the predictions at higher pressures. Note that the SC model gives better predictions for CO₂ than it did for ethane, including better prediction of the pore-filling pressure.

Figure 7b shows CO₂ adsorption predictions using the TC model. As in the case of the SC model, the general features of the CO₂ isotherm are realistically captured, whilst quantitatively the simulations slightly underpredicted the experimental adsorption. When using the TC model, contrary to what was seen with the SC model, predictions at low pressure obtained using $(\epsilon_o/k_B)_{\text{solid}} = 185$ K are slightly more accurate. As in the case of ethane adsorption, this reflects the fact that the TC model has cavities with smoother pore surfaces than those of the SC model, and the larger $(\epsilon_o/k_B)_{\text{solid}}$ parameter for the solid compensates for the lower solid-fluid interactions.

CONCLUSIONS

We used models of SBA-2/STAC-1 generated by kMC simulation to study the adsorption of species of differing molecular size and polarity. The agreement between simulated and experimental adsorption isotherms is very good, particularly for ethane and CO₂. Methane adsorption is slightly overestimated, perhaps because the simulated material has pore surfaces that are slightly rougher than the real material. The fact that there are generally accurate predictions over the entire pressure range for both polar and non-polar adsorptives is a good indication that these model pores are a realistic

representation of SBA-2/STAC-1 from the point of view of adsorption. As adsorption is a sensitive probe of both surface structure and pore geometry, our results strongly support the realism of kMC-generated models for these materials, and suggest their wider applicability to PMSs. These models provide a useful tool for predicting the impact of material properties on adsorption in this class of materials, and for designing new PMS-based adsorbents for applications in gas storage and separation.

The Lennard-Jones potential-well depth parameter $(\epsilon_0/k_B)_{\text{solid}}$ commonly used for predicting adsorption in MCM-41 is found to overpredict adsorption at low pressures in SBA-2/STAC-1, and upon optimization a value of 165 K was found to provide better overall results. The better predictive behavior of the model pores with $(\epsilon_0/k_B)_{\text{solid}} = 165$ K seems to be due to the more realistic, rough nature of the pore surface, in contrast to the simplified, smooth surface of the models used to determine the literature value of $(\epsilon_0/k_B)_{\text{solid}} = 185$ K. This emphasizes that care must be taken when transferring parameters between models representing different systems, where the models have been generated using different methodologies.

ACKNOWLEDGEMENTS

We thank the DeSANNs project (EU FP6 STREP SES6CT2005-020133) and The University of Edinburgh for financial support, as well as Dr. Christian Schumacher and Dr. Manuel Pérez-Mendoza for their helpful advice. This work has made use of the resources provided by the Edinburgh Computer and Data Facility (ECDF). (<http://www.ecdf.ed.ac.uk/>). The ECDF is partially supported by the eDIKT initiative (<http://www.edikt.org.uk>)

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