

LASER BEES

A Concept for Asteroid Deflection & Hazard Mitigation

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frontier research on visionary space systems

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ASTEROIDS





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[Alvarz L et al, 1980] -

ASTEROIDS

- Asteroid 99942 Apophis, non-negligible impact risk, 2039
- Asteroid YU55 passes in-between the Earth's-Moon orbit, 2011
- Asteroid 2002 MN missed the Earth by only 120000 km, 2002
- Ground Impact, New Guinea, 1994
- Ground Impact, Grand Teton Park, USA, 1972
- Ground Impact, Pribram, Czechoslovakia, 1959
- Ground Impact, Sikhote-Alin, Russia, 1947
- Ground Impact, Curaca Crater, Brazil 1930
- Air Impact, Tunguska, Russia 1908
- Ground impact, Arizona, Barringer Meteorite Crater, 50000 years ago





asteroid diameter [m]



DEFLECTION METHODS



Methods of asteroid mitigation and deflection have therefore been addressed by numerous authors [Melosh, 1994; Conway 200]





Kinematic Impactor(s) Nuclear Blast

Impulsive Methods







Paint & the Yarkovsky Effect

Passive Methods

The overall performance depends on how the deflection method interacts with the asteroid, the response time, the mission complexity and the technology readiness

WHY SURFACE ABLATION?



[Sanchez at al. 2009]

Analysis from a multi-criteria quantitative comparison



Compared kinematic impactor, nuclear detonation, mass drivers, low thrust tug, ablation and the gravity tractor

Relative to the miss distance at Earth, the warning time, the total mass into orbit and the technology readiness levels

Ablation was shown to be, theoretically, a promising technique

No fragmentation of the asteroid No need to physically attach and/or land on the surface Energy source is freely available and external from the Sun Ablated material is the asteroid itself

A high rate of controllable deflection can be achieved.

Both with a relatively low mass into space and a short warning time

ABLATION



Ablation is achieved by irradiating the surface by light – direct solar radiation or laser – source . The resulting heat sublimates the surface, transforming it directly from a solid to a gas.





An ejecta cloud of the ablated material forms. This acts against the asteroid, providing a continually controlled low thrust



1. Melosh & Nemchomov, 1993, 1994

A large, single mirror – solar concentrator - mounted onto a single spacecraft

To collect, direct and concentrate solar light onto a small area of the asteroid



Technique requires a 1~10 km diameter mirror; Significant space structure Becomes susceptible to the deposition of ejecta Operates in close proximity to the asteroid, under an irregular gravity field



2. Campbell, Phipps et al, 1992, 1997; Park & Mazanek, 2005 Sublimate the asteroid with a high power, mega watt, laser Powered by a nuclear rector



Develop a large nuclear reactor for space applications

Significant legal ramifications of operating a nuclear reactor in space

Difficulties of manoeuvring and operating large structure



ALTERNATIVE METHOD:

[Vasile & Maddock, 2009, 2010; Sanchez, 2009]

- Fractionate the monolithic spacecraft into a number of identical units
- Swarm of small scale spacecraft, flying in formation about the asteroid
- Each equipped with a small solar concentrator [known as Mirror Bees]



Each spacecraft simultaneously collects and focuses solar radiation directly onto the asteroid's surface

By superimposing their light beams the required surface power density can be achieved, successfully ablating a small portion of the asteroid's surface

Swarm configuration is taken to be:

- A lighter, more adaptable concept
- Increased redundancy by design
- Scaleable





However each MIRROR BEE spacecraft still needs to be placed in close proximity to the asteroid

Technique is highly susceptible to the deposition and contamination of the ablated ejecta.

To increase the distance between the asteroid and spacecraft (~1 to 4 km)

Use a swarm of spacecraft

Each equipped with a small solar collector and a laser

A collimated laser beam can propagate over extended distance, without the loss of energy

LASER BEES





However, within the vicinity of the ejecta plume, any exposed surface(s) will be subjected to the contaminating effects of the condensing ejecta

LASER BEES, OPEN QUESTION



- Physical formation and evolution of the ejecta plume
 - 1. Is it similar to the formation of the rocket exhaust in rocket propulsion?
 - 2. Is there uniform dispersion of the ejecta over the given hemisphere?
 - 3. Is a constrained plume of ejecta more plausible?
 - 4. What particles are contained within the ejecta?
 - A. Only hot gas? Any solid particles?
- Ablation response for different material
 - 1. What is the difference between dense and porous material?
- Sensitivity of contamination and degradation of the ejecta
 - 1. What is the actual degradation rates of the exposed surface? $f(r, \theta)$
 - 2. What are the physical properties of the condensed material?
 - 3. Does all the ejected material immediately stick?
 - 4. Is there any attenuation of the laser beam?

Can we ensure the maximum survivability of the system to maximise the achievable deflection of the technique ?

ABLATION EXPERIMENTS





A series of laser ablation experiments using a 90 W continuous-wave laser has been performed



Investigate the development of the ejecta plume – mass flow rate, velocity and divergence – and the potential for contamination.



Calibrate and validate the development of numerical models and existing theory

[Vasile & Maddock, 2010; Sanchez et al, 2009]



Current assumptions in the numerical method must be verified

Ejecta depends on the available energy & efficiency of the ablation process [Vasile & Maddock, 2010; Phipps 2010; Sanchez, 2009; Kahle 2006]

Plume profile is similar to a rocket exhaust



Standard methods of rocket propulsion

Uniformly expanded gas of ejecta; No solid particles

No ionization of the gas; Constant scatter factor

Assumed a spherical, dense, homogenous body



Forsterite (Mg2Si04) is typically used

Asteroid has an infinite heat sink

Constant internal temperature during sublimation

Ejected particles will immediately condense and stick

Assumptions on the degradation and attenuation



The sublimation process is modelled on the energy balance [Vasile & Maddock, 2009, 2010; Sanchez, 2009]

Combines the absorption of the laser beam P_{IN} , the heat losses of conduction Q_{COND} and radiation Q_{RAD} respectively and the sublimation enthalpy of the target material E_v

$$\frac{dm}{dt} = \frac{1}{E_v} \left(P_{IN} - Q_{RAD} - Q_{COND} \right)$$

$$Q_{RAD} = \sigma_{SB} \varepsilon A_{SPOT} \left(T_{SUB}^4 - T_{amb}^4 \right)$$
Assumes a black body
$$Q_{COND} = \left(T_{SUB} - T_0 \right) A_{SPOT} \sqrt{\frac{c_A \rho_A \kappa}{\pi t}}$$
Assumes an infinite heat sink



Average velocity of the gaseous ejecta is calculated from Maxwell's distribution Assuming the behaviour of a ideal gas

$$\overline{v} = \sqrt{\frac{8kT_{sub}}{\pi M_a}}$$

Force and acceleration acting on the asteroid:

$$F_{SUB} = \lambda v m_{exp}$$

$$a = \frac{F_{SUB}}{M_A}$$

Assumes a constant scatter factor Account for the dispersion of the ejecta plume Considered to distribute uniformly over a half sphere Conservative assumption



Density of the ejecta plume

Function of distance, r, from the spot and angle, θ , from the centre line



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Contamination and degradation

[Kahle et al, 2006]

Will occur to any exposed surface located within the ejecta volume Assumed that all particles – gas – will re-condense and stick

Variation in ejecta thickness – surface growth - is given by:

$$\frac{dh}{dt} = \frac{2\overline{v\rho}}{\rho_{layer}} \cos(\psi_{vf})$$

 ψ_{vf} is the view angle

 ρ – Density of the ejecta

 ρ_{layer} - Layer density. This is assumed to be 1000 kg/m³ η - Absorption coefficient (silica, at 800 nm, ~ 10⁶/m)

1

The degradation factor, т,

$$c = e^{-2\eta h_{END}}$$

Beer-Lambert-Bougier law





MISSION CASE

Assuming the parameters, given in Kahle Condensed ejecta density of 1000 kg/m³ Absorbitivity of 10⁶ m⁻¹



Mirror diameter d=10m, C_r=5000, laser efficiency=0.6, cell efficiency=0.4



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OBJECTIVES





Performed a series of ablation experiments using a 90 W continuous-wave laser



Investigated the development of the ejecta plume – mass flow rate, velocity and divergence – and potential for contamination.



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[Vasile & Maddock, 2010; Sanchez et al, 2009]

THE LASER





A 90 W continuous wave laser

(LIMO 90-F2000-DL808)

Fibre-coupled semiconductor

Operating at 808 nm





Horizontally mounted and cooled by a recirculation chiller at 15 °C After focusing, it provided an approximate spot diameter of 0.5 mm After losses provides 30 kW/cm², surface power density, at the focus

EXPERIMENT SEQUENCE



- Initial ablation experiments first occurred under a nitrogen purge environment
 - Transparent test chamber
 - Reduce the occurrence of atmospheric combustion to negligible levels. Any innate material combustion still occurred.
 - Tested and refined the proposed methodologies and techniques
 - Either measured, calculated or inferred quantities
- Developed and integrated the vacuum chamber system
 - Allowed for maximum expansion of the plume
 - Eliminating particle drag caused by an atmosphere

THE EXPERIMENT

Ejecta is collected on microscope slides.

Measure the deposited mass of the ejecta

Measure the affect of contamination and degradation

High resolution cameras

> Used a thermocouple measure the temperature of the target material during ablation

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University High resolution cameras

Measure the divergence and formation of the ejecta plume

> Measure the ablation time

Focusing Optics

Laser off screen

Measured the mass of the target material before and after. Enabling the mass flow rate of ablation to be determined

THE EXPERIMENT







Used a spectrometer to **measure the spectra** – wavelength vs intensity - **of the ablated spot**

Temperature of the spot was then inferred from the Wein displacement law

$$\lambda_{PEAK}T_{SUB} = 2.898 * 10^{-3}$$

 $v = \sqrt{\frac{8kT_{sub}}{\pi M_a}}$

Used a microscope to **measure the height of the collected ejecta** on the slides and the **diameter of the ablated hole**

$\eta_{EXP} = \frac{a_b}{h_{EXP}}$

Measured the depth of the ablation hole

Measured the transmittance/absorption of the ablated slides

Calculated the absorbance per unit length, η , of the ejecta

Used a Scanning Electron Microscope to study the composition of the plume









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TARGET MATERIAL



Sandstone Represent a rocky, dense asteroid Bulk density: 2250-2670 kg/m³





Fabricated a composite mixture Represent a highly porous, rubble pile asteroid Expanded perlite, sand, fly ash and water Bulk density ~ 400 kg/m³ Bulk porosity ~ 80 %

[Housen, 2004, Housen & Holsapple 2003]

THE EXPERIMENT





NITROGEN PURGE







Subjected to the structure and composition of the target material Small, and extended rocket plume Similar mass flow rate, compared to the model

Variation in cone angle and ejecta distribution Ablation process included solid ejecta particles Subjected to the volumetric removal of material Resulted in the laser tunnelling into the subsurface Technique is sensitive to the focal point of the laser




NITROGEN PURGE





Sandstone



Composite Porous

Local depositions in and around the ablation volume White residual was deposited around the ablation rim Within the ablation volume a semi-melted glassy material is created

These depositions do not contribute to the formation of the ejecta plume

Ablation hole was larger that the spot size diameter Original illumination 0.5 mm (assumed constant in model) Sandstone – 1.83 mm Porous – 2 mm

Volumetric heating of the target material

Leads to increased ablation for a lower energy input No observable attenuation of the laser beam

VACUUM

Small & extended rocket plume. Little ejecta At 3, 7 and 10 cm away from the spot: Measured the deposited mass/area, $(\Delta m/A)_{SLIDES}$ Measured the height of the ejecta, Δh_{EXP}



From this the density of the deposited material can be calculated $\rho_{EXP}(r,\theta)$ Derive the expected collection rate of ejecta on each slide



$$p_{l,EXP}(r,\theta) = \frac{\left(\frac{\Delta m(r,\theta)}{A}\right)_{SLIDES}}{\Delta h_{EXP}}$$

$$\frac{1}{A}\frac{dm}{dt} = 2\rho(r,\theta)\overline{v}$$

Measured the transmittance of the slides

MASS FLOW RATE, SAMPLE



Surface illumination of either a 43 W or 62 W laser beam

<u>-3 VV</u>	60.1
heorv: 2.59 ⁻ 10 ⁻⁸ ka/s	<u>02 v</u>
	The
Exp: 2.40 ⁻⁸ kg/s (-7 %)	
Exp: 3.90 ⁻¹⁰⁻⁸ kg/s (+50 %)	E
Exp: 2.12 ⁻¹⁰⁻⁸ kg/s (-18 %)	E
	E

ory: 3.17[•]10⁻⁸ kg/s

Exp: 4.63⁻¹⁰⁻⁸ kg/s (+25 %) Exp: 3.07⁻¹⁰⁻⁸ kg/s (-17 %) Exp: 5.65⁻10⁻⁸ kg/s (+52 %) Exp: 4.43⁻¹⁰⁻⁸ kg/s (20 %) Exp: 3.28⁻¹⁰⁻⁸ kg/s (-12 %)

Variations are considered to be caused by local variations in the rock sample







THICKNESS, DEPOSITED MATERIAL





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COMPARISON



- Model predicts significantly greater degradation that observed
 - Expected to be higher at lower angles; plume density is larger.
- HOWEVER, instead, the experimentally measured thickness is much higher
 BUT with equal mass per unit area
- Density of the deposited ejecta is much lower than assumed
 - Model: 1000 kg/m³ with an assumed absorptivity of 10⁶ m⁻¹
 - Experiment:
 - At 7 and 10 cm away

Reasonable to assume that at 3 cm the plume is very focused

Expansion leads to a more distributed layer of material at 7 and 10 cm

COMPARISON

Experiment had a correlated mass flow and deposition rate

However, the model assumed:

An incorrect growth of the deposited material

- An incorrect density of the ejected material
- An incorrect absorptivity
- That all the material bonded with the slides

Represents an inaccuracy within the modelling technique

Experiment also demonstrated

- Variation in cone angle & dispersion geometry
- Variation in distribution of ejecta
- Ablation includes the ejection of solid particles f(material)
- Subject to the volumetric removal of material & material phase change Subject to the depth of focus of the laser



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LASER BEES, OPEN QUESTION



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Can we ensure the maximum survivability of the system to maximise the achievable deflection of the technique ?





MISSION CASE

Assuming the parameters, given in Kahle Condensed ejecta density of 1000 kg/m³ Absorbitivity of 10⁶ m⁻¹



Mirror diameter d=10m, C_r=5000, laser efficiency=0.6, cell efficiency=0.4



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MISSION CASE

Using the experimental data OLIVINE



Deposited ejecta density of 250 kg/m³ and an absorbitivity of 5·10⁴ m⁻¹

Mirror diameter d=10m, C_r =5000, laser efficiency=0.6, cell efficeincy=0.4



MISSION EXTENSION



Experiment also demonstrated that laser ablation can be used for a wide range of space-based missions. Once a plume of ejecta has been formed:

In-situ Spectra Analysis Collection & Sample Return Resource Extraction Resource Exploitation Capture & Control



Contactless method

No requirement to land and attach to the asteroid No complex landing operations No fragmentation of the asteroid

Durability and diversity of a space-based laser system

DEVELOPMENT, FUTURE WORK



However a number of questions still remain unanswered. This includes:

- Ablation experiment on a pendulum, rather than static sample
- Ablation from a highly angled laser beam
- Ablation of a pulsed laser beam, assess higher energy ablation
- Ablation of inhomogeneous, irregular rotating samples, affect of porosity
- Using a thermal and high speed camera
 - Identification of the ejecta plume and measuring the velocity of the ejecta
 - Spot, slide and target material temperature profile during ablation f(t)
 - Efficiency of the self cleaning action
- Effect of slide heating in the contamination of the deposited ejecta
- Assess the composition and distribution of the ejecta
 - AFM for global topography and SEM for composition
- Measure the deposition of ejecta *in-situ* as a function of time
- Experiments with *in-situ* measuring of the mass flow, relative to the depth of focus
- Measure the force directly imparted onto the asteroid during ablation
- Enhanced quality reduced pressure of the vacuum chamber







Thank you for your time & the continued support of The Planetary Society.



Questions Please

References

Conway, B.A "Near-optimal deflection of Earth-approaching asteroids". *J.Guidance, Control and Dynamics* 24 (5), 1035–1037, 2001

Gritzner, C., Kahle, RMitigation technologies and their requirements, in: Belton, M.,Morgan, T., Samarainha, N., Yeomans, D. (Eds.), Mitigation of Hazardous Comets and Asteroid. Cambridge University Press, Cambridge, pp. 167–200, 2004

Housen "Collisional Fragmentation of Rotating Bodies", Lunar and Planetary Science XXXV, No 1826, 2004 Housen K.R, Holsapple K "Impact Cratering On Porous Asteroids". Academic Press, Icarus 163. Pg 102-119, 2003

Kahle R, Kuhrt E, Hahn G, Knolenberg J "Physical Limits of Solar Collectors in Deflecting Earth-threatening Asteroids" Advanced Science and Technology, Vol 10, pg 256-263, 2006

Melosh, H.J., Nemchinov, I.V., Zetzer, Y.I. Non-nuclear strategies for deflecting comets and asteroids, in: Gehrels, T. (Ed.), Hazards due to Comets and Asteroids. University of Arizona Press, Tucson, AZ, pp. 1111–1132, 1994

Phipps C, Birkan M, Bohn W et al "Review: Laser Ablation Propulsion", Journal of Propulsion and Power, Vol 26, No 4, 2010

Sanchez, J.P., Colombo, C., Vasile, M., et al "Multicriteria comparison among several mitigation strategies for dangerous Near-Earth objects". *J. Guid. Control Dynam.* 32, 121–141, 2009.

Vasile M, Maddock C "On the Deflection of Asteroids with Mirrors", *Journal Celestial Mechanical Dynamics*, Vol 107, pg 265-284, 2010

Vasile M., Maddock C., Radice G., McInnes C "NEO Deflection though a Multi-Mirror System", ESA Call for Proposals: Encounter 2029, Final Report for Ariadna Study Contract 08/4301, Technical officer: Summerer L., March 2009.

Alvarz L et al, Extraterrestrial Cuase for the Cretaceous-Tertiary Extinction, Science 6, Vol 208, no 4448, 1980



BACK-UP MATERIAL

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SEM – TARGET MATERIAL





Re-crystallisation around ablation hole rim

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SEM – DEPOSITED EJECTA







Ablated material is chemically identical to the target material







SPECTRA ANALYSIS





METEORITES



Spectra bands show that ordinary Choridities have similar mineralogy to S-type asteroids.



Bensour [LL]

Recovered from a 2002 fall, Morocaan-Algerian Negligible terrestrial alteration Low iron, olivine, magnesium silicate [foresterite] Porosity ~ 10 %

To represent a C-type a carbonaceous choridrite meteorite, Allende, was

selected



Allende is a meteorite from a very rate, witness fall

The carbonaceous choridrite is rich in carbon, and contains microscopic diamonds Approximately 46 billion years old

METEORITES



To represent an M-type asteroid, the meteorite Thuathe was selected



THUATHE

Witnessed fall July 21, 2002, Lesotho H4/5 Ordinary Chondrite High iron content

Each meteorite ideally needs to be sourced from a witness fall (freshly fallen stone), with limited weathering and fusion crust.

Ablation has to occur onto the meteorites surface, not the fusion crust.



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